

THE
Young Gentleman's
TRIGONOMETRY,
MECHANICKS,
AND
OPTICKS.

Containing such
ELEMENTS of the said Arts
or Sciences, as are most Useful
and Easy to be known.

By EDWARD WELLS, D.D.
Rector of Cotesbach in Leice-
stershire.

L O N D O N,
Printed for James Knapton, at the Crown
in St. Paul's Church-Yard. 1714.

THE
Young Gentlemen

TRIGONOMETRY
MILITARY

OP TICS

By J. H. M. ...
of ...
the ...

By ...
Hector of ...
Paris

LONDON
Printed for ...
in St. Paul's Church-yard

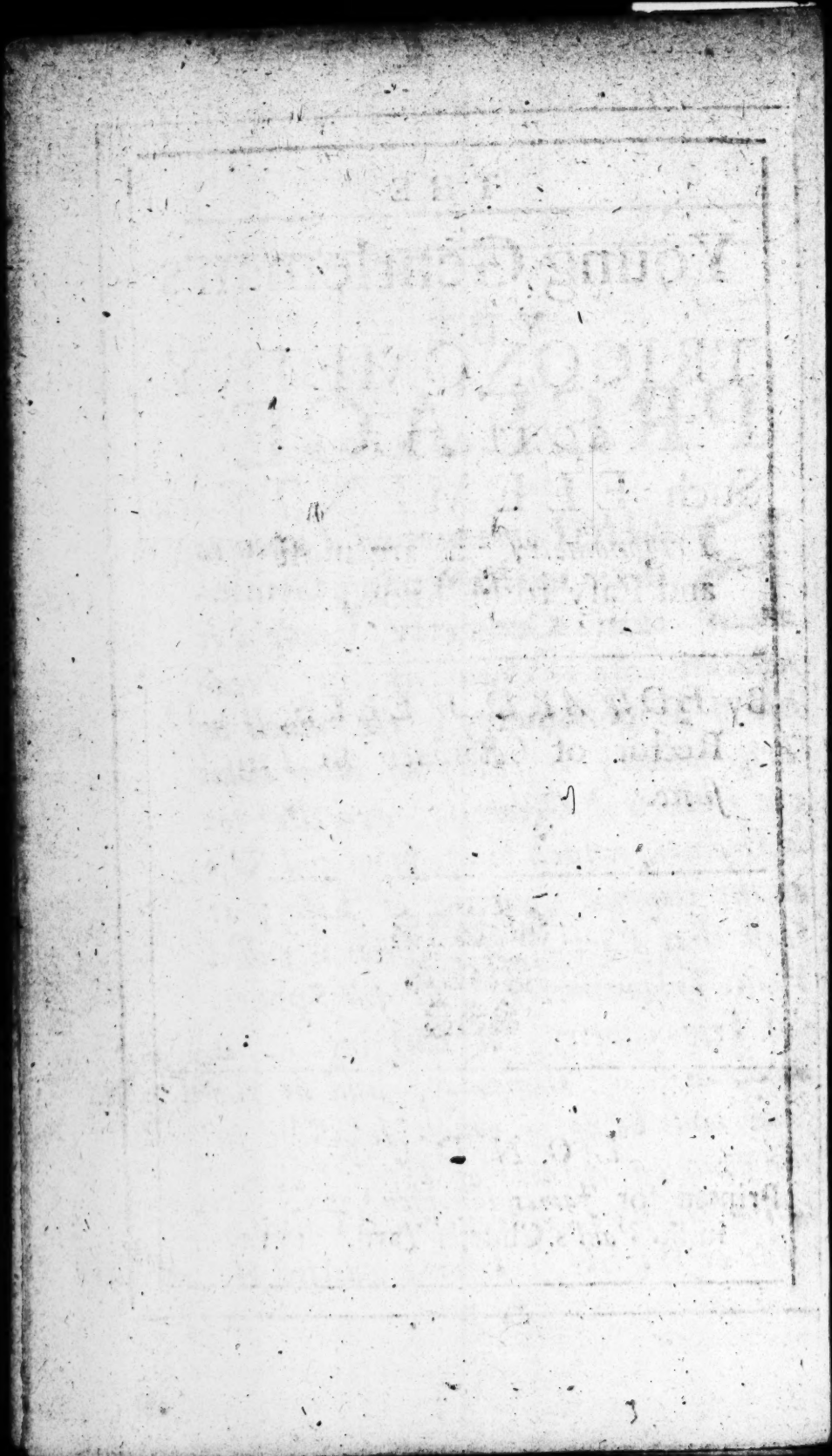
THE
Young Gentleman's
TRIGONOMETRY:

CONTAINING
Such ELEMENTS of
Trigonometry, as are most Useful
and Easy to be known,

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THE
PREFACE.

B *EING* once prevail'd upon to draw up the Young Gentleman's Geometry, I judg'd it requisite also to draw up this Treatise of Trigonometry; forasmuch as Trigonometry is really no other than one Branch of Geometry, and that too a Branch, which is of principal Use in the common Concerns of Life; at least that Part of it, which is call'd Plain Trigonometry. As for Spherical Trigonometry, it carrying in it much more of Difficulty, and at the same time being of much less Use in the common Affairs of Life, (as relating chiefly to Astronomical Calculations or the like,) I have omitted it,

The Preface.

as not agreeable to the Design of this Treatise.

On the like Account, tho' I judg'd it not proper wholly to omit the Fundamental Theorems of plain Trigonometry; yet I have plac'd them so in Chap. II. that the young Student may pass them over, without any Abruptness, if the Demonstration of the two latter prove too difficult, or at least if he cares not to take the Pains to make himself Master of the said Demonstrations.

THE

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T H E

THE
Young Gentleman's
TRIGONOMETRY.

CHAP. I.

Containing the Explication of Trigonometrical Terms.

EVERY Triangle consists in all of seven Parts, viz. three Sides, three Angles, and the Area or Space comprehended by the Sides. Now, although the Word *Trigonometry* do's in the Greek Language literally signify the Measuring of a Triangle; yet, in its proper Sense, or as it is distinguish'd from *Geometry*, it do's not denote the measuring of the Area of a Triangle, this being deduced from (*) other than what are

1.
Trigonometry, what.

(*) The Measuring of the Area of a plain right-lined Triangle, is deduced from the Principles of Geometry,

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are properly call'd Trigonometrical Principles, but it) denotes only the Measuring, or rather the Art of finding the Measure of, the unknown *Sides and Angles* of a Triangle, by the Help of those that are given or known.

2.
The Solution of a Triangle, what.

And the actual finding of the unknown *Sides and Angles* of a Triangle, is call'd, in one Word, the *Solution* or *Resolving* of a Triangle.

3.
The Solution of Triangles on what founded.

The Solution of Triangles is founded on that mutual Proportion, which is between the *Sides and Angles* of any Triangle. And this Proportion is known by finding the Proportion, which the *Ray* of a Circle has to certain other right Lines apply'd to the same Circle. And these right Lines are distinguish'd in general by the Names of *Chords, Sines, Tangents, and Secants*.

4.
A Chord, what.
Fig. 1.

A (+) *Chord* is a right Line drawn from one Extremity of any Arch to the other. Thus, Fig. 1, CH is the Chord

(as distinguish'd from Trigonometry,) viz. from *Theorem Chap. 1, of the Young Gentleman's Geometry*. And the Measuring of the Area of a Spherical Triangle, is deduced from the Measuring of a Spherical Surface.

(+) As an *Arch* is so call'd, because it resembles a *Bow*; so a *Chord* is so call'd, because it resembles the *String* of a bent Bow. It is otherwise call'd a *Subtense* because it *subtends*, (i. e. is extended under) the Arch from one End of it to the other.

bot

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both of the lesser Arch CTH , and also of the greater Arch CDH . And it is to be noted, that a Chord of 60 Degrees, is always equal to the Ray of the same Circle.

A (H) *Sine* is either a Right or Versed *Sine*. A *right Sine* is one Half CA of a Chord CH , bisected by the Diameter DT ; or, it is a Perpendicular CA , let fall from Cone End of an Arch CT , upon a Diameter DT , drawn from T the other End of the Arch. A *right Sine* is frequently stil'd simply a *Sine*; and it is to be observ'd, that by the Word *Sine*, put simply or by it self, is always to be understood a *right Sine*.

It is also to be observ'd, that, according to the fore-going Definition of a *Sine*, the *Sine* BK of an Arch KT of 90 Degrees, is always equal to the Ray of the same Circle; and so the greatest *Sine* that can be. Whence it is call'd, the *total* or *whole Sine*.

A (*) *vers'd Sine* is the Segment of the Ray intercepted between the right

8.
A *Sine*, or *right Sine*, *what*.

6.
A *total* or *whole Sine*, *what*.

7.
A *vers'd Sine*, *what*.

(H) The Use of *Sines* is said to be introduced by the *Greeks*; and for what Reason a *Sine* is so call'd, I know no good Account.

(*) A *vers'd Sine* is otherwise call'd, at least by some ancient Writers, the *Sagitta* or *Arrow*, because it stands its Arch and Chord, as an Arrow do's to its Bow when bent) and String.

B 2

Sine.

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Sine and the Arch. Thus, AT is the vers'd Sine of the Arch CT , and AD the vers'd Sine of the Arch CD .

8.

A Tan-
gent, and
Secant,
what.

A $(\dagger)$ *Tangent* and a *Secant* mutually explain one the other. For, if a right Line BN of an indeterminate Length be drawn from the Center B , through C one End of an Arch CT , and from T the End of the Diameter DT , there be erected a Perpendicular TN , extended till it meets with BN ; the said Perpendicular TN will be the *Tangent* of the Arch CT , and the Line BN will be the *Secant* of the same Arch. And it is to be noted, that the *Tangent* of 45 Degrees, is always equal to the Ray of the same Circle; as may be seen, *Fig. 2.*

9.

A Cosine,
Cotan-
gent, Cose-
cant, and
Covers'd,
what.

As when the Arch CT is less than 90 Degrees, the Arch CK (which, being added to the Arch CT , do's compleat make it up an Arch of 90 Degrees thence) is call'd the $(\parallel)$ *Complement* of the Arch CT ; so (*Fig. 1.*) the Sine CQ , the *Tangent* KO , the *Secant* BO , and the vers'd Sine KQ of the Arch CK , are re-

$(\dagger)$ A *Tangent* is so nam'd, because it touches (not cuts) one End T of its Arch CT ; and a *Secant* is so nam'd because it cuts or crosses the other End C of its Arch CT .

$(\parallel)$ It is not to be omitted, that the Excess CK of the Arch CD above 90 Degrees, is by some Writers call'd the *Complement* of the said Arch CD .

Spective

Trigonometry.

5

pectively call'd the *Sine*, the *Tangent*, the *Secant*, and the *vers'd Sine* of the *Complement* of the Arch CT; or in short, the (*) *Cosine*, the *Cotangent*, the *Cosecant*, and the *Covers'd* of the said Arch CT.

The Arch CD, (which, being added to the Arch CT, makes it up a Semicircle,) is peculiarly (†) call'd the *Supplement* or *Conjunct* of the Arch CT. And it is to be noted, that both the Arch CT, and its *Conjunct* CD, have the same *Sine* CA, the same *Tangent* TN, and the same *Secant* BN.

Tables of (II) *Sines* and *Tangents* are so call'd, because in them is set down the *Ratio* or *Proportion*, which *Sines* and *Tangents* have to their *Ray*.

10.
The Supplement or
Conjunct
of an Arch,
what.

11.
Tables of
Sines and
Tangents,
what.

B 3

And

(*) It is of Use to observe, that the *Cosine* CQ is always equal to BA, the Segment of the Ray between the Center B, and the *Sine* CA. Wherefore, if the Arch CD be greater than 90 Degrees, then the Sum of the Ray and *Cosine* is equal to the *vers'd Sine*; viz. $DB + BA = DA$. But, if the Arch CT be less than 90 Degrees, then the Difference of the Ray and *Cosine* is equal to the *vers'd Sine*, viz. $BT - BA = AT$.

(†) Namely, to avoid Confusion by giving the same Name of *Complement*, both to CK and to CD, as is done by some.

(II) It appears from §. 5, of this Chapter, that every *Sine*, (i. e. right *Sine*) is the Half of a Chord, and that the Arch of the *Sine*, is the Half of the Arch of the said Chord. Wherefore, because there is the same Proportion between two Halves, as there is between their Wholes, and the said Proportion between the Halves

12.
Natural
and artifi-
cial Sines
and Tan-
gents,
what.

And it is to be noted, that, if the said Proportion be express'd in the Tables by natural or common Numbers, then the Table is call'd, a Table of *natural* Sines and Tangents. But, if the said Proportion be express'd by artificial Numbers, *i. e.* Logarithms, then the Table is call'd, a Table of (*) *artificial* Sines and Tangents.

13.
A Scale or
Line of
Chords,
Sines, Tan-
gents, and
Secants,
&c. what.
Fig. 2.

If the said Proportion be not express'd by Numbers, but the several Sines and Tangents, as also (†) Chords and Secants, be themselves actually transferr'd into, (*i. e.* their several Lengths set off upon) several distinct Scales or Lines, (as Fig. 2); then the said Scales or Lines are respectively

(as being expressible in less Numbers) is much easier to be calculated, than the Proportion between their Wholes; hence, Sines are used rather than Chords in Trigonometrical Calculations, and the Proportion of Sines (not of Chords) to the Ray is set forth in Trigonometrical Tables.

(*) It has been afore observ'd in my *Arithmetic* that the *Multiplication* and *Division* of great Numbers is much easier to be perform'd by Logarithms than by natural Numbers. Hence it is that Tables of artificial Sines and Tangents, are more used than those of natural Sines and Tangents, and consequently adjoin'd to most Trigonometrical Treatises.

(†) The Reason, why there are no Tables of Chords has been observ'd already in the Note on §. 11. There are however Scales of Chords, these being as easily made as Scales of Sines, and as easy or easier for Use in some Respects. And the like is to be understood of Secants.

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respectively stild, one a *Scale* or *Line* of *Chords*, the other of *Sines*, the other of *Tangents*, and the other of *Secants*. And the like is to be understood of the Scales of any other Sort of Trigonometrical Lines, as of vers'd Sines, Cosines, &c.

Besides the fore-mention'd Scales, there is also another Sort of Scale, call'd a *Scale of equal Parts*; which, although it

14.

A Scale of
equal
Parts,
what.

Fig. 3, &c

4.

viz. as to the Reason, why there are few or no *Tables* of them, but there are usually, if not always, *Scales* of them adjoin'd to the other Scales. If it be ask'd, why the Scale of Chords is never continued beyond 90 Degrees, when the greatest Chord is the Diameter or Chord of 180 Degrees? The Reason is, because the Chords above 90 Degrees, may be very easily supply'd by a Scale of Chords to 90 Degrees, viz. Chord of 105 Degrees = Chord 90 Degrees + Chord 15 Degrees. And so of any other to 180 Degrees. The Reason, why Tables and Scales of Sines go no further than 90 Degrees, is obvious, viz. because a Sine of 90 Degrees, is the greatest Sine that can be, as appears from S. 5. and 6. of this Chapter. In like manner, the greatest Tangent and Secant is of 89 Degrees, 59 Minutes. For, at 90 Degrees, Lines drawn in like manner as a Tangent and Secant, become parallel one to the other, and so never meet to constitute a Tangent and Secant, at least properly so call'd. Hence Tables of Tangents proceed only to 89 Degrees, 59 Minutes. And as for Scales of Tangents, and also Secants, they are usually continued no farther than to about 70 or 75 Degrees; because, after that they extend to a vast Length, if the Scales be of any considerable Size, so as to be fit for Use. Which may be perceiv'd by Fig. 2, where the Scales are of a very small Size, as being design'd not so much for practical Use, as to shew only the Manner of Making such Scales. Such Scales, as are fit for Practice, are to be bought ready made of such as sell Mathematical Instruments,

B 4

be

be not deduced from Principles of Trigonometry, yet is of so great Use therein, (as well as in other Parts of the Mathematicks,) that it will be requisite to describe it here, especially, since it has not been afore describ'd. It is then call'd, a *Scale of equal Parts*, because it shows the Measure of any Line or Extent, apply'd thereto, or taken therefrom, in some Number of *equal Parts*, denoting either Inches, or Feet, or Yards, &c.

15.
A simple
or plain
Scale of
equal
Parts,
what.

It is usually distinguish'd into the *simple* or *plain* Scale, and the *diagonal* Scale. The *simple* or *plain* Scale, is no other than a right Line divided into any Number of equal Segments or greater Parts: One of which greater Parts, (*viz.* at either End of the said Line,) is sub-divided into Ten other lesser and equal Parts, as *Fig. 3*; So, that this Scale represents any two Degrees of decuple Proportion, *viz.* if the Sub-divisions of the Segment BA be taken to denote Units, then the other equal Segments CB, DC, &c. will denote Tens. If the aforesaid Sub-divisions denote Tens, then the Segments will denote Hundreds, &c. Hence, the Extent from C to 4 will denote either 14 or 140 (&c.) Inches, or Feet, or Yards, &c.

The *diagonal* Scale will be better apprehended by Fig. 4. than by Words. It thence appears to differ from the simple Scale principally in this, viz. that one of its extreme Segments (being like the simple Scale) subdivided into ten equal Parts, each of the said ten equal Parts, are again subdivided into ten other still less and proportional Particles, by ten right Lines obliquely crossing the Scale, which are the *Diagonals* of so many (11) Parallelograms; whence this Scale takes its Name. Hence, by the Divisions and Sub-divisions of this Scale, are represented three Degrees of decuple Pro-

A diagonal Scale what.

(11) This is illustrated, Fig. 5, which is divided after the same manner, as is the Segment KL of the diagonal Scale, Fig. 4; and has withal the Sides of each Parallelogram described by *pricks* Lines, so that the said Figure contains five Parallelograms, viz. ABCD, and CDEF, and EFGH, and GHIK, and IKLM; which are each crossed by Diagonals, viz. the first by the Diagonal GB, the second by the Diagonal ED, the third by the Diagonal GF, the fourth by the Diagonal IH, and the fifth by the Diagonal LR. And these Diagonals answer the right Lines obliquely crossing the Segment KL of the diagonal Scale, Fig. 4, and which divide each Part of the said Segment into less and proportional Particles, as is illustrated by Fig. 6. For the Lines *bk*, and *cl*, and *dm*, &c. being all parallel one to the other, hence (by Theorem 9, Chap. 1, of the Young Gentleman's Geometry) $ab :: bk :: ac :: cl :: ad :: dm :: ap :: en :: af :: fo$, &c. But $ab = po$, $ac = qz$, $ad = rz$, &c. therefore $bk = qz$, $cl = rz$, $dm = sz$, &c. And consequently, the Line *az* is divided by the Diagonal *an*, into ten lesser and proportional Parts, viz. *bk*, *cl*, &c.

portion,

portion. For Instance: If you would denote the Extent of 245 equal Parts, (*viz.* Inches or Feet, &c.) one Foot of your Compasses being placed in the middle or prick Line over-against 200, open the other Foot to that Point of the Subdivided Segment KL, wherein meet the two Lines mark'd, one with 40 on the Side of the Scale, the other with 5 on the Top of the Scale. That Extent of your Compasses will denote 245 equal Parts, (*viz.* Inches or Feet, &c.) according to the said Scale.

17.
Plain and
Spherical
Trigonome-
try, what.

Further, It is to be here observ'd, that *Trigonometry* is two-fold, *Plain* and *Spherical*. *Plain Trigonometry* is so call'd, because it teaches how to resolve any (*) plain (*i. e.* right-lin'd) Triangle: *Spherical Trigonometry* is so call'd, because it teaches how to resolve any *spherical* Triangle, *i. e.* any Triangle whose Sides are made by the Concurrence of Lines on a Spherical Surface, and are no other than the Arches of Circles. It will be sufficient to the (†) Design of this Treatise, to speak only of plain *Trigonometry*.

(*) Hence, by a *plain* Triangle is to be understood throughout this Treatise a *right-lin'd* Triangle,

(†) See the Preface.

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Lastly, The Solution of plain (as also of spherical) Triangles is two-fold, either by *Calculation*, i. e. Working by Numbers, to which are subservient the Tables of Sines and Tangents; or by *Protraction*, i. e. drawing Lines and Angles, to which are subservient the Scales of Chords, Sines, &c. of each in its Order; and first of the Solution of plain Triangles by Calculation;

18.
Calculati-
on and
Protracti-
on, what.

CHAP. II.

Of the Solution of plain Triangles by Calculation,

OF the six Trigonometrical Parts of a plain Triangle, viz. its three Sides, and three Angles, any three being given, excepting the three Angles alone, the rest may be found either by Calculation or Protraction. From the three Angles given by themselves, can be infer'd or found out, only the *Proportion* of the Sides, not the Sides themselves, or their respective determinate Lengths. For Instance: Supposing the three Angles of the Triangle BCD, Fig. 7, to be given, viz. B $27\frac{1}{2}$ Degrees, D $38\frac{1}{2}$ Degrees, and conse-

I.
In order to
resolve a
plain Tri-
angle, there
must be
always gi-
ven one
Side, and
why.
Fig. 7, &c
8.

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consequently, $C = 114\frac{1}{2}$ Degrees; from hence it may be known, that the Side $CD = \frac{1}{2}BD$, and the Side $CB = \frac{1}{2}BD$. But from hence can never be discover'd the determinate Length of BD , (or any other Side,) and consequently not of the Rest CB and CD . Namely, because $\frac{1}{2} = \frac{1}{2} = \frac{1}{2} = \frac{1}{2} = \frac{1}{2}$, &c. hence the Proportion of CD to BD will be the same, whether BD be 2 Inches (or Feet, &c.) and CD one; or BD 4 Inches, and CD 2; or BD 6 Inches, and CD 3; or BD 20 or 200 Inches, and CD 10 or 100, &c. That is in short, it can never be discover'd by the three Angles alone, whether the Triangle sought be BCD , Fig. 7, or BCD , Fig. 8, (or any other equiangular Triangle,) forasmuch as both these Triangles have the same Angles, and consequently their Sides alike proportional one to the other, though the Sides of the one are much longer than the Sides of the other. Wherefore, to determine the Length of the Sides sought, there must always be given one Side, or (which is the same) its determinate Length, and hereby will be determin'd the Length of each Side sought. Thus, the Side BD , (Fig. 7,) being given, whose Length according to the diagonal Scale, (Fig. 4.) is 324 (equal Parts, suppose) Inches; hence, it being found, that $CD = \frac{1}{2}BD$, and $CB = \frac{1}{2}BD$,

Trigonometry.

BD, thereby it is known, that $CD=162$ Inches, and $CB=216$ Inches. But, if the Side BD (Fig. 8,) be given, whose Length according to the same Scale is 135 (equal Parts, suppose) Inches, then in the same, Fig. 8, $CD=67\frac{1}{2}$ Inches, and $CB=45$ Inches.

It evidently appearing from what has been said, that, in order to resolve a plain Triangle, of the three Parts given, one must be always a Side; it hence follows, that all the Cases, that can be propos'd, are reducible in general to these Three, viz.

1. One Side and two Angles being given, to find the other two Sides, and the (*) third Angle: Or,
2. Two Sides and one Angle being given, to find the third Side, and the two other Angles: Or,
3. and lastly, All the three Sides being given, to find the three Angles.

These three general Cases are distinguish'd into a great Variety of particular Cases, (according to the particular Sides

2.
The Solution of plain Triangles reducible to three general Cases.

3.
All the particular Cases are contain'd in the two following Tables.

(*) Two Angles being given, the third may be known (without Trigonometry) by Corol. 1, Theorem 4, of the Young Gentleman's Geometry. And by the same Corollary, one Angle being given in Case 2, and one of the sought being found, the other sought is known. And so in Case 3, two of the Angles sought being found, the third sought is known.

and

and Angles given or sought,) which are all contain'd in the two following Tables. Whereof, the former contains all the particular Cases, that relate to the Solution of plain *rectangular* Triangles, and the latter contains all the particular Cases, that belong to the Solution of plain *obliquangular* Triangles.

4.
The literal
Symbols
of the se-
veral
Parts of a
plain Tri-
angle
Fig. 9, &
10.

In Reference to which Tables it is to be observ'd, that for Brevity's sake it is usual to denote the several Parts of a plain Triangle by *Letters*, instead of Words. In order whereto a rectangular Triangle is wont to be denoted by A, B, and C, so placed, as (*Fig. 9, viz.*) that A always denotes the right Angle, BA the Basis, CA the Cathetus or Perpendicular, which falling upon the Basis makes the right Angle; BC the Hypotenuse; B the Angle between the Basis and Hypotenuse, call'd in short, *the Angle at the Basis*; C the Angle between the Cathetus and Hypotenuse, call'd in short, *the Angle at the Cathetus*. And an obliquangular Triangle is wont to be denoted by B, C, and D, so placed, as (*Fig. 10, viz.*) that by a Cathetus CA, let fall from C, it may be divided into two Triangles, the Cathetus CA being a common Side to both Triangles. And then, as BD is esteem'd the Basis of the whole Triangle BCD, so BA and DA are the particular

particular Bases, and BC and DG the particular Hypotenuses of the two Triangles BCA and DCA. Hence, B and D denote the two Angles at the Basis BD of the whole Triangle BCD, whereof B is always the Angle opposite to the Side CD, and D the Angle opposite to the Side CB, as C is always the Angle opposite to the Basis BD.

It is likewise to be observ'd, that in the following Tables, the Letter *s* denotes a Sine, *t* a Tangent, and the Greek σ a Cosine. Thus, *Tab. I, Case 1*, *sB* denotes the Tangent of the Angle B. And *Case 3*, *sC* denotes the Sine of the Angle C. And *Tab. II, Case 16*, *sB* and *sD* denote the Cosines of the Angles B and D. Also note, that *Z* do's (in this Treatise, as in *Algebra*) denote the Sum of two Things, *X* their Difference. Lastly, This Character $\angle$ denotes an Angle, $\angle\angle$ two Angles; *l* a Leg or Side, *ll* two Legs or Sides. And consequently, *Zll* denotes the Sum of two Legs of a Triangle; *ZLL* the Sum of two Angles, &c.

It is also to be observ'd, that a right Angle being always 90 Degrees, hence it is put down, neither among the Parts *given*, nor the Parts *sought*, in the several Cases of *Tab. I*. As for the other two oblique Angles of a plain rectangular Triangle, they are both put down among the

5.
Other
Symbols
used in the
following
Tables.

6.
Some other
Observa-
tions in
Reference
to the two
following
Tables.

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the Parts given in each of the first six Cases in Tab. I, (not $(+)$ because it is necessary both the said Angles should be actually given, but) because one of them being given, the other is in effect given also, its Quantity being known (by Corol. 1, Theorem 4, of the *Young Gentleman's Geometry*,) to be the Complement of the given oblique Angle. On this and the like Accounts, some Tables are drawn up in a much more contracted or shorter Form, than the two which follow. But I judg'd it more agreeably to my Design, to have *all* the particular Cases *distinctly* set down: So, that the young Student may, both more readily find the Case propos'd to him; and also, having found it, may more readily perform the Calculation, having Nothing else to do, but to Work according to the Proportion, which answers to the Case propos'd.

(+) Hence it is said in the first six Cases of Table I, thus, viz. B or C, denoting, that if either be given, it is sufficient.

T A B.

TABLE

TABLE I.

Shewing the Solution of plain rectangular Triangles.

Cases.	Parts given.	Sought.	Proportions.
1	B or C. BA	CA	$R : CB :: BA : CA$
2	B or C. CA	BA	$R : CB :: CA : BA$
3	B or C. BA	BC	$C : R :: BA : BC$
4	B or C. CA	BC	$B : R :: CA : BC$
5	B or C. BC	BA	$R : C :: BC : BA$
6	B or C. BC	CA	$R : B :: BC : CA$
7	BA . CA	B	$BA : CA :: R : B$
8	BA . CA	C	$CA : BA :: R : C$
9	BC . CA	B	$BC : R :: CA : B$
10	BC . BA	C	$BC : R :: BA : C$
11	BA . CA	BC	$CA : B :: BA : BC$; & then $AC : BC :: R : BC$
12	BC . BA	CA	$BC : R :: BA : C$; & then $BC : BA :: R : CA$
13	BC . CA	BA	$BC : R :: CA : B$; & then $CB : CA :: R : BA$

C T A B

TABLE II.

Shewing the Solution of plain obliquangu-
lar Triangles.

Case	Given	Sought	Proportions.
1	BC. BD. D.	C	BC : BD :: sD : (II) sC
2	BC. BD. C.	D	BD : BC :: sC : sD
3	BC. CD. D.	B	BC : CD :: sD : sB
4	BC. CD. B.	D	CD : BC :: sB : sD
5	BD. CD. C.	B	BD : CD :: sC : sB
6	BD. CD. B.	C	CD : BD :: sB : sC
7	B.C.D. BC	BD	sD : BC :: sC : BD
8	B.C.D. BC	CD	sD : BC :: sB : CD
9	B.C.D. BD	BC	sC : BD :: sD : BC
10	B.C.D. BD	CD	sC : BD :: sB : CD
11	B.C.D. CD	BC	sB : CD :: sD : BC
12	B.C.D. CD	BD	sB : CD :: sC : BD

(II) It is to be noted, that in this Case it may be doubtful, whe-
ther the Angle sought C be Acute or Obtuse. The Reason of which
Doubtfulness arises from what is said, §. 10, Chap. 1. This happens
when two Sides being given, whereof one is the greatest Side, toge-
ther with the Angle opposite to the lesser of the given Sides, the An-
gle opposite to the greater of the given Sides is demanded. And
in this Case, the Doubtfulness can't be better taken away, than by Pro-
tracting the Triangle; as is shewn, Chap. 3.

The Use of the foregoing Tables

Calc.	Given	Sought	Propositions.
13	BC. BD. B	C or D	$\frac{BC+BD}{2} : \frac{BC-BD}{2} :: \frac{D+C}{2} : \frac{D-C}{2}$ Then $\frac{D+C}{2} = \frac{C+D}{2}$ and $\frac{D-C}{2} = \frac{C-D}{2}$
14	BC. CD. C	B or D	$\frac{BC+CD}{2} : \frac{BC-CD}{2} :: \frac{B+D}{2} : \frac{B-D}{2}$ Then $\frac{B+D}{2} = \frac{B+D}{2}$ and $\frac{B-D}{2} = \frac{B-D}{2}$
15	BD. CD. D	B or C	$\frac{BD+CD}{2} : \frac{BD-CD}{2} :: \frac{C+B}{2} : \frac{C-B}{2}$ Then $\frac{C+B}{2} = \frac{C+B}{2}$ and $\frac{C-B}{2} = \frac{C-B}{2}$
16	BC. CD. BD	B or D or C	B or D: DG :: DE: DE. Then DB-DE=2BA. And DB-BA=DA. Then or C: B :: BA: B, and CD: R :: DA: C. And Complement of B+D to 180=C.

...the Logarithm of 8 to 1
...Having found the three Angles
...that are to constitute the three Angles

Terms of the Golden Rule in the Method
...I then (according to the Method)
...the Golden Rule

(*) It is to be observ'd, that, in this and the like Cases, the Sum of the two Angles sought, C and D, is found by subtracting the Quantity of B, the Angle given, out of 180, according to Theorem 4, of the young Gentleman's Geometry.

(††) It is also to be observ'd in Reference to Case 13th, 14th, and 15th, that having found the three Angles B, C, and D, the third side not given in either Case may be found by some of the twelve foregoing Cases.

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appears
roge
the An
And
by Pro

C 2

The

Cafe

7.
The Use
of the fore-
going Ta-
bles illu-
strated, as
to artifi-
cial Sines,
&c.

The Use of the fore-going Tables shall be illustrated by one or two Examples. And first, supposing of the rectangular Triangle ABC, (Fig. 9.) I have the Side BA given, viz. 8 (II) Foot long, and the Angle B, viz. 36 Degrees, 52 Minutes, and it is requir'd to find the Side CA. I consult the fore-going Tables, and find that this is Case 1, of Tab. I, and consequently, that $R : \sin B :: BA : CA$, the Side requir'd. Hereupon I turn to my Table of artificial Sines, &c. whose Ray I find to be 10.000000, and the Tangent of 36 Degrees, 52 Minutes, to be 9.875010. Then in my Table of Logarithms, I find the Logarithm of 8 to be 0.903090. Having thus found the Numbers, that are to constitute the three first Terms of the Golden Rule in my Calculation, I then (according to the Method of Working the Golden Rule by Logarithms) add the 2d and 3d Terms, and out of the Sum subtract the 1st Term, and the Residue is the 4th

Tangent of B	}	9.875010
36 Degr. 52 Min.		0.903090
BA 8 f. long.		
Sum		10.778100
The Ray		10.000000
Residue		0.778100

(II) This Extent of BA in Fig. 9, answers to the diagonal Scale, Fig. 4, and so of BC.

Ter

(*)

Trigonometry.

Term of my Proportion, and so the Number sought, viz. 0.778100. I look for this Number in my Table of Logarithms, and (though I find not exactly the same Number, yet) I find one very near it, viz. 0.778151, the Logarithm of the Number 6. Wherefore, the Side requir'd CA is 6 Foot long very nearly, viz. wanting only $\frac{1}{10}$ of a Foot.

The Reason, why the fore-going Example is wrought by artificial rather than natural Numbers, is, because (as has been ^{8.} afore observ'd) Tables of artificial Sines, &c. are more easy to work by, and so are generally made Use of, and therefore usually adjoin'd to Books of Trigonometry. Whereas few Books have Tables of natural Sines, &c. Howsoever I shall here shew (for the Satisfaction of the more Curious) how natural Sines, &c. may be found by artificial Sines, and also, how the fore-going Example is to be wrought by natural Sines or Tangents, &c. when they are found.

If then you would have the natural Sine or Tangent of any Angle, and want a Table of them, but have a Table of artificial Ones; then look out the artificial Sine or Tangent in the Table, and

8.
The Use
of the Ta-
bles illu-
strated, as
to natural
Sines, &c.

(*) See the Second Note on §. 12, Chap. 1.

not much regarding the Characteristic thereof, see what Number answers to the other Part thereof in the Table of Logarithms, and that will shew you the natural Sine or Tangent desired. For Instance: Not regarding the Characteristic of the artificial Tangent (above-found of B, viz. 9.875010, I look in the Table of Logarithms for the other Part, viz. 875010; and the nearest to it, there may be found, is the Logarithm 875061, which answers to the Number 750, which therefore may be taken as the natural Tangent sought of the Angle B, the Difference being only .000051.

Having thus found the natural Tangent of B, if thereby you would find the Side CA requir'd; then you must place (as afore) the Terms according to the Direction answering to Case 1, Tab. and must work the Golden Rule, (as natural Numbers, i. e.) by multiplying the 2d and 3d Terms together, and dividing the Product by the 1st Term. The Quotient will be the Number Sought or CA, viz.

$$\begin{array}{l} \text{Ray. } (\dagger) \text{ Nat. Tang. BA. CA.} \\ 1000 : 750 :: 875061 : 675030 \end{array}$$

(†) The Ray always consists of an Unit, and so many Cyphers, as there are Figures in the (natural or artificial) Sine or Tangent.

Trigonometry

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For $750 \times 8 = 6000$, and $1000 \div 6000 = 6$.
 And thus the Length of the Side CA requir'd, hath been found to be 6 Foot by both Sort of Operations.

Again, of the fore-mention'd Triangle ABC, suppose CA and BA to be given, and BC to be requir'd. I find this to be Case 4, of Tab. I, and consequently, the Rule for finding BC to be this, viz. $\sin B : \sin A :: CA : BC$. Wherefore, $\sin B$ is to $\sin A$ as CA is to BC .

Another Example.

As artifi. Sine of B 36 Deg. 52 Min. 9.778119
 To the Ray 10.000000
 So CA 6 Foot long 0.778151
 To BC the Side requir'd (10 f.) 1.000032.

For $10.000000 + 0.778151 = 10.778151$;
 and $10.778151 - 9.778119 = 1.000032$,
 which is (but 1.000032 is e. is nothing different from 1000000) the Logarithm of the Number 10, which, therefore is the Measure of the Side requir'd BC. And thus having given the Side BA (= 8 f.) of the Triangle ABC, the Side CA has been found equal to 6 Feet, and BC to ten Feet; agreeable to what is observ'd in the Use of Theorem 12, of the Young Gentleman's Geometry; whence may be observ'd the Truth of trigonometrical, as well as geometrical Principles.

$R : BC :: \sin C : \sin A$
 $R : BA :: \sin B : \sin A$
 $R : CA :: \sin C : \sin A$

I pro-

10.
Of the four
Theorems, on
which plain
Trigonometry is
founded.

I proceed now to speak of the *fundamental Theorems of Trigonometry*, so called, because on them is founded the Solution of plain Triangles, in all the Variety of Cases contain'd in the two fore-going Tables. And these Theorems are four, on the first of which is founded, *Tab. I*, or the Solution of plain rectangular Triangles; and on the other three is founded, *Tab. II*, or the Solution of plain obliquangular Triangles.

THEOREM I

Whereon is founded the Solution of plain rectangular Triangles.

Fig. II.

In every plain rectangular Triangle ABC, if BC be the Ray, then BA is the Sine of the Angle C, and CA the Sine of the Angle B. If BA be the Ray, then BC is the Secant, and CA the Tangent of the Angle B. But, if CA be the Ray, then BC is the Secant, and BA the Tangent of the Angle C; as is illustrated

Fig. II.

Whence it follows,

1. $R : sB :: BC : CA$
2. $R : sC :: BC : BA$
3. $R : tB :: BA : CA$
4. $R : tC :: CA : BA$

And

Trigonometry.

And these four Proportions are the same with those appertaining to *Case 6*, 1, and 2, of *Tab. I.* and from these are deduced all the other Proportions, belonging to the several other Cases of *Tab. I.* as may be seen by comparing them together. And therefore it evidently appears, how on this fundamental Theorem 1, is founded *Tab. I.* Proceed now to Theorem 2.

THEOREM II.

Whereon is founded the Solution of plain obliquangular Triangles, when, there being given either all the Angles with one Side, or two Angles with the Side opposite to one of the said Angles, the Rest are sought.

In every plain Triangle, the Sides are proportional to the Sines of the opposite Angles; that is, $sB : DC :: sC : BD :: sD : BC$. For $\frac{BC}{2} : \frac{CD}{2} :: sD : sB$, and $\frac{BC}{2} : \frac{BD}{2} :: sD : sC$, and $\frac{CD}{2} : \frac{BD}{2} :: sB : sC$; as is illustrated, *Fig. 12.*

THE-

THEOREM III.

Whereon is founded the Solution of plain obliquangular Triangles, when, there being given two Sides with the Angle contain'd between them, the Rest are sought.

$$\frac{ZII}{XII} :: \frac{ZLLop}{XLLop}; \text{ that is}$$

in Words, as Half the Sum of the (Leg or) Sides given, is to Half the Difference of the Sides given; so is the Tangent of Half the Sum of the opposite Angles sought, to the Tangent of Half the Difference of the opposite Angles sought. That is, in Fig. 13, $GE : BE :: GH : FH$.

Fig. 13.

Demonstration. In the Triangle BCD Fig. 13, let the Legs or Sides given be BD and BC. Draw $BG = BC$, and there will be $GE = \frac{ZII}{2}$, and $BE = \frac{XII}{2}$ and the (||) extern Angle $GBC = BCD + BDC$, the two intern and opposite An

(||) By Theorem 4, Chap. 1, of the Young Gentleman's Geometry.

gles of the Triangle BCD. Then draw CG, and after that draw EH, and also BF parallel to CD; whence will arise the Angle (*) GBF = BDC, and (†) FBC = BCD. Then bisect CG by BH, and there will arise the Angle (‡) GBH = HBC. But GBH + HBC = GBC = GBF + FBC = BDC + BCD, i. e. $\angle Lopp$. And therefore, (because GBH = HBC, and GBH + HBC = GBC,) $GBH = \frac{\angle Lopp}{2}$;

and so GH the Tangent of $\frac{\angle Lopp}{2}$. Then make the Angle HBK = FBH. Now, because (as afore has been shewn) the Angle GBH = HBC, therefore GBH — FBH = HBC — HBK, i. e. GBF = KBC. Wherefore FBC (BCD) — KBC (GBF or BDC) = FBK or $\angle Lopp$. Wherefore FBH = $\frac{\angle Lopp}{2}$; and so FH is the Tangent of $\frac{\angle Lopp}{2}$.

But now GE : BE :: GH : IH,

that is, $\frac{\angle Lopp}{2} : \frac{\angle Lopp}{2} :: t, \frac{\angle Lopp}{2} : t, \frac{\angle Lopp}{2}$.

(*) By Theorem 3, Chap. 1, of the Young Gentleman's Geometry.

(†) By Corol. 2, Theorem 3, Chap. 1, of the Young Gentleman's Geometry.

(‡) By Theorem 5, Chap. 1, of the Young Gentleman's Geometry.

THEOREM IV.

On which is founded the Solution of plain obliquangular Triangles, when, the three Sides being given, the Angles are sought.

Fig. 14.

$DB : DG :: DF : DE$, that is in Words. The greatest Side DB of any plain Triangle, is to the Sum DG of the other two Sides, as is the Difference DF of those Sides, to that Segment DE of the greatest Side, which being taken away, the Cathetus CA will bisect the remaining Segment EB of the greatest Side.

Demonstration. By Prop. 36, 3 Euclid. $DG \times DF = DT^2 = DB \times DE$. Wherefore, by Prop. 15, 6 Euclid, $DB : DG :: DF : DE$.

From the three last Theorems is deduced, Tab. II, or the Solution of plain obliquangular Triangles, in all the Variety of Cases that can be propos'd. Nay, the said Theorems may serve for the Resolution of all plain Triangles whatever Rectangular as well as Obliquangular. But forasmuch as the first Theorem doth suffice to shew the Solution of plain rectangular Triangles, and that after a more easy Manner in some Cases, hence

Trigonometry.

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the three last Theorems are wont to be restrain'd to the Solution only of plain obliquangular Triangles. And consequently, *Tab. II*, is accommodated only to obliquangular Triangles. Of which Table the twelve first Cases are founded on the 2d Theorem, the three next Cases, (*viz.* 13th, 14th, and 15th,) on the 3d Theorem; and Case the 16th or last on the 4th and last Theorem. And thus much for the Solution of plain Triangles by Calculation.

C H A P. III.

Of the Solution of plain Triangles by Protraction.

HERE are two Things to be shewn; ^{I.} **1st**, How to *protract* or describe any plain Triangle requir'd. ^{Two Things to be here taught.} **2^{dly}**, How to *resolve* the said Triangle, when it is protracted; *i. e.* how to find the Measure of the unknown Angles or Sides in the said Triangle, when protracted.

2. Protraction is either of some Side, or of some Angle. A given Side is protracted by drawing a right Line BC, *Fig.* ^{First, how to protract any given Side.} 15. taken off from the (simple or diagonal) *Fig. 15.*

nal) Scale of equal Parts, at such Length, as to contain the same Number of equal Parts according to the Scale, as is the Number of Inches or Feet, &c. in the Side given, viz. 254.

3.
Secondly,
how to
protract
any given
Angle.

A given Angle B=48 Degrees, is protracted, by (taking a Chord of 60 Degrees for your Ray, i. e. by) opening your Compasses to the Extent of 60 Degrees on your Scale of Chords, and then one Foot being fastened on one End B of the given Side BC, drawing with the other Foot the Arch CA; and on the said Arch setting off from A to E, the Extent of 48 Degrees taken from your Scale of Chords; and after that drawing the right Line BD.

4.
A plain
Triangle
how to be
describ'd,
when the
three Sides
are given,
and no An-
gle.

After this manner is any given Side and Angle to be protracted, and so any plain Triangle to be describ'd, when either one Side and two Angles, or two Sides and one Angle are given. But, if the three Parts given be the three Sides; then the Triangle is to be describ'd, as is shewn Chap. 2, Problem 2, Case 1st, or 2d, or 3d, of the Young Gentleman's Geometry.

5.
How to
find the
Measure of
a Side not
given.

The Triangle BCD; (Fig. 15,) being protracted, the Measure of any Side not given, is found, by applying the Extent thereof with your Compasses to your (simple or diagonal) Scale of equal Parts, and so finding how many such equal Parts

are contained in the said Side. which equal Parts are to be esteemed in Inches, or Feet, or Yards, accordingly as the Measure of the given Side is denoted by Inches, or Feet, or Yards, &c. Thus, supposing BC to be 254 Feet long, CD shall be 198 Feet, and BD 204 Feet.

In like Manner, the said Triangle being protracted, the Measure of any Angle C or D not given, is found, by opening your Compass to the Extent of 60 Degrees on your Scale of Chords, and then fixing one Foot on the Point of the Angle sought, and making an Arch from one Leg to the other of the said Angle. The Extent of the Arch apply'd to your Scale of Chords, will shew the Degrees and the respective Angle. Thus, Fig. 15, the Extent of the Arch FG, shews C to be an Angle of 52 Degrees; and the Extent of the Arch EG, shews D to be an Angle of 80 Degrees.

It remains to be observed, that the Solution of plain Triangles by Protraction, is founded on Theorem 9, Chap. 1, of the young Gentleman's Geometry. Namely, because the protracted Triangle is equiangular to the real Triangle, (i. e. the triangular Ground, or the like,) therefore, the Sides of that have the same proportion one to the other, as have the Sides

6.

How to find the Measure of an Angle not given.

7.

The Solution of plain Triangles by Protraction, on what founded.

Sides of this ; albeit those are in a manner infinitely less than these.

8.

*The Use of
plain Tri-
gonome-
try ap-
pears in
taking
Heights
and Di-
stances,
&c.*

And thus having shewn, how to solve any plain Triangle, either by Calculation or Protraction ; I proceed now to illustrate the great Usefulness of plain Trigonometry, in taking Heights and Distances, as also in Surveying and Fortification.

CHAP. IV.

Of Taking the Altitude or Height of an Object, viz. Tower, Tree, &c.

I.

*The Heights
of an Ob-
ject, what.*

IT is to be remember'd, that (according to Definition 42, Chap. 1. of the *Young Gentleman's Geometry*.) the Altitude or Height of an Object, viz. Tower, Tree, and the (*) like, is measur'd by a Perpendicular from its Top to its Bottom. Thus, the Height of the Tower, Fig. 16, and of the Tree, Fig. 17, is denoted

(*) For as to the Height of the Sun, or any other Celestial Light, that is computed by its Distance above the Horizon on a vertical Circle : Of which in *Trigonometry*.

by the Perpendicular CA; and so
in all other such Cases through this Treas-

For the Line CA of Altitude, and the
Line BA of Distance, (*viz.* between the
Observer B, and the Foot of the Object
,) and the Line BC of Vision do always
constitute the three Sides of a rectangular
Triangle ABC. Wherein the Height of
the Object is the Cathetus or Perpendi-
cular, and therefore, (according to the
receiv'd Method of denoting the several
parts of a rectangular Triangle in *Trigo-*
metry.) is aptly denoted by CA. In
like manner, the Distance of the Ob-
server from the Object, making always
the Basis, is aptly denoted by BA; and
the Line of Vision, making always the
Hypotenuse, is aptly denoted by BC.
And so as to the several Angles, A de-
notes the right Angle between the Line
of Altitude and the Basis, B the Angle
between the Basis and Hypotenuse, which
may be call'd, *the Angle of Altitude*, be-
cause the Altitude of the Object is al-
ways either (+) its Sine or Tangent; and
C will denote the remaining Angle

The Sym-
bols made
Use of in
taking
Heights.

(+) Namely, if BA be taken for the Ray, then CA is
the Tangent of B; but if BC be taken for the Ray,
then CA is the Sine of B.

D between

between the Lines of Vision and Altitude.

3.
How to
take the
Angle of
Altitude.

The best Instrument for taking the Angle of Altitude is the Quadrant, then commonly distinguish'd by the Name of *the Quadrant of Altitude*; by which it is done thus. Hold your Quadrant upright, so as the String may have Liberty to slip to either Edge, and move the Quadrant so held, till through the Sight you see the Top of the Object, whose Height you would take. Then the Degrees, intercepted between the Beginning of the Quadrant and the String, are the Degrees of the Angle of Altitude; namely, of the Altitude of the Object above your Eye. Wherefore, if you stand upright, when you take the Angle of Altitude, to the Altitude found by the said Angle of Altitude, there must be always added the Height of your Eye above the Ground, to know the Altitude required of the Object.

4.
An accessible
and inaccessible
Height,
what.

If one may come to measure from the Place B of Observation, to the Foot of the Object, (*i. e.* to the very Bottom of the Perpendicular CA,) then it is call'd an *accessible* Height. But, if any Thing hinders from coming to A the Foot of the Object, then it is call'd an *inaccessible* Height.

PROBLEM I.

To find an accessible Height.

Measure your Line BA of Distance, and find the Measure of the Angle B by your Quadrant. These two being known, CA is found by Tab. i, Case 1, viz. $R : \tan B :: BA : CA$. For Instance: suppose $BA = 347$ Feet, and $B = 35$ Degrees. Wherefore,

the Ray	10,000000	
the Logarithm of BA 347 Feet	2.540329	} Add
the artificial Tangent of B 35 Degr.	9.845227	
To the Logarithm of the Side sought CA 243 Feet very near.	2.385556	
	10.000000	Subst.
	2.385556	Residue.

If you would find the Height sought CA by Protraction, work thus. Draw according to Chap. 3, §. 2. the Line of Distance $BA = 347$ (equal Parts or) Feet. Then, (by Chap. 3, §. 3.) make the Angle $B = 35$, and the Angle $A = 90$ Degrees, or a right Angle. Then draw the Sides BC and CA, till they meet in C. Apply CA to your diagonal scale, and it will be equal to 243 (equal parts thereof, or) Feet.

D 2

To

7.

Some o-
ther Me-
thods of
taking ac-
cessible
Heights.

To the Method of taking Heights by Protraction, may be referr'd the Method of taking Heights by a Staff, or a Bowl of Water, or the like. Forasmuch as by the Help of the Staff or Bowl of Water (&c.) there is as it were protracted a Triangle, equiangular to the Triangle made by the three Lines of Vision, Distance, and of the Altitude sought. Namely, in Fig. 17, or 18, the Triangle *bac*, is equiangular to the Triangle BAC, (as shall be shewn by and by.) and therefore, the Measure of the Sides *ba* and *ca* being known, as also of *BA* thereby is found (according to the Rule of Proportion) *CA* the Altitude sought. For, (according to Theorem 9, Chap. of the Young Gentleman's Geometry,) $ba :: BA : CA$.

8.

Accessible
Heights
may be ta-
ken by a
Staff two
Ways.

Now the Way to find the Altitude of an Object by a Staff, is two-fold, either by the Staff and its Shade, when the Sun shines; or else by the Staff alone, at any Time, or whether the Sun shines or Not.

9.

To take an
accessible
Height by
a Staff and
its Sha-
dow.

Fig. 17.

To find the Altitude of an Object by a Staff and its Shade, work thus. At the End of the Shadow cast by the Top of the Object, set up your Staff *ca* perpendicularly, (as Fig. 17,) and measure the End *b* of the Shadow made by your Staff. For, as $ba :: ca :: BA : CA$,

Trigonometry.

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As the Length of the Staff's Shadow, is
to the Height of the Staff; so is the
Length of the Object's Shadow, to the
Height of the Object. For Instance:
Suppose your Staff ca to be three Foot
long, or just a Yard, and its Shadow bc
to be nine Foot long, and the Shadow
of the Object to be 60 Foot long;
Then the Height of the Object will be
twenty Foot. For $9 : 3 :: 60 : 20$. This
Method depends (as is afore said) on
Theorem 9, Chap. 1, of my Geometry, or)
On the Triangles bac , and BAC being
mutually equiangular. And that they
are so, is thus shewn, *viz.* the Staff ca
being erected perpendicularly, therefore
the Angle a is a right Angle, and so e-
qual to A . Also, because the (II) Ray
of the Sun, (or, which comes to the
same, the Extremity of the shaded Air)
is always parallel to the other Ray
 BC , therefore, (by *Theorem 3, Chap. 1,*
of my Geometry) the Angle $b=B$, and
consequently, the Angle $c=C$; and so

(II) Although the Rays of the Sun, as proceeding from
the Sun as their Center, are in Strictness, not parallel, yet
by Reason of their immense Length or Distance from
the Sun, wherein they concur, their Obliquity is not dis-
cernible in such Cases, but they may be esteem'd as par-
allel; especially as to such small Segments or Portions of
them as are herein concern'd.

D 3

the

The Young Gentleman's

the Triangle abc , equiangular to the Triangle ABC .

10.

To take an
accessible
Height by
a Staff a-
lone.

Fig. 18.

If the Sun do's not shine, then you may nevertheless find the Height of the Object by your Staff alone, thus. Having set up (as afore) your Staff ca perpendicularly, go backward till you can see the top C of your Object, in a Line with the top c of your Staff, as is represented, Fig. 18, by the Line bc or Bc . Then (*) $ba : ca :: BA$ (or ba) : CA that is, as the Distance ba of the Place where you saw the Top C of the Object and the Top c of your Staff in one Line bc (or Bc) from the Place a of your Staff is to the Height ca of the Staff; so is the Distance of the former Place (b or B) from the Foot A of the Object, to the Height CA of the Object.

11.

To take an
accessible
Height by
a Dish or
Bowl of
Water.

Fig. 19.

If you would for Curiosity Sake know how to find the Height of an Object by a Bowl or Dish of Water, it is done thus. Go backward from the Bowl, till standing upright, you can see the Top C of the Object in the Water. Then $ba : ca :: BA : CA$, i. e. as is the Distance ba of an

(*) For here also bca and BCA are equiangular Triangles. For CA and ca being both Perpendiculars, are therefore Parallel. And consequently, (by Theor. 4. Chap. 1. of my Geometry,) the Angle $\angle C$, as well as $\angle A$ and the Angle B or b is common to both Triangles.

you

Trigonometry.

our Station A from $(\dagger)$ the Bowl B , to
our own Height ca . as far as to your
eyes; so is the Distance BA of the Foot
of the Object, to the Height CA of
the Object. For, according to that prin-
cipal Theorem of Catoptricks, the Angle
of Reflexion Pbc , is equal to the Angle
of Incidence PBC . And therefore, the
angle $abc (= 1 \text{ Right} - Pbc = 1 \text{ Right} -$
 $PBC) = ABC$. And the Angle $A = a$,
because both Right; and therefore, the
remaining Angles C and c are equal;
and so the Triangles ABC and abc equi-
angular.

Lastly, There is one Way more to take
an accessible Height, which I shall here
mention by Reason of its easiness and
expediteness, when it may be us'd. It
is thus. Go towards or from your ob-
ject CA , if you have Room, 'till the
sight of your Quadrant falls just on the
45th Degree. Then the Height CA of
your Object, will be equal to BA the
Distance between your Place B , and the
Foot A of the Object. For the Angles
 B and C will be equal, (*viz.* each 45
degrees,) and therefore, the Triangle

20.

To take an
accessible
Height by
Quadrant
only.
Fig. 29.

(†) If you would be exact, your Distance, and the
Distance of the Object must be both taken from the
very Point of the Water, whereon you see the Top of
the Object,

D 4

ABC

The Young Gentleman's

ABC will be an Iſofceles; i. e. $BA = CA$ by Theorem 3, Corol. 2, of the Young Gentleman's Geometry.

PROBLEM II.

To find an inaccessible Height.

13.
By Calcula-
tion.
Fig. 21.

Take two Stations B and b lying in a direct Line with the Foot A of the Object. The Distance Bb between the two Stations, with the two Lines of Vision BC and bC, make an obliquangu-
Triangle BCb. Whose Angles are known, by taking the two Angles of Altitude CBA and CbA, in their respective Triangles BCA and bCA. For $180 - \text{Angle } CBA = \text{Angle } CBb$, and $180 - \text{Angle } CbA = \text{Angle } CBb$. The three Angles of the Triangle BCB being thus known, and the Distance Bb between the two Stations being me-
sur'd, the Side BC is found by Case 1. Tab. II, (viz. $sB : CD :: sD : BC$. For that is in Respect of the Notation of the several Sides of the Triangle BCB, Fig. 21.) $sBCb : Bb :: sCbB : BC$. But now BC is also the Hypotenuse of the rectangular Triangle ABC; and the Measure of BC being known, as also of the Angle CBA, (viz. $CBA = 180 - \text{Angle } CbA$) hence may be found CA the Height

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the Object, by Case 6, Tab. I. viz. R;
 $B :: BC : CA.$

For Instance : I would know the
 Height of the Church-Steeple, Fig. 21,
 between A the Bottom of which, and b
 the Place where I am, runs a River, so
 that it is an *inaccessible* Height. Where-
 fore, by my Quadrant, I take the Angle
 bA of Altitude at my Station b, which
 I find to be 27 $\frac{1}{2}$ Degrees. Then measur-
 ing in a straight Line from b to B my
 second Station, (which I find to be 92.7
 foot,) I take the Angle CBA of Altitude
 again at my second Station B, and find
 it there to be 52 $\frac{1}{2}$ Degrees. Hence it
 follows, that the Angle CBb = 127 $\frac{1}{2}$ De-
 grees, (for $CBb = 180 - CBA$;) and al-
 so, that the Angle BCb = 25 Degrees,
 for $BCb = 180 - : CBb + CbB : = 180$
 $- 155$;) Having thus in the Triangle
 BCb the three Angles, and one Side Bb
 given, thereby is found the Side BC, by
 Case 11, Tab. II, Viz.

The Young Gentleman's

As the Sine of BCb 25 D. 30 M. 9.63398

To the Log. of Bb 92.7 Foot 1.96708

So the Sine of CbB 17 D. 30 M. 9.66440

To the Log. of BC somewhat above 9.63398

99.4 f. viz. 100 f. very nearly 1.99750

Having thus found the Measure of BC and having afore found the Angle CBA thereby is found CA the Height sought by Case 6. Tab. 1. viz.

As the Ray 10.00000

To the Log. of BC 100 2.00000

So the Sine of CBA 32 D. 30 M. 9.89946

To the Log. of CA 793 and some 1.90000

what more, viz. 80.3 very nearly 1.89946

I 4.

To take an
inaccessible
Height by
Protracti-
on.
Fig. 21.

If you would work by Protraction, you must proceed thus. Having (as afore) at the two Stations B and b , found the Angles of Altitude, viz. CbB and CBA and measur'd the Length of Bb , then draw a right Line Bb of as many Parts of the Scale, as the Measure of Bb is found to be of Feet (or Yards, &c.) At the two Points B and b make two Angles CBA and CbA equal to the Angle

Altitude taken by you at B and b.
 From C the Point, where CB and Cb in-
 terfect or cross one the other being
 drawn, let fall the Perpendicular CA to
 the Line of Distance Bb extended, if need
 be, 'till it meets with CA. The Perpen-
 dicular CA apply'd to the Scale of equal
 Parts will shew the Number of Parts, i. e.
 Feet or Yards, &c.

An inaccessible Height may also be
 found by the Help of a Staff, and its
 Shade, thus. Set up the Staff ca perpen-
 dicularly, and mark the End b of its Sha-
 dow Fig. 23; and at the very same time
 mark the End B of the Shade of the inac-
 cessible Object CA Fig. 22. Then three
 or four Hours after mark again the End d
 of the Staff's Shadow, and also the End D
 of the Shadow of the Inaccessible Object.
 Then measure the Distance between the
 two mark'd Ends b and d of the Shade of
 the Staff, and also between the two
 mark'd Ends B and D of the Shade of the
 inaccessible Object. As bd to ca, so BD
 to CA, i. e. As the Distance between the
 two different Ends of the Staff's Shadow,
 to the Height of the Staff; so will the
 Distance between the two different Ends
 of the Object's Shadow, be to the Height
 of the Object. For (by Theor. 9. Chap. 1.
 of my Geom.) $da : ca :: DA : CA$. Where-
 fore

15.
 To take an
 inaccessible
 Height by
 a Staff and
 its Sha-
 dow.
 Fig. 22,
 & 23.

fore da — (†) $ba : ca :: DA$ — (†) BA
 CA i. e. $bd : ca :: BD : CA$.

16.
 To take an
 inaccessible
 Height,
 when there
 is not
 Room to
 take two
 Stations
 on the
 Ground.

Fig. 24.

If it should happen, that you have no Room to take two Stations, as Fig. 24. then an inaccessible Height may be found thus. First take the Arch CBA of Altitude on the Ground B; and then go to the Top of the House (or Tree) where you are, and there take the Angle CDB. Draw an indeterminate Line BA, and thereon at B erect the Perpendicular BD of an equal Length with the Height of the House DB, (which is suppos'd to be known,) and thereon at D make an Angle CDB equal to the Angle taken on the Top of the House, and at B make an Angle CBA equal to the Angle of Altitude taken on the Ground. Then extend BA and DC till they meet in C. A Perpendicular CA, let fall from C upon the indeterminate Line BA, being apply'd to the Scale of equal Parts, will shew the Height of the Object CA.

(††) For as the Lines da and DA are proportional to the fore-mention'd Theorem, so will their Parts ba and BA ; because, the Shade of the Staff will be proportionably lengthened or shortened, as is the Shade of the Object.

PROBLEM III.

To measure the Height of an Object, which stands on the Top of another Object.

I would know the Height of the Spire *Fig. 25,*
above the Tower *A*. Find the whole *& 26.*
Height *CA* (by *Prob. 1.* if *A* be accessible,
Fig. 24; if inaccessible, as *Fig. 25*, then
by *Probl. 2.*) Then find the Height *Ad*
(or *ca*) of the Tower alone, (as afore by
Probl. 1. or 2.) Then *CA—Ad* (or *ca*)
=Cd the Height of the Spire.

PROBLEM IV.

To find the Height of an Hill or Mountain.

This may be done in some Manner by *Fig. 27.*
Probl. 2. But because the Tops of Hills
or Mountains, if of any considerable
Height, do appear higher than really
they are, by reason of the Refraction of
the Ray of Vision; therefore there is an-
other more exact Method to find the
Height of Hills and Mountains, by the
Help of an Instrument called the *Brazen T*,
from

from its resembling the Letter of the Name, as may be seen *Fig. 27.* For the Instrument being plac'd between two Staves (or Spikes, divided into a certain Number of Feet, and those subdivided into Inches) thereby may be observ'd (at least by the Help of slipping Marks to be mov'd upwards or downwards) what Number of Feet and Inches the Hill rises or the Ascent increases at all the several Positions of the said Staves, from the Bottom to the Top of the Hill or Mountain. And consequently, by adding together the several Feet and Inches which at the several Positions of the two Staves, have been observ'd to be contain'd, between the horizontal or level Lines, thence will arise the Sum of all the Feet and Inches from the Bottom to the Top of the Hill, and so the Height sought. Thus the Height CA of the Hill or Mountain *Fig. 27.* is equal to the Sum of $ab+cd+ef+gh$. And this Method is called *Cultellation*:

CHAP. V.

Taking the Distance between two Objects.

In taking Distances (as well as Heights)

there are in general two different Cases.

For either we may come to (*) One,

Neither of the Two Objects, whose

Distance one from the other we would

take.

The Angle which is opposite to the

Side of Distance (between the two Ob-

jects) may be call'd, the *Angle of Dis-*

tance, and is here denoted by the Letter

A: Forasmuch as the Triangles arising in

taking Distances are generally obliquan-

gular Triangles.

The most commodious Instrument for

taking Angles of Distance is the *Theodo-*

lite or *Circumferentor*, i. e. a Brass Circle

divided into 360 Degrees, and fitted with

1.
Two different general Cases in taking Distances.

2.
The Angle of Distance, what.

3.
How to take the Angle of Distance.

(*) As for the third Case, viz. wherein both the Objects, whose Distance is requir'd, may be come at, that need not stand in need of Trigonometry to find the Distance, because it may be measur'd (without any more) by a Chain or other long Measure.

See Fig.
40, of
Geometry.

four Sights. For the Sights being mov'd, as that you can through two of them (lying in a strait Line AB) see one, A, of the Objects, and through the other two (on the Line DE) see the other, E, of the Objects, the Angle ACE will be the Angle of Distance; whose Measure will be the Degrees intercepted between C and CE; and are always equal to the Degrees between CD and CB, because the Angles ACE and DCB are vertical Angles, and consequently equal. Whence BCD as well as ACE may be esteem'd the Angle of Distance.

P R O B L E M I.

To take the Distance between two Objects, when One of the Objects is accessible.

4.
By Calculation.
Fig. 28.

I would know the Distance of the Object B (Fig. 28.) from the Object C, one, B, of which Objects is accessible, but the other, C, is not. On one Side of B choose a Station D, at a (†) considerable Distance from B. The Line BC of D

(†) Note, That the greater the Distance BD is between the accessible Object B, and the Station D, much more exact will the Operation be.

sta

Trigonometry.

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Distance between the two Objects B and C, the Lines BD and CD of Distance between each Object and my Station, make an obliquangular Triangle BCD. Now the Angles CBD and BDC being found by the theodolite, and consequently the Angle B being known, (*viz.* $DCB = 180 - D + BDC$) and the Side BD being asur'd, hereby may be found BC the Distance requir'd between the two Objects B and C, by *Tab. II, Case 9, viz.* $BD :: sD : BC$.

For Instance: Suppose BD, the Distance my Station D from the accessible Object B, to be one hundred and four Yards; the Angle BDC = 86 Degt. and the Angle DBC = 63 Degr. and consequently Angle BCD = 31 Degr. It follows, according to the foremention'd *Case 9, . II, that*

*5.
An Example.*

the Sine of C 31 Deg.	9.711839
the Logarithm of BD 104 Yards	2.017033
the Sine of D 86 Deg.	9.999404
	12.016437
	9.711839
the Log. of BC 202 very nearly	2.304598

If you would take the Distance by Proportion, you must work thus. Draw a Line containing 104 equal Parts upon your

6.
By Protraction.
Fig. 28.

E

dia-

diagonal Scale, equal to the Number Yards found upon measuring BD. then at one End B describe the Angle equal to its Measure of 63 Degrees for by the Theodolite; and likewise at other End D describe the Angle D = Deg. as found by the Theodolite. Then draw the Lines BC and DC, till they meet in C, the Line BC apply'd to your diagonal Scale, will shew the Distance of the two Objects B and C, viz. about 2 Yards.

7.
By a Chain
or Pole
only.
Fig. 29.

If you have no Theodolite, or like Instrument by you, the Distance may be taken only by a Chain or Pole (or the like) thus. Measure with Chain the Distance BD between the accessible Object B and your Station which your Station choose so in this Case as that it may be (as near as you guess) at an equal Distance with B from the inaccessible Object C. Then in the Lines of Vision DC and BC mark out two Points *d* and *b*, and measure with Chain the several Lines DB, B*b*, *b**d*, and *d*B. Then protract a Trapezoid BD*b**d* of the same Sides; the two Sides B*b* and D*d* of which being produc'd, will meet in C, which will denote the Place of your inaccessible Object. And consequently the Line BC, being apply'd to the Scale of equal Parts, will thereon shew

Trigonometry.

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the Distance sought. For by measuring and protracting the Sides of the Trapezium $BDdb$, you do in effect find and protract the Angles B and D of the obliquangular Triangle BCD , as well as the Side D of the said Triangle. And therefore the protracted Triangle BCD is equiangular to the Triangle made by the Lines Vision at B and D , and the Line BD ; and consequently the Sides of the protracted Triangle are proportional to the Sides of the real Triangle, represented by the protracted one.

By this last Method may the Breadth of a River be taken. For if you suppose D to be one Bank of the River, and C denote a Point of the Bank on the other Side of the River; then the Distance between the Banks or Breadth of the River will be equal to BC . Where it is to be noted, that in this Method the Trapezium $BDdb$ may be taken or measur'd out, on either side of BD , viz. either towards the inaccessible Object C , or on the other Side of D , as you have Room or most Convenience.

The same may be performed also after this Manner. Set up a Staff perpendicularly on the Bank where you are, and thereon place a square Rule with its Angle downwards on the Head of the Staff. Move the square Rule, 'till the Line BA

8.

To take the Breadth of a River.

Fig. 29.

9.

To take the Breadth of a River, or any such like Distance, by a Staff and a Square-rule.

of Fig. 30.

of Vision from B a Point in the opposite Bank of the River, falls in directly with the upper Edge of one Side of the square Rule; and then from the Point C (where the upper Edges of the two Sides of the square Rule meet) draw, along the upper Edge of the other Side, a String, or Rope, or Chain, 'till it comes in a straight Line to the Ground at *b*. As (+) $bA : CA$ as $CA : BA$, *i. e.* As the Distance bA between the Point *b*, where the String came to the Ground, and the Foot A of your Staff, is to CA the Height of your Staff so is the Height CA of your Staff to the Distance BA of A (the Foot of your Staff) to the Bank where your Staff is, from the other Bank. And after the same Manner may any other Distance be taken where only one Object is inaccessible.

10.
To take
the Distance of
an Object
of Height,
as of a
Tower, &c.
Fig. 21,
or 22, &
23.

If the inaccessible Object be an Object of Height, *viz.* a Tower, or Tree, or like, then having found (by the Problem for taking an inaccessible Height) the Height CA of the said Object, and Angle B of Altitude, thereby may you find the Distance sought BA by Table Case 2; *viz.* $R : \tan C :: CA : BA$. For Angle B being known, thereby is the Angle C known; *viz.* $C = 90 - B$.

(+) Namely, by Corol. 1, Theorem 11, of the Young Gentleman's Geometry.

PROBLEM II.

To take the Distance between two Objects, when both are inaccessible.

Take your first Station D as you please; and on the Side of the former choose a second Station *d*, so as *Dd* may be parallel to BC as nearly as you can. Then with your Theodolite at D one of your Stations, take the Angles BDC and CD*d*, which together make the Angle BD*d*. Then at your other Station *d* take the Angles B*d*C and C*d*F, (the Mark F being up in a right Line with your two Stations D and *d*) which together make the Angle B*d*F. Now in the Triangle BD*d* the Angles BD*d* + DB*d* = B*d*F. Wherefore the Measure of the Angle B*d*F being found by the Theodolite, DB*d* = B*d*F - BD*d*. And therefore the stationary Distance D*d* being measur'd, $sDBd : Dd :: Dd : Bd$ by Case 12, Tab. II; viz. $sB : D :: sC : BD$. In like manner in the Triangle Cd*d*, the Angles CD*d* + DC*d* = C*d*F. Wherefore the Measure of C*d*F being found by the Theodolite, the Angle DC*d* = C*d*F - CD*d*. And therefore Case 12, Tab. II, $sDCd : Dd : sCDd :$

II.
By Calculation.
Fig. 31.

Cd. Wherefore the Angle CdB of the Triangle BCd being found afore, and the Angle $CBd = CDd$ found also afore, follows by *Case 12, Tab. II.* that $sCBd : Cd :: sCdB : BC$ the Distance sought.

12.
By Pro-
traction.
Fig. 31.

To take the like Distance by Protraction, you must work thus. Take (as afore) at your two Stations, D and d , the several Angles BDC and CDd , and CdB and BdD . Then having measur'd your ordinary Distance Dd , and protracted it, from one End D thereof protract its respective Angles BDC and CDd ; and on the other End d its respective Angles CdB and BdD . Draw out the several Sides of these Angles meet respectively, two BD and Bd in B , the other two, Cd and CD , in C . The Distance BC apply'd to your Scale of equal Parts, will give you the Distance sought.

P R O B L E M III.

*To take the Draught of a City,
Port, or the like.*

*Fig. 32,
& 33.*

This is done after the same Manner as is taken the Distance between two Objects, when both are inaccessible; it being no other than a Repetition of the former Operation, according to the Variety

Trigonometry.

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the remarkable Objects which you would delineate or describe in the Draught. For instance: Let A, B, C, D, E and F denote so many remarkable Buildings (*viz.* Churches, or Pillars, or other publick Edifices) in a City; or else let them denote so many Ships lying in a Port or Harbour. I take two Stations M and N at so considerable a Distance, as that the Line MN of the said Distance may be long enough to serve conveniently for the Basis of all the Triangles to be taken. Then at M placing the fixt Index of my theodolite in a right Line with MN, I take the moveable Index, as Occasion requires; and so take in order the several Angles MNA, MNB, MNC, &c. and so the last MNF. Then removing to my other Station N, and placing (as afore) the fixt Index of my Instrument in a Line with MN, I take the several Angles NMA, NMB, NMC, &c. Having done this, I (+) protract the Line MN of Distance between my two Stations M and N, taking from my Scale equal Parts the Line *mn* answerable to

(+) Having the Basis MN, and the two Angles at the Ends in each Triangle, the other Sides in each Triangle may be found by *Calculation*; but this Method being tedious, therefore *Protraction* is generally made Use of in this Case,

E 4

MN

MN. And then at the End *m* of the Line *mn*, I protract the Angles $\angle mna = \angle MNB$, $\angle mnb = \angle MNB$, $\angle mnc = \angle MNC$, &c. Likewise at the other End *n* of the Line *mn*, I protract the Angles $\angle nma = \angle NMA$, $\angle nmb = \angle NMB$, $\angle nmc = \angle NMC$, &c. The Lines of the several Angles being produced, will shew in the several Points of Intersection on *a*, *b*, *c*, &c. the respective Places of the several Objects A, B, C (&c.); and consequently their respective Distances both one from the other, and also from each of my Stations M and N; viz. Extents *ab*, or *ac*, &c. or *bc*, or &c. being apply'd to my Scale of equal Parts, give the Measure of the said Distances.

PROBLEM IV.

To find the Horizontal Line Length of an Hill or Mountain.

Fig. 34.

On the Top of the Hill, at C, set a Staff or Mark of an equal Height with your Eye (above the Ground) or with the Staff to which the Quadrant is fastened at B the Bottom of the Hill. Then move the Quadrant till you see the Top of the (Staff or) Mark at C, where

You'll take the Angle CBA. Then measure up the Side BC of the Hill. Being come up to C, measure the Level Cc on the Top of the Hill. Then measure the other Side bc of the Hill, and take the Angle cba, as you did afore the Angle CBA. Having done this, you may find the Length of the Hill, either by Calculation or Protraction.

If you work by Calculation, then in the Triangle ABC, having the Angle (CBA or) B, and the Hypotenuse BC, the Basis BA is found by *Case 5, Tab. I*, viz. $R : sC :: BC : CA$. In like manner, in the Triangle abc having the Angle b, and the Hypotenuse bc, the Basis ba is found by *Case 5, Tab. II*.

If you work by Protraction, then having protracted the Hypotenuse BC, and on one End B thereof protracted also the Angle (CBA or) B; from the End C of the Hypotenuse let fall a Perpendicular CA upon the other Leg of the Angle B. The Extent BA will be the Basis of the Triangle ABC. In like manner will be found ba, the Basis of the other Triangle abc.

Having thus found (either by Calculation or Protraction) the Measure of the two Bases BA and ba, these two added together, and also to the Length of the Level-Line Cc on the Top of the Hill, will give the total Measure of the horizontal

zontal Line or Length of the whole Hill Namely, Supposing $BA=160$ Yards or Chains, &c. and $ba=182$, and the Level-Line $Cc=122$, the total Measure of the Length of the Hill will be 464. And thus much for taking of Distances. • Proceed we next to Surveying.

C H A P. VI

Of Surveying or Measuring of Land.

I.
Surveying,
why e-
steem'd as
belonging
to Trigo-
nometry,

THE Surveying or Measuring of Land is esteem'd as belonging to Trigonometry, and so usually taught in Treatises of Trigonometry, because the Way formerly us'd to survey, was by taking the Angles and Sides of the several Triangles, into which any Spot or Tract of Ground may be divided; and then protracting the said Angles and Sides on Paper; and after that finding the Area or Content of the several Triangles so protracted.

2.
An Exam-
ple of the
old Me-
thod of
Surveying.

This Method is illustrated *Fig. 35* wherein the several Lines AB , BC , CD , &c. represent the several Sides or Hedges of a Ground; and the small Circle T represents the Place of the Theodo-

lite

te. Which being there plac'd, by turning the moveable Index thereof as Occasion requires, the several Angles ATB , BTC , CTD , &c. are taken. And then by measuring with a Chain (or the like) from T respectively to A , B , C (&c.) whereby is found the Length of the several Sides TA , TB , TC , TD , &c. of the several Triangles ATB , BTC , CTD , &c. And so by the Help of the Angles and Sides thus found, the other unknown Angles and Sides of the several Triangles may be found, (either by Calculation or Protraction;) and so the several Triangles may be protracted, and consequently the whole Ground, made up of the said Triangles. The Ground being thus protracted, its Area or Content is found (as has been observ'd in the Use of *Theor. 7, Chap. 1, of the Young Gentleman's Geometry*) by letting fall a Perpendicular from any Angle in each Triangle to its opposite Side, and multiplying the said opposite Side into half the Perpendicular, Thus the Content of the Triangle ATB may be found, by letting fall a Perpendicular from the Angle ABT to the Side AT , and multiplying the Side AT into half the said Perpendicular, (or, which comes to the same, by multiplying half the Side AT into the whole Perpendicular,) And in like manner may be found the

the Contents of the other several Triangles BTC, CTD (&c.) and consequently of the whole Ground ABCDEF.

3.
A better
Method of
Surveying.

But now forasmuch as the Finding of the Angles and Sides in each Triangle into which any Ground may be divided is only in order to protract the Triangles and so to find the Contents of the said Triangles when protracted; hence there is found out another and much more expedite and exact Way for finding the said Contents, (without being at the Trouble first to find the Angles and Sides of each Triangle, and then to protract them when found, viz.) by finding the Measure of the Perpendicular and its Basis in the Field or Ground it self. I shall therefore say no more of the old Method of Surveying, (which properly belongs to Trigonometry) but shall forthwith proceed to shew the other Method, as being much to be prefer'd before the old Method, for the Reasons already mention'd. And this Method I shall illustrate, by shewing how to survey thereby the same Ground ABCDEF.

4.
An Example.
Fig. 36.

And this Method is illustrated Fig. 36. For being come into the said Ground after viewing it, I perceive it may be conveniently distinguish'd into two Trapezium's ABCD and ADEF. Wherefore ha

ing set up (*) Marks at the several Angles or Corners of the Ground ABCDEF, the strait Line AD (suppos'd to be drawn between the Angles A and D) will divide the Ground into the two Trapezium's aforementioned. Then I (†) measure with my Chain from A to C for the Diagonal AC, whereby the Trapezium ABCD is distinguish'd into two Triangles ABC and ADC. And (either (||) as I go along measuring the Diagonal AC, or else after I have measur'd it) I find the Perpendiculars PB and PD by the Instrument for that Purpose; which from its Use and Shape

(*) These need be no other than Sticks, with some white Thing (as linnen Rags or Paper) fastened on their tops.

(†) In order to measure aright the Diagonal AC, (or any other straight Line or Side of your Ground,) with the Chain, you must take great Care, that you keep in a straight Line (as you go measuring) from A to C. In order whereto, he that carries the End of the Chain, must take Care that he that carries the Beginning of it, is always (at least that Hand of his which carries the Beginning of the Chain) directly between him and the mark C they are measuring to, every Time the Chain is laid down, And in order to prevent any Mistake as to the Number of Chains, it is advisable for him that goes first at the Head of every Chain's Length to thrust or fasten a Stick into the Ground, to be taken up by him that carries the End of the Chain. And so at last the Number of Sticks will shew the Number of whole Chains.

(||) It seems most advisable to measure the whole Diagonal first, because, hereby there is the less Danger of mistaking the Length of the Diagonal.

may

may be call'd the (*) *Perpendicular-Top*. In like manner I measure from A to E for the Diagonal AE, which distinguishes the Trapezium ADEF into two Triangles ADE and AEF. And then by my *Perpendicular-Top*, I find (one after the other) the two Perpendiculars PD and PE, and measure them with my Chain. And thus, the outer Sides or Hedges AB, BC, CD, DE, EF, FA, being all of them straight or right Lines, the Work is done in the Field; all that remains to be done being only to multiply half the Perpendiculars into their respective Diagonals, in order to know the Area or Content of each Triangle or Trapezium; and so of the whole Ground: Which may be done at Home, the Numbers of the Measure

(*) For this Instrument is best made in the Shape of a common Top, which Boys use to whip. It is best made of a dried Piece of Box or Pear-tree, that will bear three Inches, or three Inches and an half Diameter. This being turn'd flat on the upper Round, (with a Neck to fit to the Head of a Staff,) find the Center of the said upper Round or circular Surface, and thereon draw two or three concentric Circles, (as you see, *Fig. 38*.) divide the said Circles exactly into four equal Parts, (as in *Fig. 38*.) and then, with a Whipsaw very thin, saw by the Marks *a, b, c, d*, the two Lines *ac* and *bd* at right Angles pretty Deep. Thus, your Instrument is made; only in order to use it, it must be put on the Head of a Staff, as has been above intimated. To which End it is to be made with an Hole at the Bottom to slip on upon the Head of a Staff.

of the several Diagonals and Perpendiculars being set down in Writing, as soon as taken.

And here it must be shewn, how the Numbers, denoting the Number of whole Chains or of single Links, are to be multiplied in order to find the Content. The Chain then here suppos'd to be made use of by the Surveyor is that, which from its Contriver goes by the Name of *Gunter's Chain*, and which is best contrived for Surveying. It contains four Statute-Poles or Perches, each Perch containing sixteen Feet and an half, or five Yards and an half: so that the whole Chain is sixty-six Feet or twenty-two Yards long. The whole Chain is divided into an hundred equal Links, so that twenty-five Links are just a Pole or Perch. And for the more ready counting the Links, it is usual to distinguish every Ten with a Brass Plate, (or the like) so contriv'd as to shew, some way or other, whether it be the first, or second, or third, &c. Length i. e. the 10th, or 20th, or 30th, &c.) Link from either End; the 50th or Middle Link having a more remarkable Plate than the rest.

In measuring any Line or Extent by this Chain, regard need be had only to whole Chains or whole Links; which are to be writ down with a separating Note, (whc-

5.
Of Gunter's Chain, and the Way of Working by Numbers, to find the Content of a Ground by the said Chain.

(whether Full-point or Comma, or any other Mark) between the Chains and Links, (as is usual to do between Integers and Decimals,) viz. 6.35 denotes 6 Chains and 35 Links. If the Links be under 10, a Cypher must be prefix'd, viz. 7.09 denotes 7 Chains and 9 Links.

The Numbers denoting the Chains and Links being set down, as has been directed; to find the Content (of an exact Square or other rectangular Parallelogram) you multiply (*) the Length by the Breadth; but it seldom hap'ning that the Grounds are of such a Shape, hence it is generally requisite to distinguish your Ground into Trapeziums, as has been before shewn, and then to find the Content you multiply the Diagonal by (†) half the Perpendicular, (or (‡) the like) and from the Product cut off five Figures (accounting Cyphers for such,) reckoning from the right Hand, with a Dash

(*) Agreeably to what has been taught in *Defin. 4 Chap. 1, of the Young Gentleman's Geometry.*

(†) Agreeably to what has been taught in the *Use Theorem 7, Chap. 1, of the Young Gentleman's Geometry.*

(‡) Namely, the Product will be the same, whether you multiply the whole Diagonal (or Basis) by Half the Perpendicular, or the whole Perpendicular by Half the Diagonal, or the whole Diagonal by the whole Perpendicular; and take Half the said Product for the Product sought.

ur Pen : So that the Figures to the left
and denote the Acres. If the five Figures cut off to the right
and were not all Cyphers, multiply
them by 4 ; and from the Product cut
again five Figures towards the right
end, and the rest will denote Roods or
quarters of an Acre.

Lastly, if among the five Figures of the
Product, cut off towards the right
end, there be any Figures besides Cy-
phers, multiply all the five Figures by
4. From the Product cut off again five
Figures to the right Hand ; and those of
the left Hand will denote square Perches
or Poles. I shall now illustrate the fore-
going Rules by some Examples.

Suppose then in Fig. 36, the Diagonal
to be just 7 Chains long, and the Per-
pendicular PF to be 2 Chains and 88
Links, and the other short Perpendicular
to be 60 Links. I, (+) add the two
perpendiculars together, and the Sum of
them makes 3 Chains and 48 Links.

fin. 4

Use

For this is the most expedite Way, hereby ha-
ving the Trouble of two distinct Multiplications,
+ PF by 700, and then of + pD.

Half of
Perpe
Produ

F

Then

you

Then the Half of the said Sum of my Perpendiculars, viz. 174, I multiply by the whole of my Diagonal (¶) 700. I cut off the five Figures to the right Hand, and the remaining 1 denotes one Acre.

Then I multiply the five Figures by 4, and the Product, (viz. 218000) 87200, not amounting to above five figures, I perceive the Trapezium above does not contain a full Rood (or Quarter of an Acre) above the whole Acre before.

Therefore I multiply again the Product 87200 by 40, and cutting off again the five Figures to the right Hand in this third Product, the two remaining Figures 34 denote 34 square Perches or Poles. Which wants almost six square Perches to a Rood, or Quarter of an Acre, this containing 840 square Perches. For a full Acre contains 160 square Perches.

(¶) I choose my Diagonal for the Multiplier, it being 700, I need multiply only by the 7, and to the Product thereof add the two Cyphers.

Upon the Whole therefore I find, that
 the Trapezium AB EF contains one Acre,
 and a Quarter of an Acre over, wanting
 square Perches. I proceed then to find
 the Content of the other Trapezium
 BCD; whose Diameter AC, suppose
 be 5 Chains and 15 Links; the Perpen-
 dicular PB to be 1 Chain and 67 Links;
 and the other Perpendicular PD to be 1
 Chain and 89 Links. Where-
 fore I multiply the Diagonal 515
 by Half the Sum of the 175
 Perpendiculars, viz. 175 1 2575
 and the Product not arising to 3605
 above five Figures, I perceive. 515
 that the said Trapezium does 90125
 contain a Whole Acre.

Then I multiply the Product found by
 and from the second Pro-
 duct cutting off five Figures to 90125
 the right Hand, there remains 4
 the Figure 9, which denotes the
 contents of the Trapezium to 360500
 3 Rods or three Quarters of
 Acre, and somewhat more.

I proceed therefore to find what more
 is, which I do by multiplying the 5 Fi-
 gures cut off by 40. From
 the third Product I cut off 4
 in the five Figures to the 40
 right Hand, and the remain-
 2420000
 24 denote so many square

F 2

Perches;

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Perches; which is a little above Half Quarter of an Acre. So that upon Whole I find the Trapezium ABCD contain 3 Roods and a little (viz. 4 square Perches) above half a Rood.

In the last Place then, by adding Contents of the two Trapeziums AB and ADEF together, I find the whole Ground ABCDEF to contain one Acre, three Roods, and fifty-eight square Perches: Which

Acre Roods Sq. Per.

1 . 00 . 34

0 . 03 . 24

1 . 3 . 58, that

2 . 0 . 18

square Perches amounting to a Rood more, and eight square Perches over, therefore the Content of the said Ground is in all, (which express'd after the more proper Manner) two Acres, and eighteen odd square Perches.

After the same Manner may the Content of the Ground ABCDEFGHIKL, presented Fig. 37, be found. Namely, first, set out in it as large a Trapezium ABGL as you can; and find the Content of the said Trapezium, by multiplying Half the Diagonal, AG into Whole Sum of the two Perpendiculars and PL. Then find the Content of Triangle BFG by multiplying its B

into Half the Perpendicular PF. Then
the Content of the Nook CDE by
engulthing it into as many Trian-
(*) as you see requisite, viz. CDE,
and Δ CE; and finding the Content
each Triangle, as you did of the Tri-
le BFG. And in like manner is the
Content of the other two Nooks GHI and
to be found. And then at last, the
several Contents of the several Parts of
said Ground being added all together,
give the Content of the Whole
Ground. And after this Method may a
Piece of Land be survey'd, the several
cases that can happen in measuring the
or Hedges of any Ground being re-
sented in Fig. 37.

Hitherto it has been shewn, how to
survey or measure a Piece of Land already
or laid out within its respective
bounds. It may be of use to observe
next, how to set or lay out a Piece
of Ground of such a Measure,
shall be requir'd, or containing such or
a Number of Acres, &c.

6.
Of Laying
or Setting
out a Piece
of Land
requir'd.

Namely, by this Method circular Nooks may be
found as exactly as by any other; at least so exactly, as
that is wanting of Exactness, shall be so little as
altogether inconsiderable. But it must be noted,
in Triangles such circular Nooks or Windings are
into, the nearer you'll come to the exact Measure

7.

A Statute-
Acre,
what,

In order hereto, it is to be knowne the first Place, that an Acre according to Statute-Law does contain one hundred and sixty square Statute-Poles or Perches each such Pole or Perch containing has been above observ'd) fifteen Feet and an Half, or five Yards and an Half.

Such being the Content of an Acre follows, that all rectangular Pieces of Ground, any of whose contiguous Sides of any of the

two Lengths set Perches

opposite here

to, will contain

just an Acre.

Whence it is

obvious, how a

Ground of a sin-

gle Acre may be laid out, if there

Room to make its contiguous Sides

perpendicular one to the other, viz, by

making the two contiguous Sides of some

the two Lengths set together

Hence also it is obvious, that Ground

which have very different Sides, may

have the very same Content.

If there be not Conveniency to lay

the Acre of Ground in a rectangular

Shape, then it may be laid out in

other Shape or Figure, by considering

what Proportions are to be taken

make the Content of the said Figure

Perches

80

40

32

26

18

etc.

Square Perches

= 160 = 1 Acre

al to 160 equal Perches. For In-
ce; if I can lay out the Acre in
Triangular

pe; then

	Basis	Perpend.	
	160 &	2	160×1
Base and	80 &	4	80×2
perpendicular	64 &	5	$64 \times 2\frac{1}{2} = 160$
the said	40 &	8	40×4
angle must	32 &	10	32×5
be some of	(&c.)		&c.
opposite	Perpend.	Basis	

(such like) Proportions one to the o-
r, forasmuch as the Basis multiplied
o Half the Perpendicular (or vice ver-
gives the Content of a Triangle.

The Way, how to lay out an Acre of
ound in a triangular Shape, being
own, thereby may be known the Way
lay out an Acre of Ground in any mul-
gular Figure; forasmuch as all Poly-
is may be constituted by adjoining to-
her several Triangles. And it being
known how to lay out a *single Acre*
Ground in any Shape or Figure;
ence may be known how to lay out
ounds of *more Acres than one* in any
ape, by proportionably encreasing the
ngths of the respective Parts. And thus
ave taken notice of so much of Sur-
ving, as seems requisite to the Design
this Treatise.

C H A P. VII.

Of Fortification.

- I.**
A Fort,
what.
BY a *Fort* or *Fortress* is signify'd, a Place fortify'd, i. e. made strong by the Art of Military Architecture, or Fortification.
- 2.**
A Rampart, what.
The principal Part of a Fort, is that which is called the *Rampart* or *Rampart*, being a Wall of a good Height and Breadth, compos'd chiefly of Earth, encompassing the Place fortify'd. It is presented *Fig. 39*, by DEWXYZ.
- 3.**
A Bulwark or Bastion, what.
The *Bulwark* or *Bastion* of a Rampart is that Part of it, which runs farther out than the rest, ending in an Angle. It is represented *Fig. 39*. by IFEGH, &c.
- 4.**
The Face, Gorge, Shoulder, and Flank of a Bastion, what.
The several Parts of a Bastion are, its *Face* or *Front* FE; its *Gorge* (or Neck) IH; its *Shoulder* F; and its *Flank* (or *Wing*) FI; which, according to the Method of the *French*, is not built in a straight Line, but rounding, as is represented in some of the other Bastions, by Prick'd-circular Lines about the Flank.
- 5.**
A Curtain, what.
The Part of the Rampart between two Bastions is called the *Curtain* KI, which joyns together the two Bastions IFEGH and KLD MN.

Moreover, forasmuch as (according to the Rules of Fortification) every Rampart is either a (*) Polygon, or at least Tetragon; hence the Line DE is call'd the Side of the outer Polygon; BC the Side of the inner Polygon; AC the Semi-diameter of the inner Polygon; AE the Semi-diameter of the outer Polygon; PA the Cathetus of the inner Polygon; PA the Cathetus of the outer Polygon; PP the Distance of the Polygons.

Besides which there are wont to be peculiarly distinguish'd also these several Lines, viz. the Gorge-line IC; the Head-line CE; the (†) Longest Line of Defence KE, the Shortest Line of Defence

6.
The Side of the outer and inner Polygon, &c. what.

7.
The Gorge-Line, Head-Line, &c. what.

By the foremention'd Lines and Parts of the Rampire are constituted several Angles, whereof the Chief are these; viz. BAC the Angle of the Center; BCA or CBA the Angle of the Polygon; FEG the Angle of the Bastion, otherwise called the Diamond Point, and the Flanked Angle; DOE the outer Flanking Angle; FEl the

8.
Of the principal Angles in Fortification.

(*) The Reason of this Rule of Fortification depends upon the due Proportion there ought to be between the several Parts of the Rampart. And hence, according to the said Rules, a regular Polygon is to be preferr'd before an Irregular. The Rampart, Fig. 39, is a regular Hexa-

(†) See Sect. 30, 31, 32, of this Chapter.

inner

inner Flanking Angle; FCE the *Front angle*, or Angle forming the Face; E the *Flank angle*, or Angle forming the Flank; CEF the *Head-line Angle*, &c.

9.

How Fortification belongs to Trigonometry.

It is also obvious, that by the foremention'd Lines are made several plain Triangles, viz. ABC, ADE, APD, APE, ApC; pFI, kFI, FIC, FCE, &c. Hence any three Parts of each of the said Triangles (except the (||) three Angles) being known, the other three unknown may be found by Trigonometry, as has been before shewn. Such as would have particular Illustrations by Examples, may consult such Treatises as are professedly written of Fortification. Those young Gentlemen, for whose Use this Treatise is especially design'd, being such as are not likely to concern themselves in the practical Part of Fortification, it seems abundantly sufficient to my Design, to have thus shewn in general how Fortification depends upon Trigonometry.

10.

The Explanation of other Terms of Fortification.

However being thus led, by (the Subject of this Treatise) Trigonometry, to take notice of the foremention'd Part and Terms of Fortification, because it may be of good Use, in order to make

(||) The Reason of this Exception is largely given, Chap. 2. §. 1, of this Trigonometrical Treatise.

young

young Gentlemen understand, in a convenient measure, Relations given of Sieges, shall therefore here add the Explication of such other Parts and Terms of Fortification, as are of principal Note and Use, and so most frequently occur in the Accounts of Sieges.

A *Parapet* then is (properly) a Work rais'd on the Rampart, behind which the Soldiers stand, and where the Cannon is plac'd for the Defence of the Fort. As in Fig. 51 and 52, *ab* denotes the Breadth of the Rampart at its Basis or Bottom, so *cd* denotes the Breadth of the Parapet at its Bottom, or where it is rais'd on the Rampart.

A *Banquet* is no other than a Foot-space at the Bottom of a Parapet, upon which the Soldiers stand up to fire into the Ditch, or upon the Covert-way beyond the Ditch. Some Parapets have only one Foot-space, as is represented by *de*, Fig. 51. But it is the more commodious to have two, one for the taller Soldiers, and another (somewhat above the former) for the shorter, as is represented between *d* and *e*, Fig. 52.

According to the old Way of Fortification, there is erected between the Ramparts and the Ditch, a Work called the *Fausse-braye*, or *Fals braye*, being a smaller Sort of a Rampart, having a Parapet, and

11.

A Parapet, what.

12.

A Banquet, what.

13.

A Fausse-braye, what.

and running round the whole main part of the Fort. It is represented Fig. 51, by *xyz*. But the French omit the Work now-a-days in their Fortification leaving between the Rampart and the Ditch only a Space about three or four Foot wide, to receive the Earth which falls from the Parapet. This Space they call the *Berme*. See Fig. 52. Wherein, as also Fig. 51, *klmn* denote the Ditch.

14.
The Co-
vert-way,
what.

On the outer-side of the Ditch is the *Covert-way*, being a Way or Walk (round the out-side of the Ditch) covered or defended by the *Glacis*. It is represented Fig. 51 and 52, by *np*.

15.
The Glacis,
what.

The *Glacis* serves as a Parapet to the *Covert-way*, and loses it self insensibly in the Field. Hence the Largest are esteem'd the Best, because they lose themselves more insensibly than shorter ones. It is denoted Fig. 51 and 52, by *pr*.

16.
The Counter-
scarp,
what.

The *Counter-scarp* is properly the Slope *nm* of the Ditch on its Out-side, as being opposite to the *Scarp* or Slope *kl* of the Ditch on its Inside. But by this Term now-a-days is generally understood the *Covert-way* with its Parapet.

17.
Of the ad-
ditional
Works of
Fortificati-
on.

Besides the Works hitherto spoken of, and which are requisite to all Fortifications, there are also other *additional* Works contrived by Masters of Military Architecture,

re, for to further fortify the several Parts of Fortification already describ'd. And these are *Half-Moons*, *Horn-works*, *Crown-works*, *Star-works*, *Ravelins*, *Tenailles*, &c. of which the four former take their Names from their Shape. They will all be better apprehended by their respective Draughts, than by verbal Descriptions.

I begin with the *Tenaille*; of which there are three Sorts, represented *Fig. 40*, *41*, and *42*. They are placed in the ditch, and before the Curtains of the Rampart. They are said to be contriv'd by the *French* instead of the *Fausse-braye*. The *Tenaille*, *Fig. 41*, is distinguish'd by the Name of the *single Tenaille*; and that *Fig. 42*, by the Name of the *double Tenaille*.

A *Ravelin* is represented *Fig. 43*; being a small triangular Work. It is generally rais'd also before some Curtain, either of the main Rampart, as *Fig. 43*, and *46*, or of some Out-work, as the *Ravelin*, *Fig. 44*, before the Curtain of the Horn-work, *Fig. 47*, or else before some other Part analagous to a Curtain, the *Ravelin*, *Fig. 45*, before the single *Tenaille*, *Fig. 41*.

An *Half-Moon* (*Fig. 53*.) is generally confounded with a *Ravelin*, its Difference being principally (if not only) this, that its Gorge is an Arch in Shape of

18.

A *Tenaille*,
what.

19.

A *Ravelin*,
what.

20.

An *Half-Moon*,
what.

of the Concave Part of an Half-Moon, and it is placed overagainst the Point of a Bastion to cover it, whereas a Ravelin consists of two straight Demi-gorges as *de ef*. Fig. 46, and is placed overagainst some Curtain, as is afore observ'd.

21. An Horn-work is represented Fig. 47. The Fore-part of it consists of a Curtain between two Half-Bastions, which run out like Horns, whence it takes its Denomination. It is placed either before a Curtain or a Bastion.

22. A Crown-work is represented Fig. 48. It is so called, because the Fore-part of it resembles a Crown. It is usually placed before an Horn-work, to keep the Enemy at a Distance. It is also placed immediately before a Curtain or Bastion of a Rampart.

23. A Star-work is represented Fig. 49. A Star is a Work with several Faces, which flank one the other, as

24. A Redoubt is a small square Fort, or Guard-house, having no Defence but its Front. It is usually designed for maintaining the Lines of Circumvallation, Countervallation. In watery Places they are often made of Mason's Work. It is represented Fig. 50.

25. All the foremention'd Works, which lie without the Rampart of the Forts, are in general call'd the Out-works.

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A *Battery* is a Place rais'd whereon to plant the great Cannon, in order to batter or play upon the Place besieg'd.

26.

A Battery, what.

Cavaliers are Works rais'd on the Parapet of a Rampart, whereon to plant Cannon in order to scour the Field, and to oppose any Work rais'd by the Besiegers, which commands the Place besieg'd.

27.

Cavalliers, what.

Fascins are a Sort of Faggots, made to throw into the Ditch, where there is much Water, in order to make the Passage over to the Wall or Rampart of the Place besieg'd, more easie.

28.

Fascins, what.

Gabions are Baskets filled with Earth, and usually placed upon Batteries, and Parapets, that have suffer'd very much, and also before other Places, to secure them from the Enemies Shot. Lesser Gabions are call'd *Corbeilles*.

29.

Gabions, what.

A *Gallery* is a made Way or Walk, cover'd with Earth or Turf, and upheld with Planks. They are made in the Ditch already fill'd with Fascins, to the end the Miners may approach safe to the Bastion.

30.

A Gallery, what.

The *Line of Defence* is that, which is represented by the Discharge of the small Shot towards the Face of a Bastion. It is distinguish'd into the *Longest* and *Shortest*, otherwise called *Figant* and *Rasant*.

31.

Line of Defence, what.

The

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32.
Line of
Defence
Fichant,
what.

The *Line of Defence Fichant* (or *Longest Line of Defence*) is the Line KE, called, because the Bullets or Shot, which pass along this Line, may fix on the Face of the opposite Bastion.

33.
Line of
Defence
Razant,
what.

The *Line of Defence Razant* (or the *Shortest Line of Defence*) is the Line KE drawn from the Face of the Bastion, to that Point K, of the adjoining Curtain, where the Face of the said Bastion begins to be discovered. It is so called because the Shot, that passes along the said Line, only rases the Face of the said Bastion.

34.
A Lodg-
ment,
what.

A *Lodgment* is a Work cast up in a dangerous Post won by Attack, to secure the Besiegers against the Enemies Fire. It is made of any Materials, that are capable of making Resistance.

35.
To Nail up
a Cannon,
what.

To *nail up a Cannon*, is to drive a Nail (or the like) into its Touch-hole.

36.
To Sap,
what.

To *Sap*, is to dig deep into the Earth of the Covert-way and Glacis in the Front of a Trench. The Earth dug out serves for a Security on the Right and Left, and covers above, the Soldiers (or others) in the Trench against the Enemies Fire-works, by the help of Hurdles laden with the said Earth.

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Military Trenches are of the same Kind with common Trenches, only larger, being usually from six to seven Foot in Depth, and from eight to ten Foot in breadth. They are made by the Besiegers, to approach more securely the Place besieged; whence they are otherwise called the *Lines of Approaches*, or sometimes *the Approaches*. And they are therefore carried on, as not to be in View of the Enemy, or presently and easily discoverable by the Enemy or Besieg'd.

37.

Trenches, what.

Lines of Circumvallation are Trenches made by the Besiegers about their Camp: well to hinder the Relief of the Besieged, as to stop Deserters from their own Army. They are guarded with a *Parapet*.

38.

Lines of Circumvallation, what.

Lines of Countervallation are Trenches which the Besiegers make to secure themselves from the Sallies of the Besieg'd. They are also guarded with a *Parapet*.

39.

Lines of Countervallation, what.

Lines of Communication are Trenches made from one Work to another by the Besiegers, for the better holding Communication one with the other, and helping the other, in case of an Attack by the Enemy, in any of their Works.

40.

Lines of Communication, what.

A Retrenchment is a Work made by the Besieg'd to secure themselves, and so to enable them to hold out some time longer.

41.

A Retrenchment, what.

G

ger

ger against the Enemy, who is so far advanced as to be lodg'd on the Rampart. It has either a good Parapet, or instead thereof Gabions. And thus I have explain'd the more usual Terms of Fortification, and such as more frequently occur in Relations of Sieges.

C H A P. VIII.

Of the Tables of Logarithms, and Artificial Sines and Tangents.

I.
The Method of the Tables of artificial Sines and Tangents, adjoin'd to this Treatise.

THE Tables of Artificial Sines and Tangents belonging properly to Trigonometry, they are therefore here adjoin'd to the End of this Treatise. They are so contriv'd, by placing the Sines and Cosines by the Side one of the other, and likewise the Tangents and Cotangents, that each Page shews the Sine and Cosine of two Angles, one whereof is set down on the Top of the Page, the other (being the Complement of the former to 99) at the Bottom of the Page. Thus the Page (or Pages,) that hath Degree 2 at the Top, hath Degree 87 at the Bottom. And as the Sines and Cosines, Tangents and Cotangents belong

belonging to the Degrees specified at the Top, are respectively shewn by the respective Words set at the Top of the several Columns in each Page; so the Sines and Cosines, &c. belonging to the Degrees specified at the Bottom, are respectively shewn by the respective Words set at the Bottom of the several Columns in each Page.

The Minutes between each two Degrees are set down on the Sides of the Pages, those appertaining to the Degrees at the Top increasing downwards; the other appertaining to the Degrees at the Bottom increasing upwards. And on the Side of each Minute stands its respective Sine and Cosine, Tangent or Cotangent.

And, although Logarithms are of Use, in other Parts of Mathematicks as well as in Trigonometry, yet because they must always be used with Artificial Sines and Tangents; I have therefore judg'd this the most proper Place also for the Table of Logarithms belonging to my Mathematical Treatises: of which I need say no more here, the Use of the said Table of Logarithms having been already explain'd, in the Appendix to the *Young Gentleman's Arithmetick*.

2.
*The Table
of Loga-
rithms,
why ad-
join'd also
to this
Treatise.*

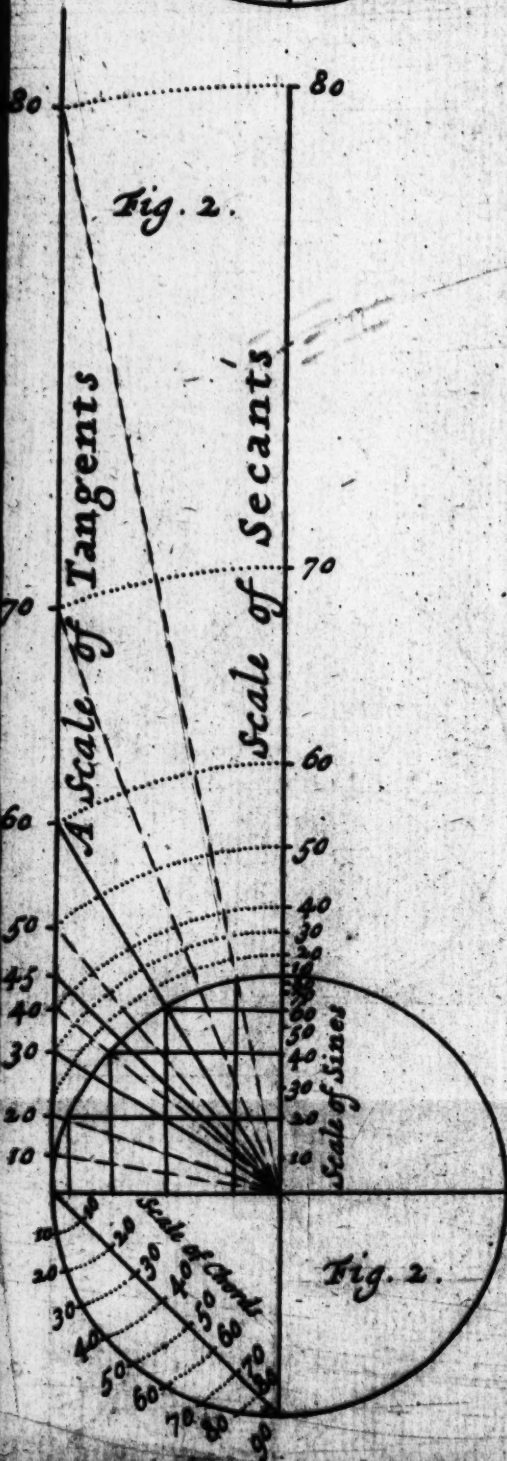
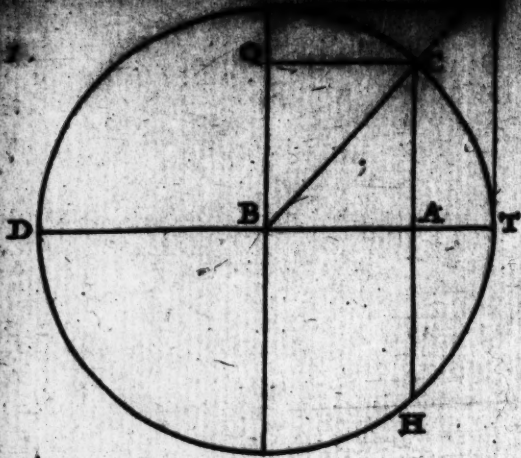


Fig. 3.

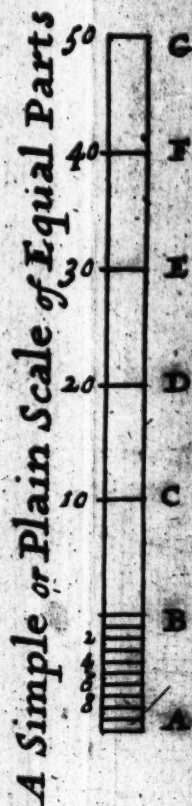
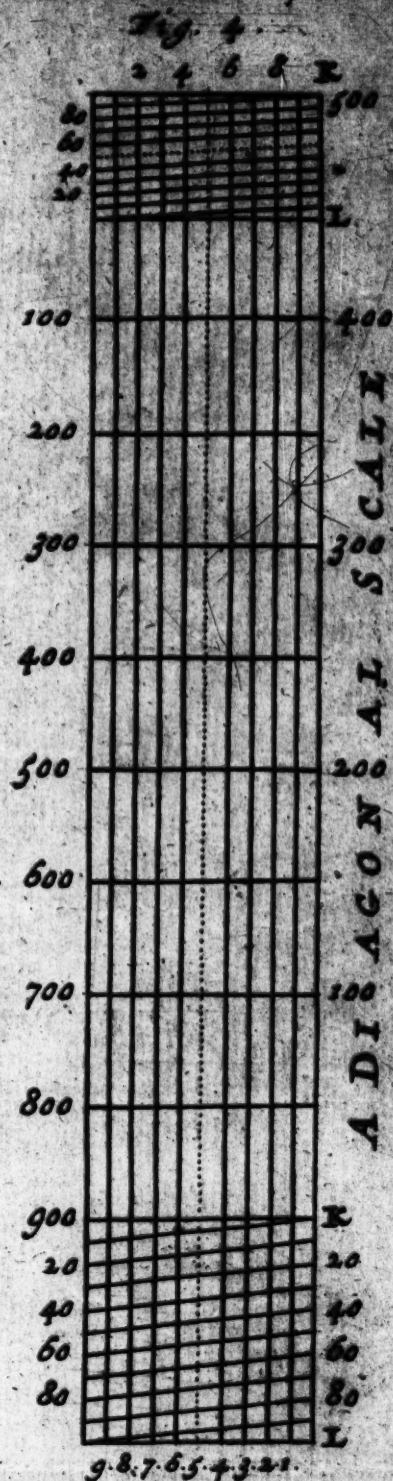
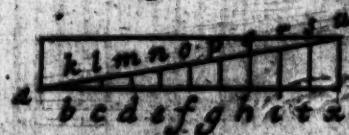
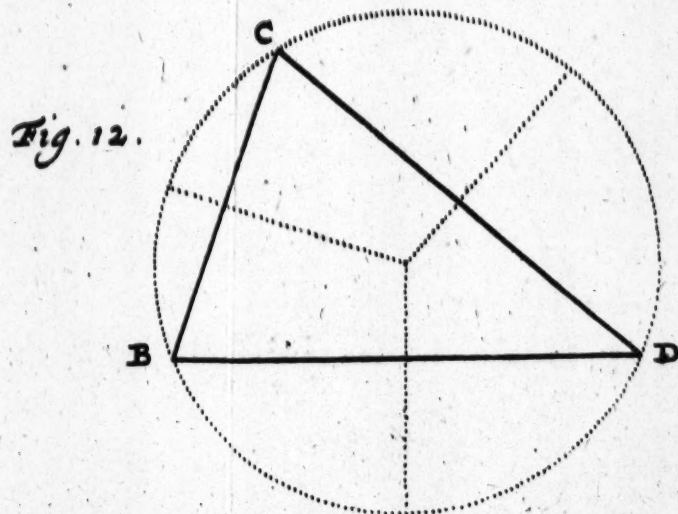
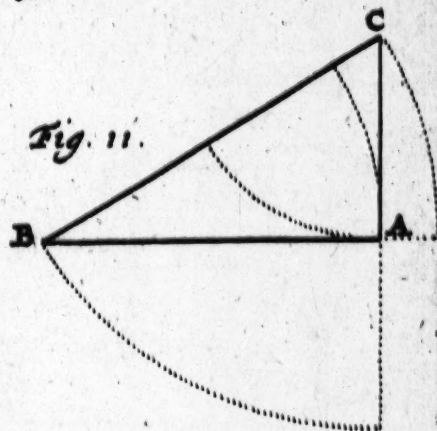
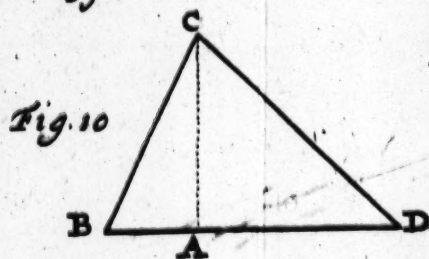
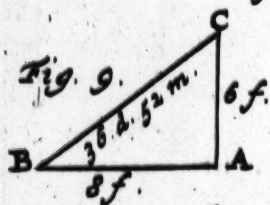
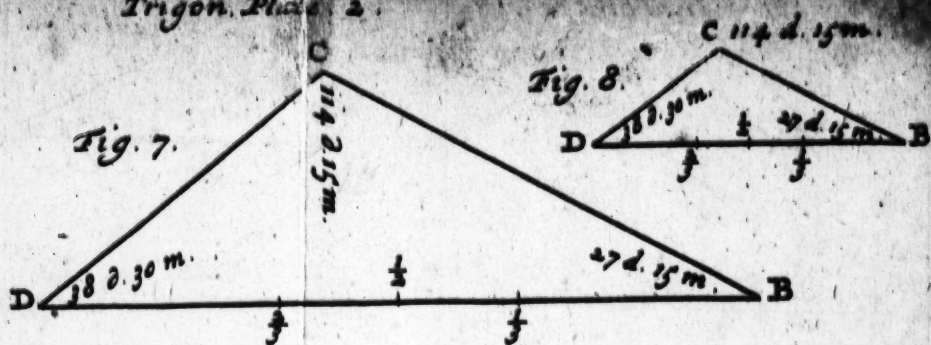


Fig. 6.



Trigon. Plac. 2.



Trigon. Plate. 3.

Fig. 13

Fig. 15

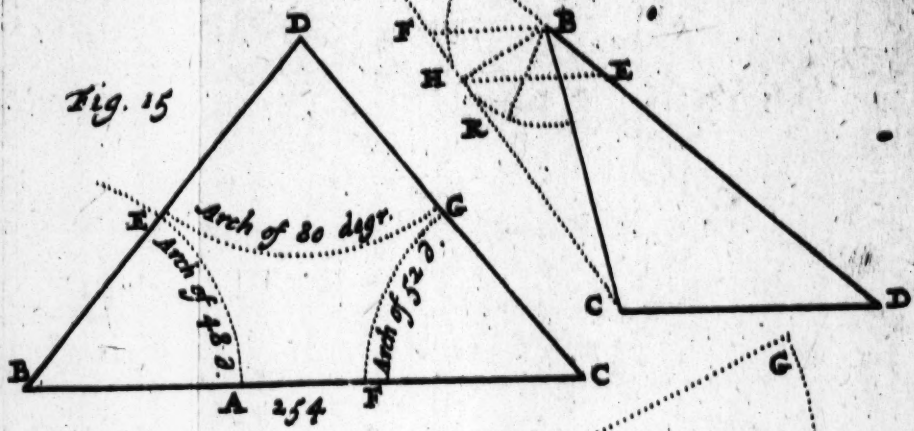


Fig. 14.

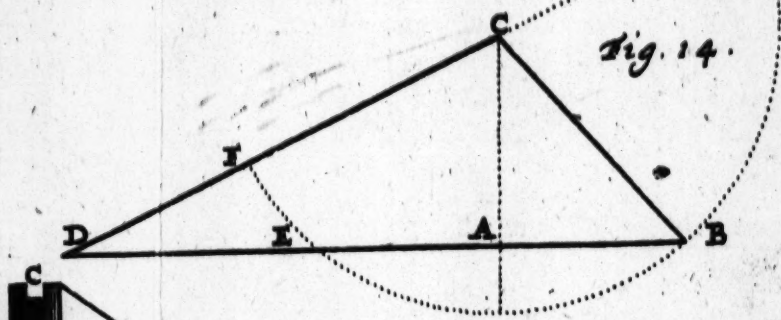


Fig. 16

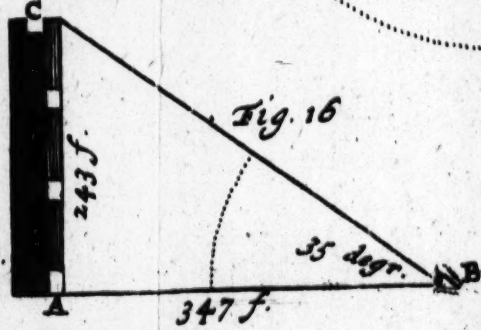


Fig. 17

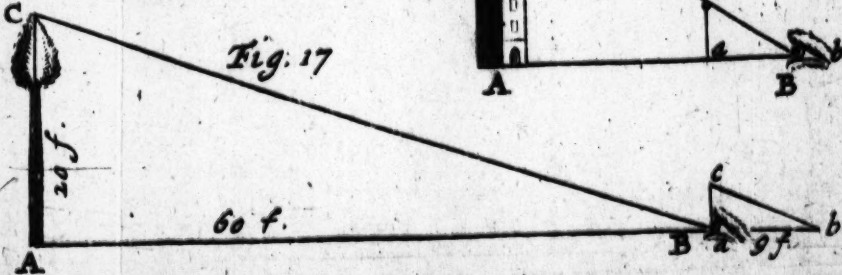
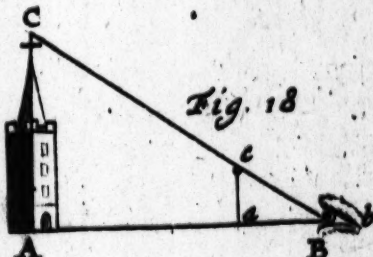
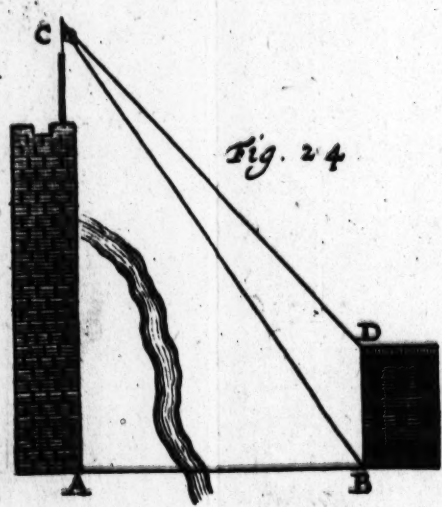
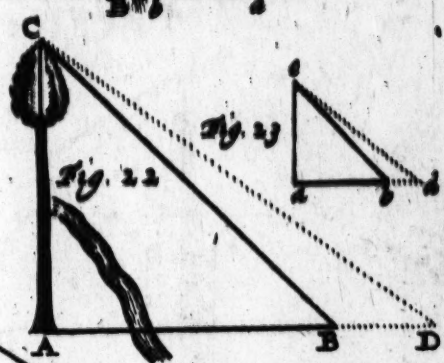
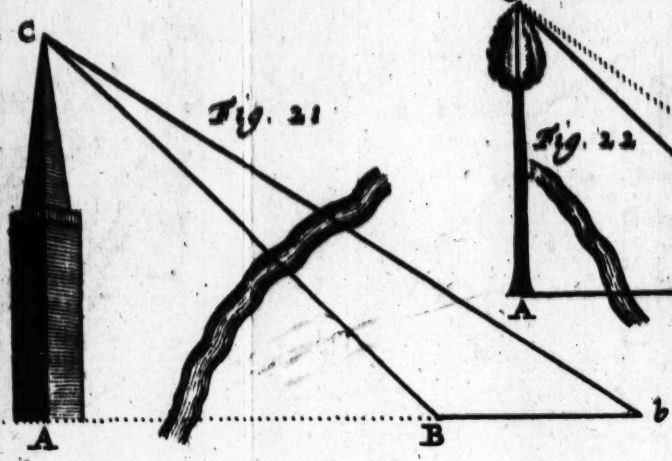
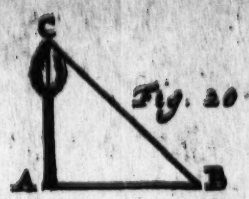
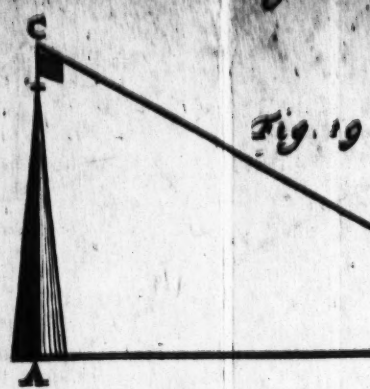


Fig. 18





Trigon. Plate 5.

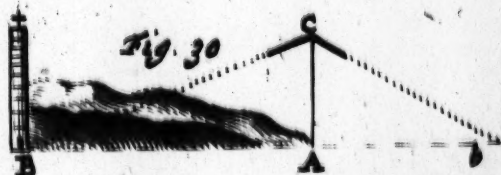
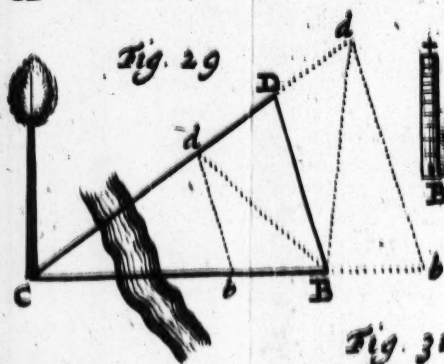
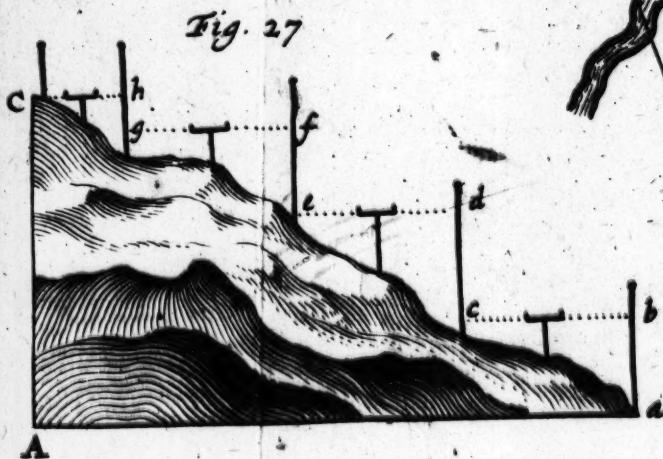
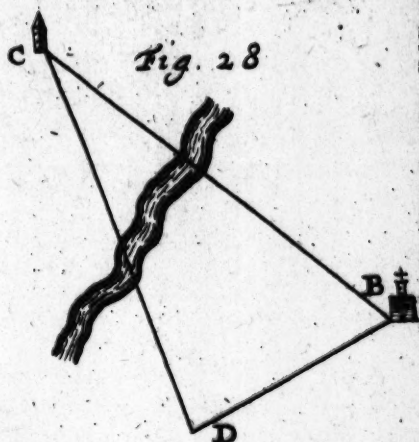
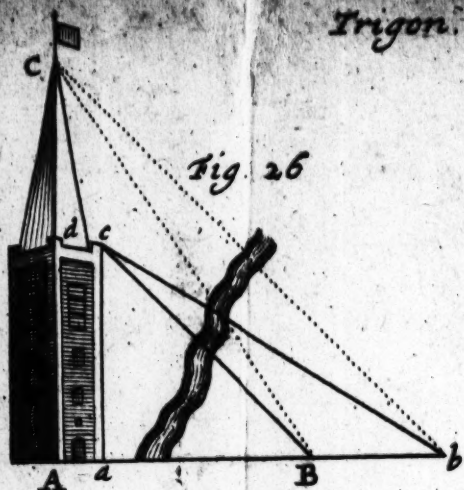
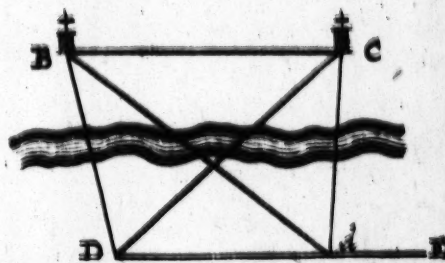


Fig. 31



Trigon. Plate. 6.

Fig. 32

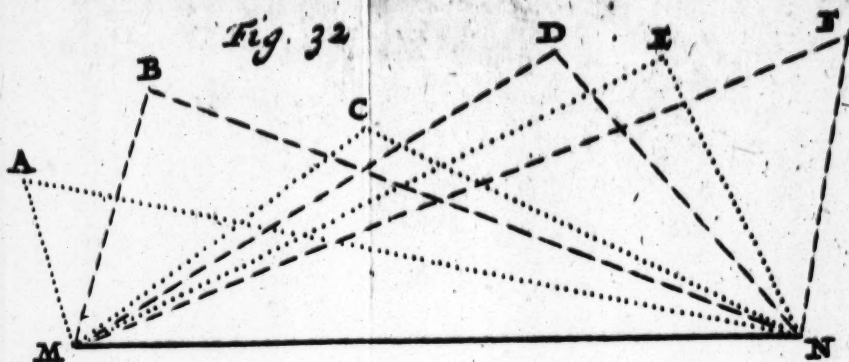


Fig. 33

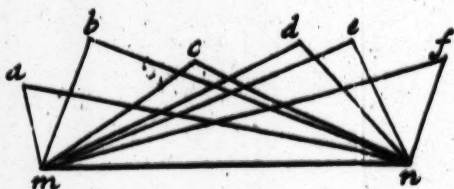


Fig. 34

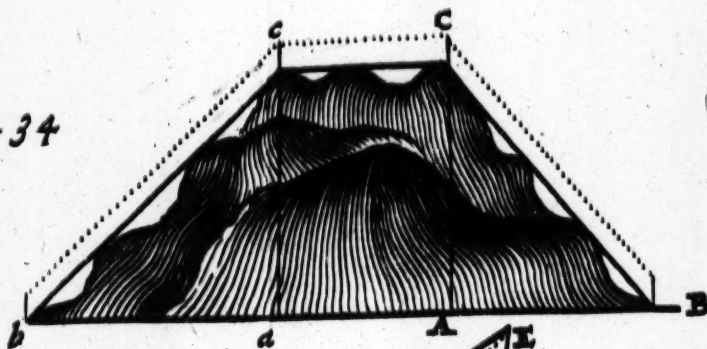
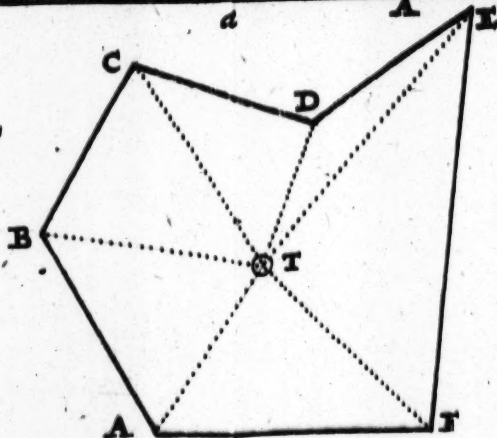


Fig. 35



Trigon. Plate 7.

Fig. 36

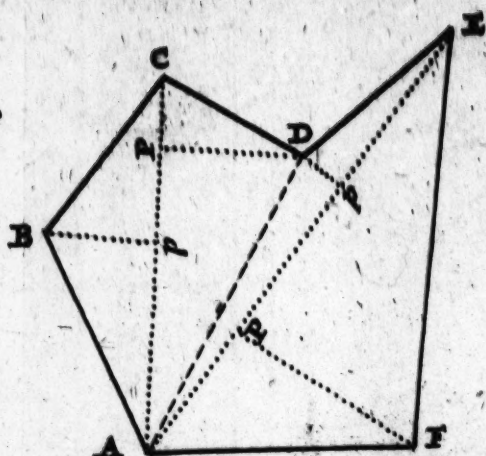


Fig. 37

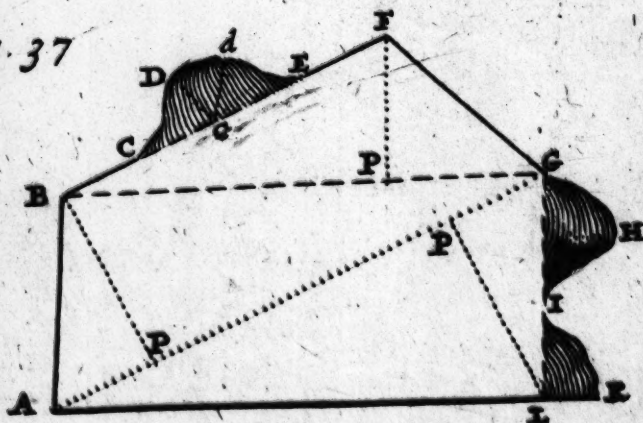
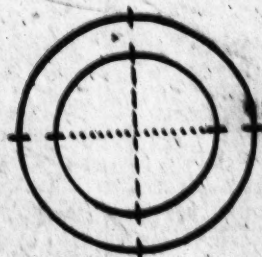


Fig. 38



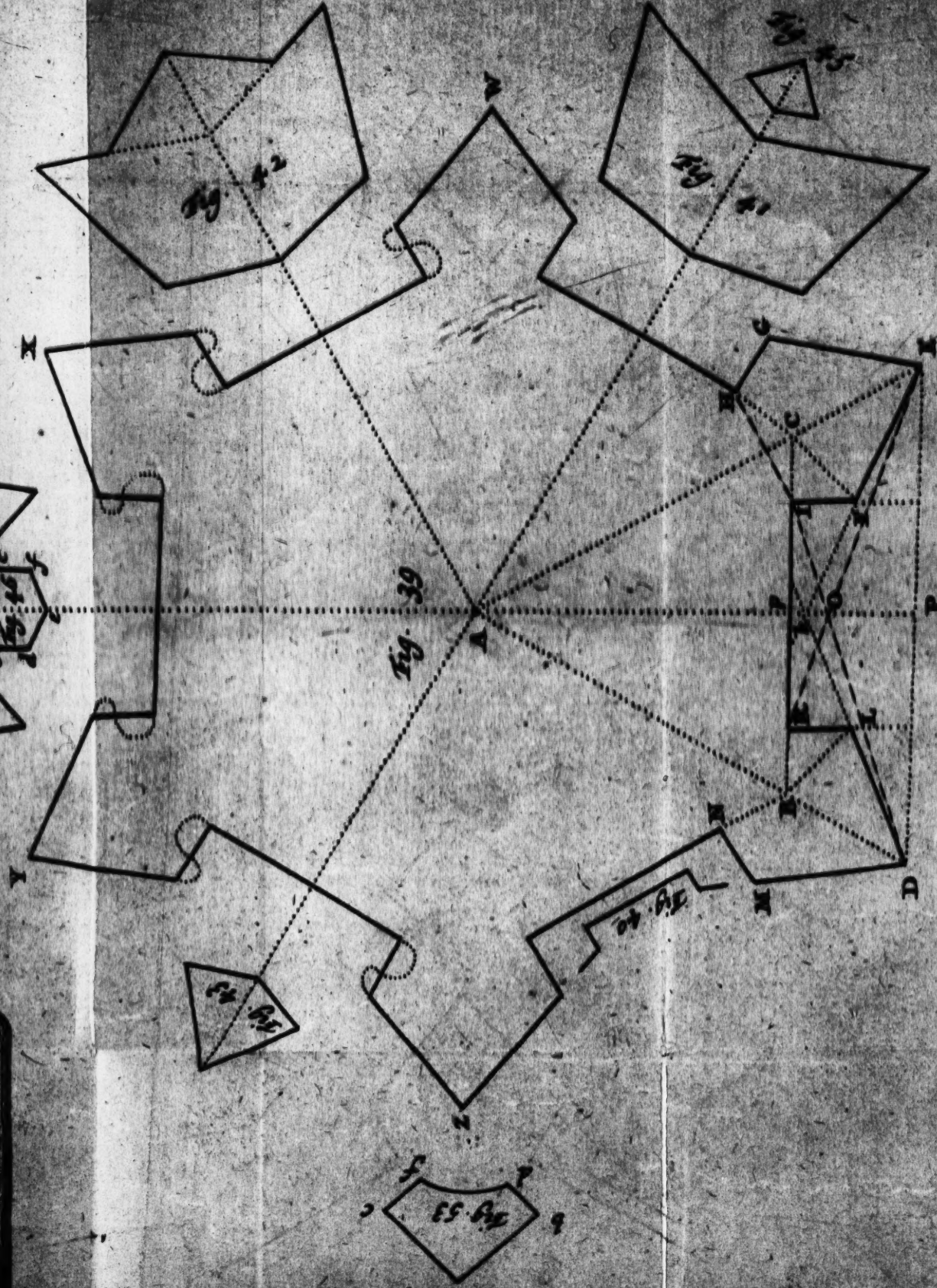
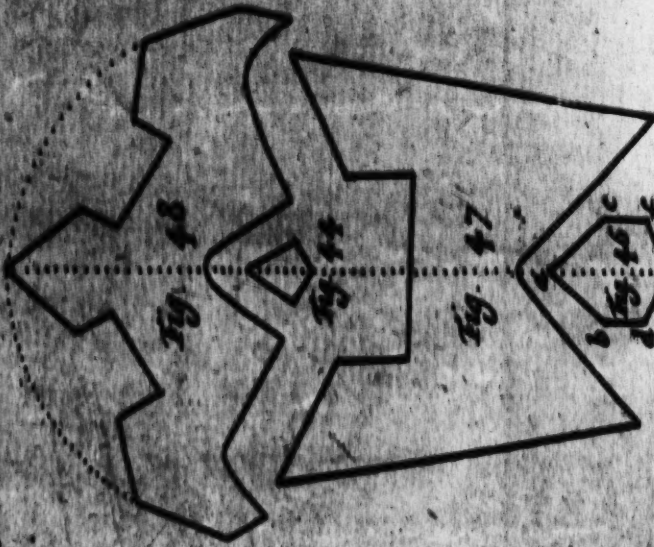
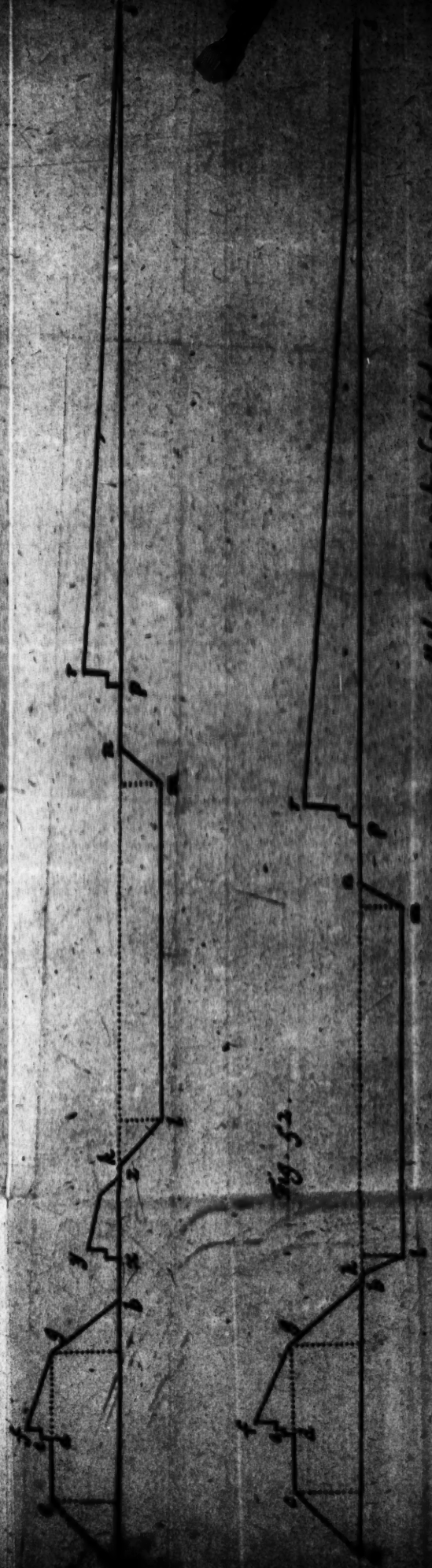


Fig. 51.



All the Cases to be folded out

A
TABLE

OF

MUSEUM

logarithm's,

from One to Ten Thousand



Log.	N	Log.	N	Log.
0.000000	34	1.531479	67	1.826075
0.301030	35	1.544068	68	1.832509
0.477121	36	1.556303	69	1.838849
0.602060	37	1.568202	70	1.845098
0.698970	38	1.579783	71	1.851258
0.778151	39	1.591064	72	1.857332
0.845098	40	1.602060	73	1.863323
0.903090	41	1.612784	74	1.869232
0.954242	42	1.623249	75	1.875061
1.000000	43	1.633468	76	1.880813
1.041393	44	1.643452	77	1.886491
1.079181	45	1.653212	78	1.892094
1.113943	46	1.662758	79	1.897627
1.146128	47	1.672098	80	1.903090
1.176091	48	1.681241	81	1.908485
1.204120	49	1.690196	82	1.913814
1.230449	50	1.698970	83	1.919078
1.255272	51	1.707570	84	1.924279
1.278753	52	1.716003	85	1.929419
1.301030	53	1.724276	86	1.934498
1.322219	54	1.732394	87	1.939519
1.342422	55	1.740362	88	1.944482
1.361728	56	1.748188	89	1.949390
1.380211	57	1.755875	90	1.954242
1.397940	58	1.763428	91	1.959041
1.414973	59	1.770852	92	1.963788
1.431364	60	1.778151	93	1.968483
1.447158	61	1.785330	94	1.973128
1.462398	62	1.792391	95	1.977723
1.477121	63	1.799340	96	1.982271
1.491361	64	1.806180	97	1.986772
1.505150	65	1.812913	98	1.991226
1.518514	66	1.819544	99	1.995635

The Table of Logarithm's.

N	0	1	2	3	4
100	000000	000434	000868	001301	001735
101	004321	004755	005181	005609	006037
102	008600	009026	009451	009876	010301
103	012837	013259	013679	014100	014521
104	017033	017451	017868	018284	018701
105	021189	021603	022016	022428	022841
106	025306	025715	026125	026533	026941
107	029384	029789	030195	030599	031003
108	033424	033826	034227	034628	035029
109	037426	037825	038223	038620	039018
110	041393	041787	042182	042576	042971
111	045323	045714	046105	046495	046886
112	049218	049606	049992	050379	050765
113	053078	053463	053846	054229	054612
114	056905	057286	057666	058046	058425
115	060698	061075	061452	061829	062206
116	064458	064832	065206	065579	065951
117	068186	068557	068928	069298	069667
118	071882	072249	072617	072985	073352
119	075547	075912	076276	076640	077003
120	079181	079543	079904	080266	080627
121	082785	083144	083503	083861	084219
122	086359	086716	087071	087426	087781
123	089905	090258	090610	090963	091315
124	093422	093772	094122	094471	094820
125	096910	097257	097604	097951	098298
126	100371	100715	101059	101403	101746
127	103804	104146	104487	104828	105169
128	107209	107549	107888	108227	108566
129	110589	110926	111263	111599	111935

The Table of Logarithmes.

	6	7	8	9	D
166	002598	003029	003461	003891	432
486	006894	007321	007748	008174	428
724	011147	011570	011993	012415	424
940	015359	015779	016197	016616	419
116	019532	019947	020361	020775	416
352	023664	024075	024486	024896	412
349	027757	028164	028571	028978	408
408	031812	032216	032619	033021	404
429	035829	036229	036629	037028	400
414	039811	0402	040602	040998	496
362	043755	044148	044539	044932	393
275	047664	048053	048442	048830	389
152	051538	051924	052309	052694	386
996	055378	055760	056142	056524	382
805	059185	059563	059942	060320	379
582	062958	063333	063709	064083	376
326	066699	067071	067443	067815	372
039	070407	070776	071145	071514	369
718	074085	074451	074816	075182	366
868	077731	078094	078457	078819	363
887	081347	081707	082067	082426	360
576	084934	085291	085647	086004	357
36	088490	088845	089198	009552	355
67	092018	092369	092721	093071	351
69	095518	095866	096215	096562	349
44	098989	099335	099681	100026	346
91	102434	102777	103119	103462	342
10	105851	106191	106531	106871	340
03	109241	109579	109916	110253	338
69	112605	112939	113275	113609	335

The Table of Logarithmes.

N	0	1	2	3	4
130	113943	114277	114611	114944	115277
131	117271	117603	117934	118265	118596
132	120574	120903	121231	121559	121887
133	123852	124178	124504	124830	125156
134	127105	127429	127753	128076	128400
135	130334	130655	130977	131298	131619
136	133539	133858	134177	134496	134815
137	136721	137037	137354	137671	137987
138	139879	140194	140508	140822	141136
139	143015	143327	143639	143951	144263
140	146128	146438	146748	147058	147367
141	149219	149527	149835	150142	150450
142	152288	152594	152899	153205	153511
143	155336	155639	155943	156246	156550
144	158362	158664	158965	159266	159567
145	161368	161667	161967	162266	162565
146	164353	164650	164947	165244	165541
147	167317	167613	167908	168203	168498
148	170262	170555	170848	171141	171434
149	173186	173478	173769	174059	174350
150	176091	176381	176669	176959	177248
151	178977	179264	179552	179839	180126
152	181844	182129	182415	182699	182984
153	184691	184975	185259	185542	185826
154	187521	187803	188084	188365	188646
155	190332	190612	190892	191171	191451
156	193125	193403	193681	193959	194237
157	195899	196176	196453	196729	197006
158	198657	198932	199206	199481	199756
159	201397	201670	201942	202216	202489

The Table of Logarithmes.

	5	6	7	8	9	D
5611	115942	116276	116608	116939	333	
8926	119256	119586	119915	120245	330	
2216	122544	122871	123198	123525	328	
5481	125806	126131	126456	126781	325	
8722	129045	129268	129685	130012	323	
939	132259	132579	132899	133219	321	
133	135451	135769	136086	136403	318	
303	138618	138934	139249	139564	315	
449	141763	142076	142389	142702	314	
574	144885	145196	145507	145818	311	
676	147985	148294	148603	148911	309	
756	151154	151369	151676	151982	307	
815	154119	154423	154728	155032	305	
852	157154	157457	157759	158061	303	
868	160161	160469	160769	161068	301	
862	163161	163459	163758	164055	299	
838	166134	166430	166726	167022	297	
792	169086	169380	169674	169968	295	
726	172019	172311	172603	172895	293	
641	174932	175222	175512	175802	291	
536	177825	178113	178401	178689	289	
413	180699	180986	181272	181558	287	
269	183555	183839	184123	184407	285	
108	186674	186674	186956	187239	283	
28	189209	189490	189771	190051	281	
30	192009	192289	192567	192846	279	
14	194792	195069	195346	195623	276	
81	197556	197832	198107	198382	276	
29	200303	200577	200850	201124	274	
61	203033	203303	203577	203848	272	

The Table of Logarithmical

N	0	1	2	3	4
160	204119	204391	204663	204934	205205
161	206826	207096	207365	207634	207902
162	209515	209783	210051	210319	210586
163	212187	212454	212720	212986	213251
164	214844	215109	215373	215638	215901
165	217484	217747	218010	218273	218535
166	220108	220369	220629	220889	221148
167	222716	222976	223235	223494	223752
168	225309	225568	225826	226084	226341
169	227887	228144	228400	228657	228913
170	230449	230704	230959	231215	231469
171	233096	233350	233604	233857	234110
172	235718	235971	236223	236475	236727
173	238316	238567	238818	239068	239318
174	240849	241099	241348	241597	241845
175	243388	243636	243884	244131	244378
176	245911	246158	246404	246650	246895
177	248423	248668	248913	249157	249401
178	250916	251159	251402	251645	251887
179	253388	253630	253872	254113	254354
180	255773	256014	256254	256494	256734
181	258131	258371	258610	258849	259087
182	260461	260699	260937	261174	261411
183	262771	263008	263244	263480	263715
184	265051	265287	265522	265757	265991
185	267301	267536	267770	268004	268237
186	269521	269755	269988	270221	270453
187	271651	271884	272116	272348	272579
188	273781	274013	274244	274475	274705
189	275891	276122	276352	276582	276811

The Table of Logarithmes.

	5	6	7	8	9	D
475	205746	206016	206286	206556	206826	267
173	208441	208710	208978	209247	209516	269
853	211121	211388	211654	211921	212188	267
518	213783	214049	214314	214579	214844	266
166	216429	216694	216957	217221	217485	264
798	219060	219323	219585	219846	220107	262
414	221675	221936	222196	222456	222716	261
015	224274	224533	224791	225051	225310	259
599	226858	227115	227372	227629	227886	258
169	229426	229682	229939	230193	230448	256
724	231979	232234	232488	232746	233001	254
264	234517	234770	235023	235276	235529	253
789	237041	237292	237544	237795	238046	252
299	239549	239799	240049	240299	240549	250
95	242044	242293	242441	242789	243037	249
77	244525	244772	245019	245266	245512	248
45	246991	247237	247482	247728	247973	246
98	249443	249687	249932	250176	250420	245
38	251881	252125	252368	252610	252853	243
64	254306	254548	254789	255031	255272	242
77	256718	256958	257198	257438	257678	241
77	259116	259355	259594	259833	260072	239
93	261501	261739	261976	262214	262452	238
86	263873	264109	264346	264582	264818	237
96	266232	266467	266702	266937	267172	235
74	268578	268812	269046	269279	269513	234
99	270912	271144	271377	271609	271842	233
71	273233	273464	273696	273927	274158	232
1	275542	275772	276002	276232	276462	230
98	277838	278067	278296	278525	278754	229

The Table of Logarithmes.

N	0	1	2	3	4
190	278754	278982	279211	279439	279667
191	281033	281261	281488	281714	281941
192	283307	283527	283753	283976	284198
193	285557	285782	286007	286232	286456
194	287802	288026	288249	288473	288696
195	290035	290257	290479	290702	290924
196	292256	292478	292699	292920	293141
197	294466	294687	294907	295127	295347
198	296665	296884	297104	297322	297541
199	298853	299071	299289	299507	299724
200	301025	301247	301464	301581	301798
201	303196	303412	303628	303844	304059
202	305351	305566	305781	305996	306211
203	307496	307705	307924	308137	308351
204	309630	309843	310056	310268	310481
205	311754	311956	312177	312389	312599
206	313867	314078	314289	314499	314709
207	315970	316180	316389	316599	316808
208	318063	318270	318481	318689	318898
209	320146	320354	320562	320769	320976
210	322219	322426	322633	322835	323041
211	324282	324488	324694	324895	325096
212	326336	326541	326745	326945	327146
213	328379	328583	328787	328991	329193
214	330414	330617	330819	331022	331224
215	332438	332640	332842	333044	333245
216	334454	334655	334856	335057	335257
217	336459	336659	336856	337055	337254
218	338456	338656	338856	339054	339253
219	340444	340642	340841	341039	341237

The Table of Logarithmes.

	5	6	7	8	9	D
9895	280123	780351	280578	280896	228	
2169	282396	282622	282849	283075	227	
4431	284656	284882	285107	285332	226	
6681	286905	287125	287354	287578	225	
8919	289143	289366	289589	289812	223	
1147	291369	291591	291813	292034	222	
3362	293584	293804	294025	294246	221	
5567	295787	296007	296226	296446	220	
7761	297979	298198	298416	298635	219	
9943	300161	330378	600595	300813	218	
114	302331	302547	302764	302979	217	
275	304491	304706	304921	305136	216	
425	306639	306854	307068	307282	215	
564	308778	308991	309204	309417	213	
695	310906	311118	311329	311542	212	
812	313023	313234	313445	313656	211	
910	315130	315340	315551	315760	210	
018	317227	317438	317646	317854	209	
106	319314	319522	319730	319938	208	
204	321391	321598	321805	322012	207	
32	323458	323665	323871	324077	206	
10	325516	325721	325926	326131	205	
32	327563	327767	327972	328176	204	
98	329601	329805	330008	330211	203	
27	331629	331832	332034	332236	202	
47	333649	333850	334051	334253	202	
58	335658	335859	336055	336255	201	
59	337659	337858	338058	338257	200	
51	339650	339849	340047	340246	199	
25	341632	341830	342028	342225	198	

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N	0	1	2	3	4
220	342422	342620	342817	343014	343211
221	344392	344589	344785	344981	345178
222	346353	346549	346744	346939	347135
223	348305	348499	348694	348889	349084
224	350258	350442	350636	350829	351023
225	352183	352375	352568	352761	352954
226	354108	354301	354493	354685	354878
227	356026	356217	356408	356599	356790
228	357935	358125	358316	358506	358696
229	359835	360025	360215	360404	360594
230	361728	361917	362105	362294	362483
231	363612	363799	363988	364176	364364
232	365488	365675	365862	366049	366236
233	367356	367542	367729	367915	368102
234	369216	369401	369587	369772	369958
235	371068	371253	371437	371622	371807
236	372912	373094	373279	373464	373649
237	375577	375759	375942	376124	376307
238	376577	376759	376942	377124	377307
239	378398	378579	378761	378942	379124
240	380211	380392	380573	380754	380935
241	382017	382197	382377	382557	382738
242	383815	383995	384174	384353	384533
243	385606	385785	385964	386142	386322
244	387389	387568	387746	387923	388103
245	389166	389343	389520	389698	389876
246	390935	391112	391288	391464	391641
247	392697	392873	393048	393224	393400
248	394452	394627	394802	394977	395152
249	396199	396374	396548	396722	396897

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	6	7	8	9	D
09	343606	343802	343999	344196	197
73	345569	345766	345962	346157	196
30	347528	347720	347915	348110	195
78	349472	349659	349860	350054	194
16	351409	351603	351796	351989	193
47	353339	353532	353724	353916	193
68	355239	355452	355642	355834	192
81	357172	357363	357554	357744	191
86	359076	359266	359456	359646	190
83	360972	361161	361350	361539	189
71	362859	363048	363236	363424	188
51	364739	364926	365113	365301	188
23	366609	366796	366983	367169	187
87	368473	368659	368845	369030	186
43	370328	370513	370698	370882	185
91	372175	372359	372544	372728	184
31	374015	374198	374382	374565	184
64	375846	376029	376212	376394	183
88	377670	377852	378034	378216	182
06	379487	379668	379849	380030	181
51	381296	381476	381656	381837	181
77	383097	383277	383456	383636	180
22	384891	385069	385249	385428	179
99	386677	386856	387034	387212	178
93	388456	388634	388811	388989	178
01	390228	390405	390582	390759	177
77	391993	392169	392345	392521	179
33	393751	393926	394101	394277	176
69	395501	395676	395850	396025	175
37	397245	397419	397592	397766	174

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N	0	1	2	3	4
250	397940	398114	398287	398461	398635
251	399674	399847	400019	400192	400365
252	401401	401573	401745	401917	402089
253	403121	403292	403464	403635	403806
254	404834	405005	405176	405346	405517
255	406540	406710	406881	407051	407221
256	408239	408409	408579	408749	408918
257	409933	410102	410271	410439	410608
258	411619	411788	411956	412124	412292
259	413299	413467	413635	413803	413971
260	414973	415140	415307	415474	415641
261	416641	416807	416973	417139	417304
262	418301	418467	418633	418798	418963
263	419956	420121	420286	420451	420616
264	421604	421768	421933	422097	422261
265	423246	423409	423574	423737	423900
266	424882	425045	425208	425371	425534
267	426411	426574	426736	426899	427061
268	428135	428297	428459	428621	428783
269	429752	429914	430075	430236	430397
270	431364	431525	431685	431846	432006
271	432969	433129	433289	433449	433608
272	434569	434729	434888	435048	435207
273	436163	436322	436481	436639	436798
274	437751	437909	438067	438226	438384
275	439333	439491	439648	439806	440000
276	440909	441066	441224	441381	441538
277	442479	442637	442793	442949	443105
278	444045	444201	444357	444513	444668
279	445604	445759	445915	446071	446226

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	6	7	8	9	D
398981	399154	399328	399501	173	
400711	400883	401056	401228	173	
402433	402605	402777	402949	172	
404149	404320	404492	404663	171	
405858	406029	406199	406369	171	
407561	407731	407901	408070	170	
409257	409426	409595	409764	169	
410946	411114	411283	411451	169	
412629	412796	412964	413132	168	
414405	414472	414639	414806	167	
415974	416141	416308	416474	167	
417638	417804	417969	418135	166	
419295	419460	419625	419791	165	
420945	421110	421275	421439	165	
422589	422754	422918	423082	164	
424228	424392	424555	424718	164	
425860	426023	426186	426349	163	
427486	427648	427811	427973	162	
429106	429268	429429	429591	162	
430719	430881	431042	431203	161	
432328	432488	432649	432809	161	
433929	434089	434249	434409	160	
435526	435685	435844	436004	159	
437116	437275	437433	437592	159	
438701	438859	439017	439175	148	
440279	440437	440594	440752	158	
441852	442009	442166	442323	157	
443419	443576	443732	443889	157	
444981	445137	445293	445449	156	
446537	446692	446848	447003	155	

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N	0	1	2	3
280	447158	447313	447468	447623
281	448706	448861	449015	449169
282	450249	450403	450557	450711
283	451786	451939	452093	452247
284	453318	453471	453624	453777
285	454845	454997	455149	455302
286	456366	456518	456669	456821
287	457889	458033	458184	458336
288	459392	459543	459694	459845
289	460898	461048	461196	461348
290	462398	462548	462697	462847
291	463893	464042	464191	464340
292	465383	465532	465680	465829
293	466868	467016	467164	467312
294	468347	468495	468643	468790
295	469822	469969	470116	470263
296	471292	471438	471585	471732
297	472756	472903	473049	473195
298	474216	474362	474508	474653
299	475671	475816	475962	476107
300	477121	477266	477411	477555
301	478566	478711	478855	478999
302	480007	480151	480294	480438
303	481443	481586	481729	481872
304	482874	483016	483159	483302
305	484299	484442	484585	484727
306	485721	485863	486005	486147
307	487138	487279	487421	487564
308	488551	488592	488833	488974
309	489958	490099	490229	490379

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	6	7	8	9	D
932	448088	448242	448397	448552	155
947	449633	449787	449941	450095	154
961	451172	451326	451479	451633	154
975	452706	452859	453012	453165	153
989	454235	454387	454539	454692	463
606	455758	455910	456062	456214	152
620	457276	457428	457579	457731	152
634	458789	458939	459091	459242	151
648	460296	460447	460597	460748	151
662	461799	461948	462098	462248	150
146	463296	463445	463594	463744	150
160	464788	464936	465085	465234	149
174	466274	466423	466571	466719	149
188	467756	467904	468052	468199	148
202	469233	469380	469527	469675	447
557	470704	470851	470998	471145	147
571	472171	472318	472464	472610	146
585	473633	473779	473925	474071	146
599	475089	475235	475381	475526	146
613	476542	476687	476833	476976	145
844	477989	478133	478278	478422	145
858	479431	479575	479719	479863	144
872	480869	481012	481156	481299	144
886	482302	482445	482588	482731	143
900	483729	483872	484015	484157	143
111	485153	485295	485437	485579	142
125	486572	486714	486855	486997	142
139	487986	488127	488269	488409	141
153	489396	489537	489677	489818	141
167	490801	490941	491081	491122	140

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N	0	1	2	3	4
10	491362	491502	491642	491782	4919
11	492760	492900	493039	493179	4933
12	494155	494294	494433	494572	4947
13	495544	495683	495822	495960	4960
14	496929	497068	497206	497344	4974
15	498311	498448	498586	498724	4988
16	499687	499824	499962	500099	5002
17	501059	501196	501333	501470	5016
18	502427	502564	502700	502837	5029
19	503791	503927	504063	504199	5043
20	505149	505286	505421	505557	5057
21	506505	506640	506776	506911	5070
22	507856	507991	508126	508260	5083
23	509203	509337	509471	509606	5097
24	510545	510679	510813	510947	5110
25	511883	512017	512151	512284	5124
26	513218	513351	513484	513617	5138
27	514584	514681	514813	514946	5150
28	515874	516006	516139	516271	5164
29	517196	517328	517459	517592	5177
30	518514	518646	518777	518909	5191
31	519828	519959	520090	520221	5204
32	521138	521269	521399	521530	5217
33	522444	522575	522705	522835	5230
34	523746	523876	523976	524136	5243
35	525045	525174	525304	525434	5256
36	526339	526469	526598	526727	5269
37	527629	527759	527888	528016	5282
38	528916	529045	529174	529302	5295
39	530129	530258	530386	530514	5307

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	6	7	8	9	D
062	492401	492341	492481	492621	140
45	493597	49373	493874	494015	139
850	494989	495128	495267	495406	139
232	496370	496515	496653	496791	139
621	497759	497897	498035	498173	138
999	499137	499275	499412	499549	138
374	500510	500648	500785	500922	137
744	501880	502017	502154	502291	137
109	503240	503382	503518	503655	136
471	504607	504743	504878	505014	136
828	505964	506099	506234	506369	136
181	507316	507451	507586	507721	135
529	508664	508799	508934	509068	135
874	510009	510143	510277	510411	134
215	511349	511482	511616	511749	134
551	512684	512818	512951	513084	133
883	514016	514149	514282	514415	133
211	515344	515476	515609	515741	132
535	516668	516799	516931	517064	132
855	517987	518119	518251	518382	132
171	519303	519434	519566	519697	131
484	520615	520745	520876	521007	131
792	521922	522053	522183	522314	131
096	523226	523356	523486	523616	130
396	524526	524656	524785	524915	130
691	525822	525951	526081	526210	129
985	527114	527243	527372	527501	129
274	528402	528531	528659	528788	129
555	529687	529815	529943	530072	128
830	530968	531096	531223	531351	128

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N	0	1	2	3	4
340	531479	531607	531734	531862	5319
341	532754	532882	533009	533136	5332
342	534026	534153	534280	534407	5345
343	535294	535421	535547	535674	5358
344	536558	536685	536811	536937	5370
345	537819	537945	538071	538197	5383
346	539076	539202	539327	539452	5395
347	540329	540455	540579	540705	5408
348	541579	541704	541829	541953	5420
349	542825	542929	543072	543199	5432
350	544008	544192	544316	544440	5445
351	545307	545431	545555	545678	5458
352	546543	546666	546789	546913	5470
353	547775	547898	548021	548144	5482
354	549003	549126	549229	549371	5495
355	550228	550351	550473	550595	5508
356	551449	551572	551694	551816	5518
357	552668	552789	552911	553033	5532
358	553883	554004	554126	554247	5545
359	555094	555215	555336	555457	5555
360	556303	556423	556544	556664	5568
361	557507	557627	557748	557868	5578
362	558709	558829	558948	559068	5588
363	559907	560026	560146	560265	5605
364	561101	561221	561339	561459	5615
365	562293	562412	562531	562649	5628
366	563481	563599	563718	563837	5638
367	564666	564784	564903	565021	5648
368	565848	565966	566084	566202	5658
369	567026	567144	567262	567379	5668

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	5	6	7	8	9	10
2117	532249	532372	532489	532617	128	
3391	533518	533645	533772	533899	127	
4661	534787	534914	535041	535167	127	
5927	536053	536179	536304	536432	126	
7189	537315	537441	537567	537693	126	
8448	538574	538699	538825	538951	126	
9703	539829	539954	540079	540204	125	
10955	541079	541205	541329	541454	125	
203	542327	542452	542576	542701	125	
333	543571	543696	543819	543944	124	
444	544812	544934	545059	545183	124	
555	546049	546172	546296	546419	124	
666	547282	547405	547529	547652	123	
777	548512	548635	548758	548881	123	
888	549739	549861	549984	550106	123	
999	550962	551084	551206	551328	122	
110	552181	552303	552425	552547	122	
220	553386	553519	553640	553762	121	
330	554610	554731	554852	554973	121	
440	555819	555940	556061	556182	121	
550	557026	557146	557267	557387	120	
660	558228	558349	558469	558589	120	
770	559428	559548	559667	559787	120	
880	560624	560743	560863	560982	119	
990	561817	561936	562055	562174	119	
1000	563006	563125	563244	563362	119	
1100	564192	564311	564429	564548	119	
1200	565376	565494	565612	565729	118	
1300	566555	566673	566791	566909	118	
1400	567732	567849	567967	568084	118	

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N	0	1	2	3	4
370	568202	568319	568436	568554	568671
371	569374	569491	569608	569725	569842
372	570543	570659	570776	570893	571010
373	571709	571825	571942	572058	572175
374	572872	572988	573104	573219	573335
375	574041	574147	574263	574379	574495
376	575188	575303	575419	575534	575650
377	576341	576457	576572	576687	576803
378	577492	577607	577722	577836	577952
379	578639	578754	578868	578983	579098
380	579784	579898	580012	580126	580241
381	580925	581039	581153	581267	581381
382	582063	582177	582291	582404	582518
383	583199	583312	583426	583539	583653
384	584331	584444	584557	584670	584784
385	585461	585574	585686	585799	585912
386	586587	586699	586812	586925	587038
387	587711	587823	587935	588047	588160
388	588832	588944	589056	589167	589279
389	589949	590061	590173	590284	590396
390	591065	591176	591287	591399	591510
391	592177	592288	592399	592509	592620
392	593286	593397	593508	593618	593729
393	594398	594503	594614	594724	594835
394	595496	595606	595717	595827	595938
395	596597	596707	596817	596927	597037
396	597695	597805	597914	598024	598134
397	598790	598899	599009	599119	599228
398	599883	599992	600101	600210	600319
399	600973	601082	601191	601299	601408

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	6	7	8	9	D
88	568905	569023	569139	569257	117
59	570076	570193	570309	570426	117
26	571243	571359	571476	571592	117
91	572407	572523	572639	572755	116
52	573568	573684	573799	573915	116
09	474726	574841	574957	575072	116
65	575880	575996	576111	576226	115
17	577032	577147	577262	577377	115
66	578181	578295	578409	578523	115
12	579326	579441	579555	579669	114
53	580469	580583	580697	580811	114
95	581608	581722	581836	581949	114
31	582745	582858	582972	583085	114
65	583879	583992	584105	584218	113
96	585009	585122	585235	585348	113
24	586137	586249	586362	586475	113
59	587262	587374	587486	587599	112
75	588384	588496	588608	588719	112
75	589503	589615	589726	589838	112
45	590619	590750	590842	590953	112
99	591732	591843	591955	592066	111
09	592843	592954	593064	593175	111
18	593950	594061	594171	594282	111
24	595055	595165	595276	595386	110
27	596167	596157	596377	596487	110
27	597256	597366	597476	597586	110
024	598353	598462	598572	598681	110
119	599446	599556	599665	599774	109
210	600537	600646	600755	600864	109
299	601625	601734	601843	601951	109

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N	00	10	20	30	40
400	602039	602169	602297	602386	602462
401	602144	602253	602361	602449	602525
402	602226	602334	602442	602530	602606
403	602305	602413	602521	602628	602704
404	602381	602489	602596	602704	602780
405	602455	602562	602669	602777	602853
406	602526	602633	602739	602847	602923
407	602594	602701	602808	602914	602990
408	610660	610767	610873	610979	611055
409	611723	611829	611936	612042	612118
410	612784	612889	612996	613102	613178
411	613842	613947	614053	614159	614235
412	614897	615003	615108	615213	615289
413	615950	616055	616160	616265	616341
414	617000	617105	617210	617315	617391
415	618048	618153	618257	618362	618438
416	619093	619198	619302	619406	619482
417	620136	620240	620344	620448	620524
418	621176	621280	621384	621448	621524
419	622214	622318	622421	622525	622601
420	623249	623353	623456	623559	623635
421	624282	624385	624488	624591	624667
422	625312	625415	625518	625621	625697
423	626340	626443	626546	626648	626724
424	627366	627468	627571	627673	627749
425	628389	628491	628593	628695	628771
426	629409	629512	629613	629715	629791
427	630428	630529	630631	630733	630809
428	631444	631547	631647	631748	631824
429	632457	632559	632659	632761	632837

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	5	6	7	8	9	D
603	603117	602819	602928	603036	108	
686	603794	603902	604008	604118	108	
766	604874	604982	505089	605197	108	
844	605951	606059	606166	606274	108	
919	607026	607133	607241	607348	107	
991	608098	608205	608312	608419	107	
061	609167	609274	609381	609488	107	
128	610234	610341	610447	610554	107	
192	611298	611405	611511	611617	106	
254	612359	612466	612572	612678	106	
313	613415	613525	613630	613736	106	
369	614475	614581	614686	614792	106	
424	615529	615634	615739	615845	105	
476	616581	616686	616790	616895	105	
525	617629	617734	617839	617943	105	
571	618676	618780	618884	618989	105	
615	619719	619824	619928	620032	104	
656	620760	620864	620968	621072	104	
695	621799	621902	622007	622110	104	
732	622815	622939	623042	623146	104	
766	623869	623973	624076	624179	103	
798	624901	625004	625107	625209	103	
827	625929	626032	626135	626237	103	
853	626956	627058	627161	627263	103	
878	627979	628082	628185	628287	102	
899	629002	629104	629206	629308	103	
919	630021	630123	630224	630326	102	
936	631038	631139	631241	631342	102	
951	632052	632153	632255	632356	101	
963	633064	633165	633266	633367	101	

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N	0	1	2	3	4
430	633468	633569	633670	633771	633872
431	634477	634578	634679	634779	634880
432	635484	635584	635685	635785	635886
433	636488	636588	636688	636789	636889
434	637489	637589	637689	637789	637889
435	638489	638589	638689	638789	638889
436	639486	639586	639686	639786	639886
437	640481	640581	640680	640779	640879
438	641475	641573	641672	641771	641870
439	642465	642563	642662	642761	642860
440	643453	643551	643650	643749	643848
441	644439	644537	644636	644734	644833
442	645422	645521	645619	645717	645816
443	646404	646502	646599	646696	646794
444	647383	647481	647579	647676	647774
445	648360	648458	648555	648653	648750
446	649335	649432	649529	649627	649724
447	650308	650405	650502	650599	650696
448	651278	651375	651472	651569	651666
449	652246	652343	652439	652536	652633
450	653213	653309	653405	653502	653598
451	654177	654273	654369	654465	654561
452	655138	655235	655331	655427	655523
453	656098	656194	656289	656386	656481
454	657056	657152	657247	657343	657438
455	658011	658107	658202	658298	658393
456	658965	659060	659155	659250	659345
457	659916	660011	660106	660201	660296
458	660865	660960	661055	661149	661244
459	661813	661907	662002	662096	662191

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	6	7	8	9	D
973	634075	634075	634276	634376	100
981	635081	635182	635283	635383	100
986	636087	636187	636288	636388	100
989	637089	637189	637289	637389	100
989	638089	638189	638289	638389	99
988	639088	639188	639287	639387	99
984	640084	640183	640283	640382	99
978	641077	641177	641276	641375	99
969	642069	642168	642267	642366	99
959	643058	643156	643255	643354	99
946	644041	644143	644242	644340	98
931	645029	645127	645226	645324	98
913	646011	646109	646208	646306	98
894	646992	647089	647187	647285	98
872	647969	648067	648165	648262	98
848	648945	649043	649140	649237	97
821	649919	650016	650113	650210	97
793	650890	650987	651084	651181	97
762	651859	651956	652053	652149	97
729	652826	652923	653019	653116	97
695	653791	653888	653984	654080	96
658	654754	654850	654946	655042	96
619	655715	655810	655906	656002	96
577	656673	656769	656864	656960	96
534	657629	657725	657820	657916	96
488	658584	658679	658774	658869	95
441	659536	659630	659726	659821	95
391	660486	660581	660676	660771	95
339	661424	661529	661623	661718	95
286	662380	662475	662569	662663	95

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N	0	1	2	3
460	662758	662852	662947	663041
461	663701	663795	663889	663982
462	664642	664736	664829	664924
463	665581	665675	665769	665862
464	666518	666611	666705	666799
465	667453	667546	667639	667733
466	668386	668479	668572	668665
467	669317	669409	669503	669596
468	670246	670339	670431	670524
469	671173	671265	671358	671451
470	672098	672190	672283	672375
471	673021	673113	673205	673297
472	673942	674034	674126	674218
473	674861	674953	675045	675137
474	675778	675869	675962	676053
475	676694	676785	676876	676968
476	677607	677698	677789	677881
477	678518	678609	678700	678791
478	679428	679519	679609	679700
479	680336	680426	680517	680607
480	681241	681332	681422	681513
481	682145	682235	682326	682416
482	683047	683137	683227	683317
483	683947	684037	684127	684217
484	684845	684935	685025	685114
485	685742	685831	685921	686010
486	686636	686726	686815	686904
487	687529	687618	687707	687796
488	688419	688509	688598	688687
489	689309	689398	689486	689575

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	6	7	8	9	D
29	663324	663418	663512	663607	94
72	664266	664359	664454	664548	94
12	665206	665299	665393	665487	94
49	666143	666237	666331	666424	94
86	667079	667173	667266	667359	94
19	668013	668106	668199	668293	93
52	668945	669038	669131	669224	93
82	669875	669967	670060	670153	93
09	670802	670895	670988	671080	93
36	671728	671821	671913	672005	93
59	672652	672744	672836	672929	92
82	673574	673666	673758	673849	92
02	674494	674586	674677	674769	92
29	675412	675503	675595	675687	92
56	676328	676419	676511	676602	92
81	677242	677333	677424	677516	91
03	678154	678245	678335	678427	91
23	679064	679155	679246	679337	91
42	679972	680063	680154	680245	91
69	680879	680969	681060	681151	91
93	681784	681874	681964	682055	90
16	682686	682777	682867	682957	90
37	683587	683677	683767	683857	90
58	684486	684576	684666	684756	90
78	685383	685473	685563	685652	90
98	686279	686368	686458	686547	89
18	687172	687261	687351	687439	89
38	688064	688153	688242	688331	89
58	688953	689042	689131	689220	89
78	689841	689930	690019	690107	89

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N	0	1	2	3
490	690196	690285	690373	690462
491	691081	691169	691258	691347
492	691965	692053	692142	692229
493	692847	692935	693023	693111
494	693727	693815	693903	693991
495	694605	694693	694781	694868
496	695482	695569	695657	695744
497	696356	696444	696531	696618
498	697229	697317	697404	697491
499	698101	698188	698275	698362
500	698970	699057	699144	699231
501	699838	699924	700011	700098
502	700704	700790	700877	700963
503	701568	701654	701741	701827
504	702430	702517	702603	702689
505	703291	703377	703463	703549
506	704151	704236	704322	704408
507	705008	705094	705179	705265
508	705863	705949	706035	706120
509	706718	706803	706888	706974
510	707570	707655	707740	707826
511	708421	708506	708591	708676
512	709269	709355	709439	709524
513	710117	710202	710287	710371
514	710963	711048	711132	711217
515	711807	711892	711976	712060
516	712649	712734	712818	712902
517	713491	713575	713659	713742
518	714329	714414	714497	714581
519	715267	715351	715435	715518

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	6	7	8	9	D
39	690728	690816	690905	690993	89
24	691612	691700	691789	691877	88
06	692494	692583	692671	692759	88
87	693375	693463	693551	693639	88
66	694254	694342	694429	694517	88
44	695131	695219	695307	695394	88
19	696007	696094	696182	696269	87
93	696880	696968	697055	697142	87
69	697752	697839	697926	698014	87
35	698622	698709	698797	698883	87
04	699491	699578	699664	699751	87
71	700358	700444	700531	700617	87
36	701222	701309	701395	701482	86
99	702086	702172	702258	702344	86
61	702947	703033	703119	703205	86
21	703807	703893	703979	704065	86
97	704665	704751	704837	704922	86
65	705522	705607	705693	705778	86
20	706376	706462	706547	706632	85
74	707219	707305	707390	707475	85
26	708081	708166	708251	708336	85
76	708931	709015	709100	709185	85
24	709779	709863	709948	710033	85
37	710625	710709	710794	710879	85
21	711469	711554	711639	711723	84
06	712313	712397	712481	712566	84
90	713154	713238	713323	713407	84
74	713994	714078	714162	714246	84
58	714833	714916	714999	715084	84
41	715669	715753	715836	715919	84

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N	0	1	2	3
520	716003	716087	716170	716254
521	716838	716921	717004	717088
522	717671	717754	717837	717920
523	718502	718585	718668	718751
524	719331	719414	719497	719579
525	720159	720242	720325	720407
526	720986	721068	721151	721233
527	721811	721893	721975	722058
528	722634	722716	722798	722881
529	723456	723538	723619	723702
530	724276	724358	724439	724522
531	725095	725176	725258	725339
532	725912	725993	726075	726156
533	726727	726809	726890	726972
534	727541	727623	727704	727785
535	728354	728435	728516	728597
536	729165	729246	729327	729408
537	729974	730055	730136	730217
538	730782	730863	730944	731024
539	731589	731669	731749	731829
540	732394	732474	732555	732635
541	733197	733278	733358	733438
542	733999	734079	734159	734239
543	734799	734879	734959	735039
544	735599	735679	735759	735838
545	736397	736476	736556	736635
546	737192	737272	737352	737431
547	737987	738067	738146	738225
548	738781	738859	738939	739018
549	739572	739651	739731	739809

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	5	6	7	8	9	D
71	6421	716504	716588	716671	716754	83
72	7254	717338	717421	717504	717587	83
73	8086	718169	718253	718336	718419	83
74	8917	718999	719083	719165	719248	83
75	9745	719828	719911	719994	720077	83
76	573	720655	720738	720821	720903	83
77	398	721481	721563	721646	721728	82
78	222	722305	722387	722469	722552	82
79	045	723127	723209	723291	723374	82
80	866	723948	724029	724112	724194	82
81	685	724767	724849	724931	725013	82
82	503	725585	725667	725748	725829	82
83	319	726401	726483	726564	726646	82
84	134	727216	727297	727379	727459	81
85	948	728029	728110	728191	728273	81
86	759	728841	728922	729003	729084	81
87	569	729651	729732	729813	729893	81
88	378	730459	730540	730621	730702	81
89	186	731266	731347	731428	731508	81
90	991	732072	732153	732233	732313	81
91	796	732876	732956	733037	733117	80
92	598	733679	733759	733839	733919	80
93	399	734479	734559	734639	734719	80
94	199	735279	735359	735439	735516	80
95	998	736078	736157	736237	736317	80
96	795	736874	736954	737034	737113	80
97	590	737669	737749	737829	737908	79
98	384	738463	738543	738622	738701	79
99	177	739256	739335	739414	739493	79
00	968	740047	740126	740205	740284	79

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	0	1	2	3	4
550	740363	740442	740521	740599	740677
551	741157	741230	741309	741388	741467
552	741939	742018	742096	742175	742254
553	742725	742802	742882	742961	743040
554	743509	743586	743667	743745	743824
555	744293	744371	744449	744528	744607
556	745075	745153	745231	745309	745388
557	745855	745933	746011	746089	746168
558	746634	746712	746789	746868	746947
559	747417	747495	747573	747651	747730
560	748188	748266	748343	748421	748500
561	748963	749040	749118	749196	749275
562	749736	749814	749891	749969	750048
563	750508	750586	750663	750741	750820
564	751279	751356	751434	751512	751591
565	752048	752125	752202	752280	752359
566	752816	752893	752969	753047	753126
567	753583	753661	753738	753816	753895
568	754348	754425	754501	754579	754658
569	755112	755189	755265	755343	755422
570	755875	755951	756027	756105	756184
571	756636	756712	756788	756866	756945
572	757396	757472	757548	757627	757706
573	758155	758230	758306	758384	758463
574	758912	758988	759063	759142	759221
575	759668	759743	759819	759897	759976
576	760422	760498	760573	760651	760729
577	761176	761251	761326	761404	761483
578	761928	762003	762078	762157	762236
579	762675	762754	762829	762909	762988

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	6	7	8	9	D
740	757740836	740915	740994	741073	79
741	546741624	741703	741782	741860	79
742	332742411	742489	742568	742647	79
743	118743196	743275	743353	743431	78
744	902743979	744058	744136	744215	78
745	684744762	744840	744919	744997	78
746	465745543	745621	745699	745777	78
747	247446323	746401	746479	746556	78
748	023747101	747179	747256	747334	78
749	804747878	747955	748033	748110	78
750	576748653	748731	748808	748885	77
751	349749427	749504	749582	749659	77
752	123750199	750277	750354	750431	77
753	894750971	751048	751125	751202	77
754	664751751	751818	751895	751972	77
755	433752509	752586	752663	752739	77
756	199753277	753353	753429	753506	77
757	966754042	754119	754195	754272	77
758	730754807	754883	754959	755036	76
759	494755564	755646	755722	755799	76
760	256756332	756408	756484	756560	76
761	016757092	757168	757244	757320	76
762	775757851	757927	758003	758079	76
763	533758609	758685	758761	758836	76
764	290759366	759441	759517	759592	76
765	045760121	760196	760272	760347	75
766	799760875	760949	761025	761101	75
767	552761627	761702	761778	761853	75
768	303762378	762453	762529	762604	75
769	053763128	763203	763279	763353	75

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D	0	1	2	3
580	763428	763503	763578	763653
581	764176	764251	764326	764400
582	764923	764998	765072	765147
583	765669	765743	765818	765892
584	766413	766487	766562	766636
585	767156	767230	767304	767379
586	767898	767972	768046	768119
587	768638	768712	768786	768860
588	769377	769451	769525	769599
589	770115	770189	770263	770336
590	770852	770926	770999	771073
591	771587	771661	771734	771808
592	772322	772395	772468	772542
593	773055	773128	773201	773274
594	773786	773859	773933	774006
595	774517	774589	774663	774736
596	775246	775319	775392	775465
597	775974	776047	776119	776193
598	776701	776774	776846	776919
599	777427	777499	777572	777644
600	778151	778224	778296	778368
601	778874	778947	779019	779091
602	779596	779669	779741	779813
603	780317	780389	780461	780533
604	781037	781109	781181	781253
605	781755	781827	781899	781971
606	782473	782544	782616	782688
607	783189	783260	783332	783403
608	783904	783975	784046	784118
609	784617	784689	784759	784831

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	6	7	8	9	D
76	763877	763932	764027	764101	75
76	764524	764699	764774	764848	79
76	765370	765445	765519	765594	78
76	766115	766189	766264	766338	74
76	766859	766933	767007	767082	74
76	767601	767675	767749	767823	74
76	768342	768416	768490	768564	74
76	769082	769156	769229	769303	74
76	769820	769894	769968	770042	74
76	770557	770631	770705	770778	74
77	771293	771367	771440	771514	74
77	772028	772102	772175	772248	73
77	772762	772835	772908	772981	73
77	773494	773567	773640	773713	73
77	774225	774298	774371	774444	73
77	774955	775028	775100	775173	73
77	775683	775756	775829	775902	73
77	776411	776483	776556	776629	73
77	777137	777209	777282	777354	73
77	777862	777934	778006	778079	73
77	778585	778658	778729	778802	72
77	779308	779380	779452	779524	72
77	780029	780101	780173	780245	72
77	780749	780821	780893	780965	72
77	781468	781539	781612	781684	72
78	782186	782258	782329	782401	72
78	782902	782974	783046	783117	72
78	783618	783689	783761	783832	71
78	784332	784403	784475	784546	71
78	785045	785116	785187	785259	71

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N	0	1	2	3
610	785329	785401	785472	785543
611	786041	786112	786183	786254
612	786751	786822	786893	786964
613	787460	787531	787602	787673
614	788164	788239	788309	788381
615	788875	788946	789016	789087
616	789581	789651	789722	789792
617	790285	790356	790426	790496
618	790988	791059	791129	791199
619	791691	791761	791831	791901
620	792392	792462	792532	792602
621	793092	793162	793231	793301
622	793791	793860	793930	793999
623	794488	794558	794627	794697
624	795185	795254	795324	795393
625	795880	795949	796019	796088
626	796574	796644	796713	796782
627	797268	797337	797406	797475
628	797959	798029	798098	798167
629	798651	798719	798789	798858
630	799341	799409	799478	799547
931	800029	800098	800167	800236
632	800717	800786	800854	800923
633	801404	801472	801541	801609
634	802089	802158	802226	802295
635	802774	802842	802910	802979
636	803457	803525	803594	803662
637	804139	804208	804276	804344
638	804821	804889	804957	805025
639	805501	805569	805637	805705

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	6	7	8	9	D
78	785757	785828	785899	785970	71
79	786467	786538	786609	786680	71
70	787177	787248	787319	787389	71
71	787885	787956	788027	788098	71
72	788593	788664	788734	788804	71
73	789299	789369	789439	789510	71
74	790004	790074	790144	790215	70
75	790707	790778	790848	790918	70
76	791409	791480	791550	791620	70
77	792111	792181	792252	792322	70
78	792812	792882	792952	793022	70
79	793511	793581	793651	793721	70
80	794209	794279	794349	794418	70
81	794906	794976	795045	795115	70
82	795602	795672	795741	795811	70
83	796297	796366	796436	796505	69
84	796990	797059	797129	797198	69
85	797683	797752	797821	797890	69
86	798374	798443	798512	798582	69
87	799065	799134	799203	799272	69
88	799754	799823	799892	799961	69
89	800442	800511	800579	800648	69
90	801129	801198	801266	801335	69
91	801815	801884	801952	802021	69
92	802500	802568	802637	802705	68
93	803184	803252	803321	803389	68
94	803867	803935	804003	804071	68
95	804548	804616	804685	804753	68
96	805229	805297	805365	805433	68
97	805908	805976	806044	806112	68

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N	0	1	2	3
640	808179	808248	808316	808384
641	808258	808326	808394	808461
642	808325	808393	808461	808528
643	808393	808461	808528	808595
644	808461	808528	808595	808662
645	808528	808595	808662	808729
646	808595	808662	808729	808796
647	808662	808729	808796	808863
648	808729	808796	808863	808930
649	808796	808863	808930	809000
650	812913	812980	813047	813114
651	813114	813181	813248	813315
652	813315	813382	813449	813516
653	813516	813583	813650	813717
654	813717	813784	813851	813918
655	813918	813985	814052	814119
656	814119	814186	814253	814320
657	814320	814387	814454	814521
658	814521	814588	814655	814722
659	814722	814789	814856	814923
660	814923	814990	815057	815124
661	815124	815191	815258	815325
662	815325	815392	815459	815526
663	815526	815593	815660	815727
664	815727	815794	815861	815928
665	815928	815995	816062	816129
666	816129	816196	816263	816330
667	816330	816397	816464	816531
668	816531	816598	816665	816732
669	816732	816799	816866	816933

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	5	6	7	8	9	D
18	519	806587	806655	806723	806790	68
19	197	807264	807332	807399	807467	68
20	873	807941	808008	808076	808143	68
21	549	808616	808684	808751	808818	67
22	223	809290	809358	809425	809492	67
23	896	809964	810031	810098	810165	67
24	569	810636	810703	810770	810837	67
25	239	811307	811374	811441	811508	67
26	909	811977	812044	812111	812178	67
27	579	812646	812713	812779	812847	67
28	247	813314	813381	813448	813514	67
29	914	813981	814048	814114	814181	67
30	581	814647	814714	814780	814847	67
31	246	815312	815378	815445	815511	66
32	909	815976	816042	816109	816175	66
33	573	816639	816705	816771	816838	66
34	235	817301	817367	817433	817499	66
35	896	817962	818028	818094	818159	66
36	568	818622	818688	818754	818819	66
37	231	819281	819346	819412	819478	66
38	893	819939	820004	820074	820136	66
39	559	820595	820661	820727	820792	66
40	226	821251	821317	821382	821448	66
41	891	821906	821972	822037	822103	65
42	555	822560	822626	822691	822756	65
43	218	823213	823279	823344	823409	65
44	889	823865	823930	823996	824061	65
45	551	824516	824581	824646	824711	65
46	211	825166	825231	825296	825361	65
47	871	825815	825880	825945	826009	65

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N	0	1	2	3	4
670	826074	826139	826204	826269	826334
671	826723	826787	826852	826917	826982
672	827369	827434	827499	827563	827628
673	828015	828079	828144	828209	828274
674	828659	828724	828789	828853	828918
675	829304	829368	829433	829497	829562
676	829947	830011	830075	830139	830204
677	830589	830653	830717	830781	830846
678	831229	831294	831358	831422	831487
679	831869	831934	831998	832062	832127
680	832509	832573	832637	832701	832766
681	833147	833211	833275	833338	833403
682	833784	833848	833912	833976	834040
683	834421	834484	834548	834612	834676
684	835056	835119	835183	835247	835311
685	835691	835754	835817	835881	835945
686	836324	836387	836451	836514	836578
687	836957	837019	837083	837146	837210
688	837588	837652	837716	837779	837843
689	838219	838282	838345	838408	838472
690	838849	838912	838975	839038	839102
691	839478	839541	839604	839667	839731
692	840106	840169	840232	840295	840359
693	840733	840796	840859	840922	840986
694	841359	841423	841485	841548	841612
695	841983	842047	842109	842172	842236
696	842609	842672	842734	842797	842861
697	843233	843295	843357	843419	843482
698	843855	843918	843979	844042	844105
699	844477	844539	844601	844664	844727

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	6	7	8	9	D
399	826464	826518	826593	826658	65
046	827111	827175	827239	827305	65
692	827757	827822	827886	827951	65
338	828402	828467	828531	828595	64
982	829046	829111	829175	829239	64
625	829689	829754	829818	829882	64
268	830332	830396	830460	830525	64
909	830973	831037	831102	831166	64
549	831614	831678	831742	831806	64
185	832253	832317	832381	832445	64
828	832892	832956	833019	833083	64
466	833529	833593	833657	833721	64
103	834166	834229	834294	834357	64
739	834802	834866	834929	834993	64
373	835437	835500	835564	835627	63
007	836071	836134	836197	836261	63
641	836704	836767	836830	836894	63
273	837336	837399	837463	837525	63
904	837967	838030	838093	838156	63
534	838597	838660	838723	838786	63
164	839227	839289	839352	839415	63
792	839855	839918	839981	840043	63
419	840482	840545	840608	840671	63
049	841109	841172	841234	841297	63
672	841736	841797	841859	841922	63
297	842359	842422	842484	842547	62
921	842983	843046	843108	843170	62
544	843606	843669	843731	843793	62
166	844229	844291	844353	844415	62
788	844849	844912	844974	845036	62

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N	0	1	2	3	4
700	845098	845160	845222	845284	845346
701	845718	845779	845842	845904	845966
702	846337	846399	846461	846523	846585
703	846955	847017	847079	847141	847203
704	847573	847634	847696	847758	847820
705	848189	848251	848312	848374	848436
706	848805	848866	848928	848989	849051
707	849419	849481	849542	849604	849666
708	850033	850095	850156	850217	850279
709	850646	850707	850769	850829	850891
710	851258	851319	851381	851442	851504
711	851869	851931	851992	852053	852115
712	852479	852541	852602	852663	852725
713	853089	853150	853211	853272	853334
714	853698	853759	853819	853881	853942
715	854306	854367	854428	854488	854549
716	854913	854974	855034	855095	855156
717	855519	855579	855640	855701	855762
718	856124	856185	856245	856306	856367
719	856729	856789	856849	856910	856971
720	857332	857393	857453	857513	857574
721	857935	857995	858056	858116	858177
722	858537	858597	858657	858718	858778
723	859138	859198	859258	859318	859379
724	859739	859799	859859	859919	859979
725	860338	860398	860458	860518	860578
726	860937	860996	861056	861116	861176
727	861534	861594	861654	861714	861774
728	862131	862191	862251	862310	862370
729	862728	862787	862847	862906	862966

The Table of Logarithmes.

	6	7	8	9	D
08	845470	845532	845594	845655	62
28	846089	846151	846213	846275	62
46	846708	846769	846832	846894	62
64	847326	847388	847449	847511	62
81	847943	848004	848067	848128	62
97	848559	848620	848682	848743	62
12	849174	849235	849297	849358	61
26	849788	849849	849911	849972	61
39	850401	850462	850524	850585	61
53	851014	851075	851136	851197	61
64	851625	851686	851747	851809	61
75	852236	852297	852358	852419	61
85	852846	852907	852968	853029	61
94	853455	853516	853577	853637	61
02	854063	854124	854185	854245	61
18	854670	854731	854792	854852	61
35	855277	855337	855398	855459	61
52	855882	855943	856003	856064	61
68	856487	856548	856608	856668	60
85	857091	857152	857212	857272	60
93	857694	857755	857815	857875	60
06	858297	858357	858417	858477	60
28	858898	858958	859018	859078	60
48	859499	859559	859619	859679	60
68	860098	860158	860218	860278	60
88	860697	860757	860817	860877	60
06	861295	861355	861415	861475	60
24	861893	861952	862012	862072	60
40	862489	862549	862608	862668	60
56	863085	863144	863204	863263	60

The Table of Logarithmes.

N	0	1	2	3
730	863323	863382	863442	863501
731	863917	863977	864036	864096
732	864511	864570	864629	864689
733	865104	865163	865222	865282
734	865696	865755	865814	865874
735	866287	866346	866405	866465
736	866878	866937	866996	867055
737	867467	867526	867585	867644
738	868056	868115	868174	868233
739	868643	868703	868762	868821
740	869232	869290	869349	869408
741	869818	869877	869935	869994
742	870404	870462	870521	870579
743	870989	871047	871106	871164
744	871573	871631	871689	871748
745	872156	872215	872273	872331
746	872739	872797	872855	872913
747	873321	873379	873437	873495
748	873902	873959	874018	874076
749	874482	874539	874598	874656
750	875061	875119	875177	875235
751	875639	875698	875756	875813
752	876218	876276	876333	876391
753	876795	876853	876910	876968
754	877371	877429	877487	877544
755	877947	878004	878062	878119
756	878522	878579	878637	878694
757	879096	879153	879211	879268
758	879669	879726	879784	879841
759	880242	880299	880356	880413

The Table of Logarithmes.

1	6	7	8	9	10
861	862679	863739	863799	863858	59
862	864274	864333	864392	864451	59
863	864867	864926	864985	865045	59
864	865459	865519	865578	865637	59
865	866051	866110	866169	866228	59
866	866642	866701	866755	866819	59
867	867232	867291	867349	867409	59
868	867821	867879	867938	867998	59
869	868409	868468	868527	868586	59
870	868997	869056	869114	869173	59
871	869584	869642	869701	869759	59
872	870169	870228	870287	870345	59
873	870755	870813	870872	870930	58
874	871339	871398	871456	871515	58
875	871923	871981	871039	872098	58
876	872506	872564	872622	872681	58
877	873088	873146	873204	873264	58
878	873669	873727	873785	873844	58
879	874249	874308	874366	874424	58
880	874829	874888	874945	875003	58
881	875409	875466	875524	875582	58
882	875987	876045	876102	876160	58
883	876564	876622	876679	876737	58
884	877141	877199	877256	877314	58
885	877717	877774	877832	877889	58
886	878292	878349	878407	878464	57
887	878866	878924	878981	879039	57
888	879459	879497	879555	879612	57
889	880013	880070	880127	880185	57
890	880585	880642	880699	880756	57

The Table of Logarithms.

N	0	1	2	3
760	880814	880871	880928	880985
761	881385	881442	881499	881556
762	881955	882012	882069	882126
763	882525	882581	882638	882695
764	883093	883150	883207	883264
765	883661	883718	883775	883832
766	884229	884285	884342	884399
767	884795	884852	884909	884965
768	885361	885418	885474	885531
769	885926	885983	886039	886096
770	886491	886547	886604	886659
771	887054	887111	887167	887223
772	887617	887674	887720	887786
773	888179	888236	888292	888348
774	888741	888797	888853	888909
775	889302	889358	889414	889469
776	889862	889918	889974	890029
777	890421	890477	890533	890589
778	890979	891035	891091	891147
779	891537	891593	891649	891705
780	892095	892150	892206	892262
781	892651	892707	892762	892818
782	893207	893262	893318	893373
783	893762	893817	893873	893928
784	894316	894371	894427	894482
785	894869	894925	894980	895036
786	895423	895478	895533	895588
787	895975	896029	896085	896140
788	896526	896581	896636	896692
789	897077	897132	897187	897242

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	6	7	8	9	NE
881	099881156	8812134	881271	881328	57
881	60981727	881784	881841	881898	57
881	29882197	882354	882411	882468	57
881	09882866	882913	882979	883037	57
881	77883434	883491	883548	883605	57
881	45884002	884059	884115	884172	57
881	12884569	884615	884681	884738	57
881	78885135	885192	885248	885305	57
881	44885700	885757	885812	885869	57
881	66886265	886321	886378	886434	56
881	73886825	886885	886941	886998	56
881	36887392	887445	887501	887561	56
881	98887955	888011	888067	888123	56
881	60888516	888573	888629	888685	56
881	21889077	889134	889189	889246	56
881	82889636	889694	889749	889806	56
881	41890197	890253	890309	890365	56
881	00890756	890812	890868	890924	56
881	59891314	891370	891426	891482	56
881	16891872	891928	891982	892039	56
881	73892429	892484	892539	892595	56
881	23892985	893040	893096	893151	56
881	84893539	893595	893651	893706	56
881	35894094	894149	894205	894261	55
881	95894648	894704	894759	894814	55
881	46895201	895257	895312	895367	55
881	95895754	895809	895864	895919	55
881	71896300	896361	896416	896471	55
881	22896857	896912	896967	897022	55
881	81897407	897462	897517	897572	55

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N	0	1	2	3	4
790	897627	897682	897737	897792	897847
791	898176	898231	898286	898341	898396
792	898725	898780	898835	898890	898945
793	899273	899328	899383	899437	899492
794	899821	899875	899929	899984	900038
795	900367	900422	900476	900531	900585
796	900913	900958	901012	901067	901121
797	901458	901513	901567	901622	901676
798	902003	902057	902112	902166	902220
799	902547	902601	902655	902709	902763
800	903089	903144	903199	903253	903307
801	903633	903687	903741	903795	903849
802	904174	904229	904283	904337	904391
803	904716	904769	904824	904878	904932
804	905256	905310	905364	905418	905472
805	905796	905849	905904	905958	906012
806	906335	906389	906443	906497	906551
807	906874	906927	906981	907035	907089
808	907411	907465	907519	907573	907627
809	907945	908002	908056	908109	908163
810	908485	908539	908592	908646	908700
811	909021	909074	909128	909181	909235
812	909556	909609	909663	909716	909770
813	910091	910144	910197	910251	910304
814	910624	910678	910731	910784	910838
815	911158	911211	911263	911317	911370
816	911690	911743	911797	911849	911903
817	912222	912275	912323	912381	912434
818	912753	912806	912859	912913	912966
819	913284	913337	913389	913443	913496

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	6	7	8	9	D
897	902897957	898012	898067	898122	55
898	51898506	898561	898615	898670	55
899	999899054	899109	899164	899218	55
899	547899602	899656	899711	899766	55
900	094900149	900203	900258	900312	55
900	640900655	900749	900804	900859	55
901	186901240	901295	901349	901404	55
901	731901785	901839	901894	901948	54
902	275902329	902384	902438	902492	54
902	818902873	902927	902981	903036	54
903	361903416	903469	903524	903578	54
903	964903956	904012	904066	904120	54
904	445904499	904553	904607	904661	54
904	986905039	905094	905148	905202	54
905	526905580	905634	905688	905742	54
906	066906119	906173	906227	906281	54
906	604906658	906712	906766	906819	54
907	143907196	907250	907304	907358	54
907	680907734	907787	907841	907895	54
908	217908270	908324	908378	908431	54
909	753908807	908860	908914	908967	54
910	289909342	909396	909449	909503	54
910	823909877	909930	909984	910037	53
911	358910411	910464	910518	910571	53
911	891910944	910998	911051	911104	53
912	424911477	911530	911584	911637	53
912	956912009	912063	912116	912169	53
913	488912541	912594	912647	912700	53
913	019913072	913125	913178	913231	53
914	549913602	913655	913708	913761	53

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N	0	1	2	3
820	913814	913867	913919	913973
821	914343	914396	914449	914502
822	914872	914925	914977	915030
823	915399	915453	915505	915558
824	915927	915979	916033	916085
825	916454	916507	916559	916612
826	916980	917033	917085	917138
827	917506	917558	917611	917663
828	918030	918083	918135	918188
829	918555	918607	918659	918712
830	919078	919130	919183	919235
831	919601	919653	919706	919758
832	920123	920176	920228	920279
833	920645	920697	920749	920801
834	921166	921218	921270	921322
835	921686	921738	921790	921842
836	922206	922258	922310	922362
837	922725	922777	922829	922881
838	923244	923296	923348	923399
839	923762	923814	923865	923917
840	924279	924331	924383	924434
841	924796	924848	924899	924951
842	925312	925364	925415	925467
843	925828	925879	925931	925982
844	926343	926394	926445	926497
845	926857	926908	926959	927011
846	927370	927422	927473	927524
847	927883	927935	927986	928037
848	928396	928447	928498	928549
849	928908	928959	929009	929061

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	6	7	8	9	D
079	914132	914184	914237	914290	53
080	914660	914713	914766	914819	53
081	915189	915241	915294	915347	53
082	915716	915769	915822	915875	53
083	916243	916296	916349	916401	53
084	916769	916822	916875	916927	53
085	917295	917348	917400	917453	53
086	917820	917873	917925	917978	52
087	918345	918397	918449	918502	52
088	918869	918921	918973	919026	52
089	919392	919444	919496	919549	52
090	919914	919967	920019	920071	52
091	920436	920489	920541	920593	52
092	920958	921009	921062	921114	52
093	921478	921530	921582	921634	53
094	921998	922050	922102	922154	52
095	922518	922569	922622	922674	52
096	923037	923089	923140	923192	52
097	923555	923607	923658	923710	52
098	924072	924124	924176	924228	52
099	924589	924641	924693	924744	52
100	925106	925157	925209	925261	52
101	925621	925673	925725	925776	52
102	926137	926188	926239	926291	51
103	926651	926702	926754	926805	51
104	927165	927216	927268	927319	51
105	927678	927729	927781	927832	51
106	928191	928242	928293	928345	51
107	928703	928754	928805	928857	51
108	929215	929266	929317	929368	51

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N	0	1	2	3	4
850	929419	929470	929521	929572	929623
851	929929	929981	930032	930083	930134
852	930439	930491	930542	930592	930643
853	930949	930999	931051	931102	931153
854	931458	931509	931559	931610	931661
855	931966	932017	932068	932118	932169
856	932474	932524	932575	932626	932677
857	932981	933031	933082	933133	933184
858	933487	933538	933589	933639	933690
859	933993	934044	934094	934145	934196
860	934498	934549	934599	934649	934700
861	935003	935056	935104	935154	935205
862	935507	935558	935608	935658	935709
863	936011	936061	936111	936162	936213
864	936514	936564	936614	936665	936716
865	937016	937066	937117	937167	937218
866	937518	937568	937618	937668	937719
867	938019	938069	938119	938169	938220
868	938519	938569	938619	938669	938720
869	939019	939069	939119	939169	939220
870	939519	939569	939619	939669	939720
871	940019	940068	940118	940168	940219
872	940516	940566	940616	940666	940717
873	941014	941064	941114	941163	941214
874	941511	941561	941611	941660	941711
875	942008	942058	942107	942157	942208
876	942504	942554	942603	942653	942704
877	942999	943049	943099	943148	943199
878	943495	943544	943594	943643	943694
879	943989	944038	944088	944137	944188

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	6	7	8	∞	D
74	929725	929776	929827	929879	51
85	930236	930287	930338	930389	51
94	930745	930796	930847	930898	51
04	931254	931305	931356	931407	51
12	931762	931814	931865	931915	51
20	932271	932322	932372	932423	51
27	932778	932829	932879	932930	51
34	933285	933335	933386	933437	51
40	933791	933841	933892	933943	51
46	934296	934347	934397	934448	51
51	934801	934852	934902	934953	50
55	935306	935356	935406	935457	50
59	935809	935859	935910	935960	50
62	936313	936363	936413	936463	50
65	936815	936865	936916	936966	50
67	937317	937367	937418	937468	50
68	937819	937869	937919	937969	50
69	938319	938369	938419	938469	50
69	938819	938869	938919	938969	50
69	939319	939369	939419	939469	50
69	939819	939869	939918	939968	50
70	940317	940367	940417	940467	50
70	940815	940865	940915	940964	50
70	941313	941362	941412	941462	50
70	941809	941856	941909	941958	50
70	942306	942355	942405	942455	50
70	942801	942851	942901	942950	50
70	943297	943346	943396	943445	49
70	943791	943841	943890	943939	49
70	944285	944335	944384	944433	46

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N	0	1	2	3
880	944483	944532	944581	944621
881	944976	945025	945074	945124
882	945468	945518	945567	945616
883	945961	946009	946059	946108
884	946552	946501	946551	946599
885	946943	946992	947041	947090
886	947434	947483	947532	947581
887	947924	947973	948022	948070
888	948413	948462	948511	948559
889	948902	948951	948999	949048
890	949396	949439	949488	949536
891	949878	949926	949975	950024
892	950365	950414	950462	950511
893	950851	950900	950949	950997
894	951338	951386	951435	951483
895	951823	951872	951920	951969
896	952308	952356	952405	952453
897	952792	952841	952889	952938
898	953276	953325	953373	953421
899	953759	953808	953856	953905
900	954243	954291	954339	954387
901	954725	954773	954821	954869
902	955207	955255	955303	955351
903	955688	955736	955784	955832
904	956168	956216	956265	956313
905	956649	956697	956745	956793
906	957128	957176	957224	957272
907	957607	957655	957703	957751
908	958086	958134	958181	958229
909	958564	958612	958659	958707

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	6	7	8	9	D	
94	4729	944779	944828	944877	944927	49
94	5222	945272	945321	945370	945419	49
94	5715	945764	945813	945862	945912	49
94	6207	946256	946305	946354	946403	49
94	6698	946747	946796	946845	946894	49
94	7189	947238	947287	947336	947385	49
94	7679	947728	947777	947826	947875	49
94	8168	948217	948266	948315	948364	49
94	8657	948706	948755	948804	948853	49
94	9146	949195	949244	949292	949341	49
694	9633	949683	949731	949780	949829	49
448	10121	950170	950219	950267	950316	49
199	10608	950657	950706	950754	950803	49
079	1095	951143	951192	951240	951289	49
339	11380	951629	951677	951726	951775	49
699	11866	952114	952163	952211	952259	48
539	12350	952599	952647	952696	952744	48
389	12834	953083	953131	953179	953228	48
219	13318	953566	953615	953663	953711	48
059	13801	954049	954099	954146	954194	48
879	14284	954532	954580	954628	954677	48
869	14766	955014	955062	955110	955158	48
351	15247	955495	955543	955592	955639	48
832	15728	955976	956024	956072	956120	48
313	16209	956457	956505	956553	956601	48
793	16688	956936	956984	957032	957080	48
272	17168	957416	957464	957512	957559	48
751	17647	957894	957942	957990	958038	48
229	18125	958373	958421	958468	958516	48
707	18602	958850	958898	958946	958994	48

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N	0	1	2	3	4
910	959041	959089	959137	959185	959233
911	959518	959566	959614	959661	959709
912	959995	960042	960090	960138	960185
913	960471	960518	960566	960613	960660
914	960946	960994	961041	961089	961136
915	961421	961469	961516	961563	961610
916	961895	961943	961990	962038	962085
917	962369	962417	962464	962511	962558
918	962842	962889	962937	962985	963032
919	963315	963363	963410	963457	963504
920	963788	963835	963882	963929	963976
921	964259	964307	964354	964401	964448
922	964731	964778	964825	964872	964919
923	965202	965249	965296	965343	965390
924	965672	965719	965766	965813	965860
925	966142	966189	966239	966283	966327
926	966611	966658	966705	966752	966799
927	967079	967127	967173	967220	967267
928	967548	967595	967642	967688	967735
929	968016	968062	968109	968156	968203
930	968483	968529	968576	968623	968670
931	968949	968996	969043	969089	969136
932	969416	969463	969509	969556	969603
933	969882	969928	969975	970021	970068
934	970347	970393	970439	970486	970533
935	970812	970858	970904	970951	970997
936	971276	971322	971369	971415	971462
937	971739	971786	971832	971879	971925
938	972203	972249	972295	972342	972389
939	972666	972712	972758	972804	972851

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	6	7	8	9	D
279	959328	959375	959423	959471	48
757	959804	959852	959899	959947	48
233	960280	960328	960376	960423	48
709	960756	960804	960851	960899	48
184	961231	961279	961326	961374	47
656	961706	961753	961801	961848	47
132	962179	962227	962275	962322	47
606	962653	962701	962748	962795	47
979	963126	963174	963221	963268	47
552	963599	963646	963693	963741	47
224	964071	964118	964165	964212	47
895	964542	964589	964637	964684	47
666	965013	965061	965108	965155	47
437	965484	965531	965578	965624	47
906	965954	966001	966048	966095	47
76	966423	966470	966517	966564	47
45	966892	966939	966986	967033	47
14	967361	967408	967454	967501	47
782	967829	967875	967922	967969	47
49	968286	968343	968389	968436	47
719	968763	968809	968856	968902	47
282	969229	969276	969323	969369	47
49	969695	969741	969789	969835	47
14	970161	970207	970254	970300	47
79	970626	970672	970719	970765	46
44	971090	971137	971183	971229	46
08	971554	971601	971647	971693	49
71	972018	972064	972110	972157	46
34	972481	972527	972573	972619	46
67	972943	972989	973039	973082	46

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N	0	1	2	3	4
940	973128	973174	973220	973266	973312
941	973589	973636	973682	973728	973774
942	974050	974097	974143	974189	974235
943	974512	974558	974604	974649	974695
944	974972	975018	975064	975109	975155
945	975432	975478	975524	975569	975615
946	975891	975937	975983	976029	976075
947	976349	976396	976442	976488	976534
948	976808	976854	976899	976946	976992
949	977266	977312	977358	977403	977449
950	977724	977769	977815	977861	977907
951	978181	978226	978272	978317	978363
952	978637	978683	978728	978774	978820
953	979093	979138	979184	979229	979275
954	979548	979594	979639	979685	979731
955	980003	980049	980094	980139	980185
956	980458	980503	980549	980594	980640
957	980912	980957	981003	981048	981094
958	981366	981411	981456	981501	981547
959	981812	981864	981909	981954	982000
960	982271	982316	982362	982407	982453
961	982723	982769	982814	982859	982905
962	983175	983220	983265	983310	983356
963	983626	983671	983716	983762	983807
964	984077	984122	984167	984212	984258
965	984527	984572	984617	984662	984708
966	984977	985022	985067	985112	985158
967	985426	985471	985516	985561	985607
968	985875	985920	985965	986010	986056
969	986324	986369	986413	986458	986504

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	6	7	8	9	D
973	359	973405	973451	973497	973543
973	820	973866	973913	973959	974005
974	281	974327	974374	974419	974466
974	742	974788	974834	974879	974926
975	202	975248	975294	975339	975386
975	662	975707	975753	975799	975845
976	121	976167	976212	976258	976304
976	579	976625	976671	976717	976763
976	037	977083	977129	977175	977220
977	495	977541	977586	977632	977678
977	952	977998	978042	978089	978135
978	409	978454	978500	978546	978591
978	865	978911	978956	979002	979047
979	321	979366	979412	979457	979503
979	776	979821	979867	979912	979958
980	231	980276	980322	980367	980412
980	685	980730	980776	980821	980867
981	139	981184	981229	981275	981320
981	592	981637	981683	981728	981773
982	045	982090	982135	982181	982226
982	497	982543	982588	982633	982678
983	949	982994	983039	983085	983129
983	401	983446	983490	983536	983581
984	852	983897	983942	983987	984032
984	302	984347	984392	984437	984482
985	752	984797	984842	984887	984932
985	202	985247	985292	985337	985382
986	651	985696	985741	985787	985830
986	109	986144	986189	986234	986279
987	558	986593	986637	986682	986727

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N	0	1	2	3
970	986772	986817	986861	986906
971	987219	987264	987309	987353
972	987666	987711	987756	987800
973	988113	988157	988202	988247
974	988559	988604	988648	988693
975	989005	989049	989094	989138
976	989449	989494	989539	989584
977	989895	989939	989983	990028
978	990339	990383	990428	990472
979	990783	990827	990871	990916
980	991226	991270	991315	991359
981	991669	991713	991758	991802
982	992111	992156	992199	992244
983	992554	992598	992642	992686
984	992995	993039	993083	993127
985	993436	993480	993524	993568
986	993877	993921	993965	994009
987	994117	994361	994405	994449
988	994356	994801	994845	994889
989	995196	995240	995284	995328
990	995635	995679	995723	995764
991	996074	996117	996161	996205
992	996512	996555	996599	996643
993	996949	996993	997037	997080
994	997389	997430	997474	997517
995	997823	997867	997910	997954
996	998259	998303	998347	998390
997	998695	998739	998783	998826
998	999133	999174	999218	999261
999	999565	999609	999652	999696

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	5	6	7	8	9	D
986	996	987040	987085	987129	987175	45
987	443	987488	987532	987577	987622	45
988	889	987934	987979	988024	988068	45
989	336	988381	988425	988469	988514	45
990	782	988826	988871	988916	988960	45
991	227	989272	989316	989361	989405	45
992	672	989717	989761	989806	989850	44
993	117	990161	990206	990250	990294	44
994	561	990605	990649	990694	990738	44
995	004	991049	991093	991137	991182	44
996	448	991492	991536	991580	991625	44
997	890	991935	991979	992023	992067	44
998	333	992377	992421	992465	992509	44
999	774	992819	992863	992907	992951	44
1000	216	993259	993304	993348	993392	44
1001	57	993701	993745	993789	993833	44
1002	97	994141	994185	994229	994273	44
1003	37	994581	994625	994669	994713	44
1004	77	995021	995065	995108	995152	44
1005	16	995459	995504	995547	995591	44
1006	54	995898	995942	995986	996029	44
1007	93	996337	996380	996424	996468	44
1008	31	996774	996818	996862	996906	44
1009	68	997212	997255	997299	997343	44
1010	05	997648	997692	997736	997779	44
1011	41	998085	998129	998172	998216	44
1012	77	998521	998564	998608	998652	44
1013	12	998959	998999	999043	999087	44
1014	48	999392	999435	999479	999522	44
1015	83	999826	999869	999913	999957	43

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**A
TABLE
OF
Artificial Sines
AND
ANGENTS
To Every
DEGREE and MINUTE
OF THE
QUADRANT.**

Common Radius being 10,000,000.

L O N D O N,

Printed in the Year MDCCXIV.

Degree 0.

M Sine | Co-sine | Tangent | Co-tang

0.000000 | 10.000000 | 0.000000 | Infinite

1 5.463726	9.999999	5.463726	13.536273
2 6.764756	9.999999	6.764756	13.235243
3 6.940847	9.999999	6.940847	13.059111
4 7.065786	9.999999	7.065786	12.934811
5 7.162696	9.999999	7.162696	12.837731

6 7.241877	9.999999	7.241878	12.758111
7 7.308824	9.999999	7.308825	12.691111
8 7.366816	9.999999	7.366817	12.633111
9 7.417968	9.999999	7.417970	12.582111
10 7.463726	9.999998	7.563727	12.536111

11 7.505118	9.999998	7.505120	12.494111
12 7.442906	9.999997	7.542909	12.455111
13 7.577668	9.999997	7.577272	12.422111
14 7.609853	9.999996	7.609857	12.390111
15 7.639816	9.999996	7.639826	12.360111

16 7.667844	9.999995	7.667845	12.331111
17 7.694173	9.999995	7.694179	12.303111
18 7.718977	9.999994	7.719003	12.278111
19 7.742477	9.999993	7.742481	12.255111
20 7.764754	9.999993	7.764761	12.233111

21 7.785943	9.999992	7.785951	12.211111
22 7.806146	9.999991	7.806146	12.191111
23 7.825451	9.999990	7.825460	12.171111
24 7.843934	9.999989	7.843944	12.151111
25 7.861662	9.999989	7.861671	12.131111

26 7.878695	9.999988	7.878708	12.111111
27 7.895085	9.999987	7.895099	12.091111
28 7.910879	9.999986	7.910894	12.081111
29 7.926119	9.999985	7.926134	12.071111
30 7.940842	9.999983	7.940858	12.059111

| Co-sine | Sine | | Co-tang | Tang

Degree 89.

Degree 80.

Sine	Co-sine.	Tangent	Co-tang.
940842	7.999983	17.940858	1.2059143
95082	9.999982	7.955100	12.044900
958870	9.999981	7.968889	12.031111
982233	9.999980	7.982253	12.017747
995198	9.999978	7.995215	12.004781
007787	9.999978	7.007810	11.992191
20021	9.999976	8.010044	11.979956
31919	9.999975	8.031945	11.968055
43101	9.999973	8.043527	11.956473
54781	9.999972	8.054809	11.945181
65776	9.999971	8.065866	11.934191
06500	9.999969	8.076531	11.923469
18665	9.999968	8.086997	11.913003
297183	9.999966	8.097217	11.902783
407167	9.999964	8.107203	11.892797
516926	9.999963	8.116963	11.883037
62641	9.999961	8.126510	11.873490
735810	9.999959	8.135853	11.864149
84953	9.999958	8.144906	11.855004
95907	9.999956	8.153952	11.846048
0681	9.999954	8.162737	11.837273
1280	9.999952	8.171328	11.828672
23713	9.999950	8.179763	11.820237
347985	9.999948	8.188036	11.811964
456102	9.999946	8.196156	11.803844
564070	9.999944	8.204126	11.795874
671895	9.999942	8.211953	11.788027
7781	9.999940	8.219641	11.780359
88134	9.999938	8.227195	11.772805
98557	9.999936	8.234621	11.765379
0855	9.999934	8.241921	11.758079

Sine Sine | Co-tang. Tangent M

Degree 89.

Degree 1.

M	Sine	Co-fine	Tangent	Co-tan
0	8.24185519	9.9999341	8.24192111	7.16780
1	8.249033	9.999932	8.249102	7.17508
2	8.256094	9.999929	8.256165	7.17438
3	8.263042	9.999927	8.263115	7.17368
4	8.269881	9.999925	8.269956	7.17298
5	8.276614	9.999922	8.276691	7.17228
6	8.283243	9.999920	8.283323	7.17158
7	8.289773	9.999918	8.289856	7.17088
8	8.296207	9.999915	8.296292	7.17018
9	8.302546	9.999913	8.302634	7.16948
10	8.308794	9.999910	8.308884	7.16878
11	8.314954	9.999907	8.315046	7.16808
12	8.321027	9.999905	8.321122	7.16738
13	8.327016	9.999902	8.327114	7.16668
14	8.332924	9.999899	8.333025	7.16598
15	8.338753	9.999897	8.338856	7.16528
16	8.344504	9.999894	8.344610	7.16458
17	8.350180	9.999891	8.350289	7.16388
18	8.355783	9.999888	8.355895	7.16318
19	8.361315	9.999885	8.361430	7.16248
20	8.366777	9.999882	8.366895	7.16178
21	8.372171	9.999879	8.372292	7.16108
22	8.377497	9.999876	8.377622	7.16038
23	8.382762	9.999873	8.382889	7.15968
24	8.387962	9.999870	8.388092	7.15898
25	8.393101	9.999867	8.393234	7.15828
26	8.398179	9.999864	8.398315	7.15758
27	8.403199	9.999861	8.403338	7.15688
28	8.408161	9.999858	8.408304	7.15618
29	8.413068	9.999854	8.413213	7.15548
30	8.417919	9.999851	8.418068	7.15478
Co-fine		Sine	Co-tang.	Tan

Degree 88.

Degree 1.

Sine	Co-sine	Tangent	Co-tang.
1791	9.9998511	8.418068	11.581932
2271	9.999848	8.422869	11.577131
2746	9.999844	8.427618	11.572382
3215	9.999841	8.432315	11.567685
3680	9.999838	8.436962	11.563038
4139	9.999834	8.441560	11.558442
4594	9.999831	8.446110	11.553902
5040	9.999827	8.450613	11.549387
5489	9.999824	8.455070	11.544930
5931	9.999820	8.459481	11.540519
6365	9.999816	8.463849	11.536151
6798	9.999812	8.468172	11.531828
7226	9.999809	8.472454	11.527546
7649	9.999805	8.476693	11.523307
8069	9.999801	8.480892	11.519108
8487	9.999797	8.485050	11.514940
8896	9.999794	8.48917	11.510830
9296	9.999790	8.493250	11.506750
9697	9.999786	8.497295	11.502707
10080	9.999782	8.501298	11.498702
10485	9.999778	8.505267	11.494733
10874	9.999774	8.509200	11.490800
11267	9.999769	8.513098	11.486902
11626	9.999765	8.516961	11.483039
11951	9.999761	8.520790	11.479210
12343	9.999756	8.524586	11.475414
12702	9.999753	8.528349	11.471651
13028	9.999748	8.532080	11.467920
13323	9.999744	8.535779	11.464221
13618	9.999740	8.539447	11.460553
13919	9.999735	8.543084	11.456916
Sine	Co-sine	Tangent	Co-tang.

Degree 88.

Q

Degree 2.

Vl	Sine	Co-sine	Tangent	Co-tang
c	3.5428199.999735		8.543084	11.4569
1	8.546422	9.999731	8.546691	11.4533
2	8.549945	9.999726	8.550268	11.4497
3	8.553558	9.999722	8.553817	11.4461
4	8.557054	9.999717	8.557336	11.4426
5	8.560540	9.999713	8.560827	11.4391
6	8.563995	9.999708	8.564291	11.4355
7	8.567431	9.999703	8.567727	11.4320
8	8.570836	9.999699	8.571137	11.4284
9	8.574214	9.999694	8.574520	11.4249
10	8.577566	9.999689	8.577877	11.4213
11	8.580892	9.999685	8.581208	11.4178
12	8.584193	9.999680	8.584514	11.4142
13	8.587469	9.999675	8.587795	11.4107
14	8.590721	9.999670	8.591051	11.4071
15	8.593948	9.999665	8.594283	11.4036
16	8.597152	9.999660	8.597492	11.4000
17	8.600332	9.999655	8.600677	11.3964
18	8.603488	9.999650	8.603838	11.3929
19	8.606622	9.999645	8.606978	11.3893
20	8.609734	9.999640	8.610094	11.3858
21	8.612823	9.999635	8.613189	11.3822
22	8.615891	9.999629	8.616262	11.3787
23	8.618937	9.999624	8.619313	11.3751
24	8.621967	9.999619	8.622343	11.3716
25	8.624965	9.999614	8.625352	11.3680
26	8.627948	9.999608	8.628340	11.3645
27	8.630911	9.999603	8.631308	11.3609
28	8.633854	9.999597	8.634456	11.3574
29	8.636776	9.999592	8.637184	11.3538
30	8.639679	9.999586	8.640093	11.3503
Co-sine		Sine	Co-tang	Tan

Degree 87.

Degree 2.

Sine	Co sine	Tangent	Co-tang.
39679	9.999586	18.640093	11.359907
42563	9.999581	8.642982	11.357017
45428	9.999575	8.645653	11.354147
48274	9.999570	8.648704	11.351296
51102	9.999564	8.651538	11.348463
53911	9.999558	8.654352	11.345648
56702	9.999553	8.657149	11.342851
59475	9.999547	8.659928	11.340272
62230	9.999541	8.662689	11.337311
64968	9.999535	8.665433	11.334567
67689	9.999529	8.668160	11.331840
70393	9.999523	8.670869	11.329130
73080	9.999518	8.673563	11.326437
75751	9.999512	8.676239	11.323761
78405	9.999506	8.678899	11.321100
81043	9.999499	8.681544	11.318456
83665	9.999493	8.684172	11.315828
86272	9.999487	8.686784	11.313216
88892	9.999481	8.689381	11.310619
91438	9.999475	8.691963	11.308037
93998	9.999469	8.694529	11.305471
96543	9.999462	8.697081	11.302919
99073	9.999456	8.699617	11.300383
101589	9.999450	8.702135	11.297861
103409	9.999443	8.704646	11.295354
105176	9.999437	8.707135	11.292860
106941	9.999431	8.709618	11.290381
108707	9.999424	8.712083	11.287917
110452	9.999418	8.714534	11.285466
112183	9.999411	8.716972	11.283028
113900	9.999404	8.719396	11.280604

Ta | Sine | Co-tang. | Tangent: | M

Degree 87.

Degree 31.

Sine	Co-sine	Tangent	Co-tan
0 8.718800	9.999404	18.719346	11.2806
1 8.721204	9.999398	8.721806	11.278
2 8.723595	9.999391	8.724254	11.275
3 8.725972	9.999384	8.726588	11.272
4 8.728336	9.999378	8.728959	11.270
5 8.730688	9.999371	8.731317	11.268
6 8.733027	9.999364	8.733663	11.266
7 8.735354	9.999357	8.735996	11.264
8 8.737667	9.999350	8.738317	11.261
9 8.739969	9.999343	8.740626	11.259
10 8.742259	9.999336	8.742922	11.257
11 8.744536	9.999329	8.745207	11.254
12 8.746801	9.999322	8.747479	11.252
13 8.745955	9.999315	8.749740	11.250
14 8.751297	9.999308	8.751989	11.247
15 8.753528	9.999301	8.754227	11.245
16 8.755747	9.999294	8.756453	11.243
17 8.757955	9.999286	8.758668	11.240
18 8.760151	9.999279	8.760872	11.238
19 8.762337	9.999272	8.763065	11.236
20 8.764511	9.999265	8.765246	11.233
21 8.766675	9.999257	8.767417	11.231
22 8.768828	9.999250	8.769578	11.229
23 8.770970	9.999242	8.771727	11.227
24 8.773101	9.999235	8.773866	11.224
25 8.775223	9.999227	8.775995	11.222
26 8.777333	9.999220	8.778114	11.220
27 8.779434	9.999212	8.780222	11.218
28 8.781524	9.999204	8.782320	11.216
29 8.783605	9.999197	8.784404	11.214
30 8.785675	9.999189	8.786486	11.212
Co-sine		Sine	Co-tang.

Degree 86.

Degree 3.

Sine	Co-sine	Tangent	Co-tang.
785675	9 999185	18.786486	11.213514
787736	9.999181	8.781554	11.211446
789787	9.999174	8.790613	11.209387
791828	9.999166	8.792662	11.207338
793859	9.999158	8.794701	11.205289
795881	9.999150	8.796731	11.203239
797894	9.999142	8.798752	11.201248
799897	9.999134	8.800763	11.199237
801891	9.999126	8.802765	11.197235
803876	9.999118	8.804758	11.195242
805852	9.999110	8.806742	11.193258
807819	9.999102	8.808717	11.191283
809777	9.999094	8.810683	11.189317
811726	9.999086	8.812641	11.187359
813667	9.999077	8.814589	11.185411
815598	9.999069	8.816529	11.183471
817522	9.999061	8.818461	11.181539
819436	9.999052	8.820384	11.179616
821342	9.999044	8.822298	11.177702
823240	9.999036	8.824205	11.175794
825130	9.999027	8.826103	11.173897
827011	9.999019	8.827992	11.172008
828884	9.999010	8.829874	11.170126
830749	9.999002	8.831748	11.168252
832606	9.998993	8.833613	11.166377
834456	9.998984	8.835471	11.164529
836297	9.998976	8.837321	11.162679
838130	9.998967	8.839162	11.160837
839956	9.998958	8.840998	11.159002
841774	9.998940	8.842825	11.157175
843585	9.998941	8.844644	11.155356

Sine | Co-sine | Tangent | Co-tang.

Degree 86.

Degree 4.

M	Sine	Co sine	Tangent	Co tang
0	8.843584	9.998941	8.844644	11.15533
1	8.845387	9.998931	8.846455	11.15534
2	8.847183	9.998923	8.848240	11.15517
3	8.848971	9.998914	8.850057	11.14990
4	8.850751	9.998905	8.851846	11.14811
5	8.852525	9.998896	8.853628	11.14632
6	8.854291	9.998887	8.855403	11.14453
7	8.856049	9.998878	8.857171	11.14274
8	8.857801	9.998869	8.858932	11.14100
9	8.859546	9.998860	8.860686	11.13931
10	8.861283	9.998851	8.862433	11.13756
11	8.863014	9.998842	8.864173	11.13581
12	8.864738	9.998832	8.865906	11.13406
13	8.866454	9.998823	8.867632	11.13231
14	8.868165	9.998813	8.869351	11.13056
15	8.869868	9.998804	8.871064	11.12881
16	8.871565	9.998795	8.872750	11.12706
17	8.873255	9.998785	8.874469	11.12531
18	8.874938	9.998776	8.876162	11.12356
19	8.876615	9.998766	8.877849	11.12181
20	8.878285	9.998757	8.879529	11.12006
21	8.879949	9.998747	8.881202	11.11831
22	8.881607	9.998738	8.882896	11.11656
23	8.883258	9.998728	8.884530	11.11481
24	8.884903	9.998718	8.886185	11.11306
25	8.886542	9.998708	8.887833	11.11131
26	8.888174	9.998699	8.889476	11.10956
27	8.889801	9.998689	8.891112	11.10781
28	8.891421	9.998679	8.892742	11.10606
29	8.893035	9.998669	8.894366	11.10431
30	8.894643	9.998659	8.895984	11.10256
Co sine		Sine	Co tang	Tang

Degree 85.

Degree 4.

Sine	Co-sine.	Tangent	Co-tang.
94642	9.998659	18.845984	11.104016
96246	9.998649	18.897596	11.102404
97842	9.998639	18.899202	11.100797
99432	9.998629	18.900803	11.099197
10107	9.998619	18.902398	11.097602
10256	9.998609	18.903987	11.096013
10416	9.998599	18.905570	11.094430
10573	9.998589	18.907147	11.092853
10729	9.998577	18.908719	11.091281
10885	9.998568	18.910285	11.089715
11040	9.998558	18.911846	11.088154
11194	9.998548	18.913401	11.086599
11348	9.998537	18.914951	11.085049
11502	9.998527	18.916498	11.083505
11655	9.998516	18.918034	11.081966
11807	9.998506	18.919568	11.080432
11959	9.998495	18.921096	11.078904
12110	9.998485	18.922619	11.077381
12261	9.998474	18.924136	11.075864
12412	9.998464	18.925649	11.074351
12560	9.998453	18.927156	11.072844
12710	9.998442	18.928658	11.071344
12857	9.998431	18.930155	11.069845
13006	9.998421	18.931647	11.068353
13154	9.998410	18.933134	11.066866
13301	9.998399	18.934616	11.065384
13448	9.998388	18.936093	11.063907
13592	9.998377	18.937565	11.062435
13739	9.998366	18.939032	11.060968
13880	9.998355	18.940494	11.059506
14026	9.998344	18.941952	11.058048

Sine | Sine | Co-tang. | Tangent |

Degree 85.

Degree 5.

M	Sine	Co-sine	Tangent	Co-tang
0	8.940296	9.998344	18.94952	11.05048
1	8.941738	9.998111	18.943404	11.056596
2	8.943174	9.997882	18.944852	11.053148
3	8.944606	9.997651	18.946291	11.049709
4	8.946034	9.997420	18.947734	11.046271
5	8.947456	9.997189	18.949168	11.042833
6	8.948814	9.996957	18.950597	11.039395
7	8.950287	9.996726	18.952021	11.035957
8	8.951696	9.996495	18.953441	11.032519
9	8.953099	9.996263	18.954856	11.029081
10	8.954499	9.996032	18.956267	11.025643
11	8.955804	9.995800	18.957674	11.022205
12	8.957284	9.995569	18.959075	11.018767
13	8.958670	9.995337	18.960472	11.015329
14	8.960052	9.995106	18.961866	11.011891
15	8.961429	9.994874	18.963252	11.008453
16	8.962801	9.994643	18.964639	11.005015
17	8.964170	9.994411	18.966019	11.001577
18	8.965534	9.994179	18.967394	11.008139
19	8.966893	9.993948	18.968766	11.004701
20	8.968249	9.993716	18.970133	11.001263
21	8.969606	9.993484	18.971495	11.007825
22	8.970947	9.993252	18.972855	11.004387
23	8.972289	9.993020	18.974209	11.000949
24	8.973626	9.992788	18.975560	11.007511
25	8.974962	9.992556	18.976906	11.004073
26	8.976293	9.992324	18.978248	11.000635
27	8.977619	9.992092	18.979586	11.007197
28	8.978941	9.991860	18.980921	11.003759
29	8.980259	9.991628	18.982251	11.000321
30	8.981573	9.991396	18.983577	11.006883
Co-sine		Sine	Co-tang.	Tang

Degree 84.

Degree 5.

Sine	Co-sine	Tangent	Co-tang.
1573	9.997995	18.983577	11.016423
2883	9.997984	8.984899	11.015101
4189	9.997971	8.986217	11.013783
5491	9.997959	8.987532	11.012468
6789	9.997947	8.988842	11.011158
8083	9.997935	8.990149	11.009851
9374	9.997922	8.991451	11.008549
10660	9.997910	8.992750	11.007250
11943	9.997897	8.994045	11.005955
13228	9.997885	8.995337	11.004663
14497	9.997873	8.996624	11.003376
15768	9.997860	8.997908	11.002092
17036	9.997847	8.999188	11.000812
18299	9.997835	9.000465	10.999534
19560	9.997822	9.001738	10.998262
20816	9.997809	9.003007	10.996993
22069	9.997797	9.004272	10.995728
23318	9.997784	9.005534	10.994466
24563	9.997771	9.006792	10.993208
25805	9.997758	9.008047	10.991953
27044	9.997742	9.009298	10.990702
28278	9.997732	9.010546	10.989454
29510	9.997719	9.011790	10.988210
30737	9.997706	9.013031	10.986969
31962	9.997693	9.014268	10.985732
33182	9.997680	9.015502	10.984498
34399	9.997667	9.016732	10.983268
35613	9.997654	9.017959	10.982041
36824	9.997641	9.019183	10.980817
38031	9.997628	9.020403	10.979597
39235	9.997614	9.021620	10.978380
Sine	Co-tang.	Tangent.	M

Degree 84.

R

Degree 6.

Sine	Co-sine	Tangent	Co-tang
0.019225	0.997614	0.021620	10.97
1 0.020435	0.997601	0.022834	10.97
2 0.021632	0.997588	0.024044	10.97
3 0.022825	0.997574	0.025251	10.97
4 0.024016	0.997561	0.026455	10.97
5 0.025203	0.997548	0.027655	10.97
6 0.026386	0.997534	0.028852	10.97
7 0.027567	0.997520	0.030046	10.98
8 0.028744	0.997507	0.031237	10.98
9 0.029918	0.997493	0.032425	10.98
10 0.031089	0.997480	0.033609	10.98
11 0.032257	0.997466	0.034791	10.98
12 0.033421	0.997452	0.035969	10.98
13 0.034582	0.997439	0.037144	10.98
14 0.035741	0.997425	0.038316	10.98
15 0.036896	0.997411	0.039485	10.98
16 0.038048	0.997397	0.040651	10.99
17 0.039197	0.997383	0.041813	10.99
18 0.040342	0.997369	0.042973	10.99
19 0.041485	0.997355	0.044130	10.99
20 0.042625	0.997341	0.045284	10.99
21 0.043762	0.997327	0.046434	10.99
22 0.044895	0.997313	0.047582	10.99
23 0.046026	0.997299	0.048727	10.99
24 0.047154	0.997285	0.049869	10.99
25 0.048279	0.997271	0.051008	10.99
26 0.049400	0.997256	0.052144	10.99
27 0.050519	0.997242	0.053277	10.99
28 0.051635	0.997228	0.054408	10.99
29 0.052749	0.997214	0.055535	10.99
30 0.053859	0.997199	0.056660	10.99
Co-sine	Sine	Co-tang.	Tang.

Degree 83.

Degree 6.

Sine	Co-sine	Tangent	Co-tang.
9.997199	9.056640	10.943340	30
9.997185	9.057781	10.942219	29
9.997170	9.058900	10.941100	28
9.997156	9.060016	10.939984	27
9.997141	9.061130	10.938870	26
9.997127	9.062240	10.937760	25
9.997112	9.063348	10.936652	24
9.997098	9.064453	10.935547	23
9.997083	9.065556	10.934445	22
9.997068	9.066655	10.933345	21
9.997053	9.067752	10.932248	20
9.997039	9.068847	10.931153	19
9.997024	9.069938	10.930062	18
9.997009	9.071027	10.928973	17
9.996994	9.072113	10.927887	16
9.996979	9.073197	10.926803	15
9.996964	9.074278	10.925722	14
9.996949	9.075356	10.924644	13
9.996934	9.076432	10.923568	12
9.996919	9.077505	10.922495	11
9.996904	9.078576	10.921424	10
9.996886	9.079644	10.920356	9
9.996874	9.080710	10.919290	8
9.996858	9.081773	10.918227	7
9.996843	9.082833	10.917167	6
9.996823	9.083891	10.916109	5
9.996812	9.084947	10.915053	4
9.996797	9.085999	10.914000	3
9.996782	9.087050	10.912950	2
9.996766	9.088098	10.911902	1
9.996751	9.089144	10.910856	0
Sine	Co-sine	Tangent	M

Degree 83.

R 2





Degree 8.

M	Sine	Co-sine	Tangent	Co-tang.
0	9.143555	9.995751	19.147803	10.852197
1	9.144453	9.995735	9.148718	10.853282
2	9.145349	9.995717	9.149632	10.854367
3	9.146243	9.995699	9.150544	10.855452
4	9.147136	9.995681	9.151454	10.856537
5	9.148026	9.995664	9.152363	10.857622
6	9.148915	9.995646	9.153269	10.858707
7	9.149801	9.995628	9.154174	10.859792
8	9.150686	9.995610	9.155077	10.860877
9	9.151569	9.995592	9.155978	10.861962
10	9.152451	9.995573	9.156877	10.863047
11	9.153330	9.995555	9.157775	10.864132
12	9.154208	9.995537	9.158671	10.865217
13	9.155082	9.995519	9.159565	10.866302
14	9.155957	9.995501	9.160457	10.867387
15	9.156830	9.995482	9.161347	10.868472
16	9.157700	9.995464	9.162236	10.869557
17	9.158569	9.995446	9.163123	10.870642
18	9.159436	9.995427	9.164008	10.871727
19	9.160301	9.995409	9.164892	10.872812
20	9.161164	9.995390	9.165773	10.873897
21	9.162025	9.995372	9.166654	10.874982
22	9.162885	9.995353	9.167532	10.876067
23	9.163743	9.995334	9.168409	10.877152
24	9.164600	9.995316	9.169284	10.878237
25	9.165454	9.995297	9.170157	10.879322
26	9.166307	9.995278	9.171029	10.880407
27	9.167158	9.995260	9.171899	10.881492
28	9.168008	9.995241	9.172767	10.882577
29	9.168856	9.995222	9.173634	10.883662
30	9.169702	9.995203	9.174499	10.884747

Co-sine | Sine | Co-tang. | Tang.

Degree 81.

Degree 8.

Sine	Co-sine	Tangent	Co-tang.
169702	9.995203	9.174495	10.825501
1705469	9.995184	9.175302	10.824698
1713899	9.995165	9.176124	10.823876
1722309	9.995146	9.176981	10.823016
1730709	9.995127	9.177794	10.822105
1739089	9.995108	9.178709	10.821202
1747449	9.995089	9.179635	10.820349
1755789	9.995070	9.180508	10.819451
1764119	9.995051	9.181368	10.818506
1772429	9.995033	9.182211	10.817589
1780729	9.995012	9.183060	10.816650
1789009	9.994993	9.183907	10.815699
1797269	9.994974	9.184752	10.814748
1805519	9.994955	9.185597	10.813799
1813749	9.994935	9.186439	10.812850
1821969	9.994916	9.187280	10.811892
1830169	9.994896	9.188120	10.810934
1838349	9.994876	9.188957	10.810045
1846519	9.994857	9.189792	10.809106
1854669	9.994838	9.190619	10.808147
1862809	9.994818	9.191462	10.807188
1870929	9.994798	9.192292	10.806229
1879039	9.994779	9.193122	10.805270
1887129	9.994759	9.193953	10.804311
1895199	9.994739	9.194780	10.803352
1903259	9.994719	9.195606	10.802393
1911309	9.994699	9.196440	10.801434
1919339	9.994680	9.197253	10.800475
1927349	9.994660	9.198074	10.801516
1935349	9.994640	9.198892	10.801100
1943329	9.994620	9.199712	10.800287

Sine | Co-sine | Tangent |

Degree 81.

Degree 79.

M	Sine	Co-sine	Tangent	Co-tang
09	194332	9.994620	9.199712	10.80028
10	195129	9.994600	9.200529	10.79947
20	195925	9.994580	9.201345	10.79866
30	196718	9.994560	9.202159	10.79784
40	197511	9.994540	9.202971	10.79702
50	198302	9.994519	9.203782	10.79620
60	199091	9.994496	9.204592	10.79538
70	199879	9.994479	9.205400	10.79456
80	200666	9.994459	9.206207	10.79374
90	201451	9.994438	9.207013	10.79292
100	202234	9.994418	9.207817	10.79210
110	203017	9.994398	9.208619	10.79128
120	203797	9.994377	9.209420	10.79046
130	204577	9.994357	9.210220	10.78964
140	205354	9.994336	9.211018	10.78882
150	206131	9.994316	9.211815	10.78800
160	206906	9.994295	9.212611	10.78718
170	207679	9.994274	9.213405	10.78636
180	208452	9.994254	9.214198	10.78554
190	209222	9.994233	9.214989	10.78472
200	209992	9.994212	9.215780	10.78390
210	210760	9.994191	9.216568	10.78308
220	211526	9.994171	9.217356	10.78226
230	212291	9.994150	9.218142	10.78144
240	213055	9.994129	9.218929	10.78062
250	213818	9.994108	9.219710	10.77980
260	214579	9.994087	9.220491	10.77898
270	215338	9.994066	9.221272	10.77816
280	216097	9.994044	9.222052	10.77734
290	216854	9.994024	9.222830	10.77652
300	217609	9.994003	9.223607	10.77570

Co-sine | Sine | Co-tang. | Tang.

Degree 80.

Degree 9.

Sine	Co-sine	Tangent	Co-tang.
17609	9.994003	9.223607	10.776393
18363	9.993982	9.224382	10.775618
19116	9.993960	9.225156	10.774844
19858	9.993939	9.225929	10.774071
20618	9.993918	9.226704	10.773300
21367	9.993897	9.227471	10.772529
22115	9.993875	9.228240	10.771760
22861	9.993854	9.229007	10.770993
23606	9.993832	9.229774	10.770226
24349	9.993811	9.230539	10.769461
25092	9.993789	9.231302	10.768698
25833	9.993768	9.232065	10.767935
26573	9.993746	9.232826	10.767174
27311	9.993725	9.233586	10.766414
28048	9.993703	9.234345	10.765655
28784	9.993681	9.235103	10.764897
29518	9.993660	9.235859	10.764141
30252	9.993638	9.236614	10.763386
30984	9.993616	9.237368	10.762632
31715	9.993594	9.238120	10.761880
32444	9.993572	9.238871	10.761128
33172	9.993550	9.239622	10.760378
33899	9.993528	9.240371	10.759629
34625	9.993506	9.241118	10.758882
35349	9.993484	9.241865	10.758135
36073	9.993462	9.242610	10.757390
36795	9.993440	9.243354	10.756646
37515	9.993418	9.244097	10.755903
38235	9.993396	9.244839	10.755161
38952	9.993374	9.245579	10.754421
39670	9.993351	9.246319	10.753681

Sine | Co-sine | Tangent | Co-tang.

Degree 86.

Degree 70.

1	Sine	Co-sine	Tangent	Co-tang.
c	9.239670	9.993351	9.246319	10.7536
1	9.240386	9.993329	9.247057	10.7539
2	9.241101	9.993307	9.247794	10.7542
3	9.241814	9.993284	9.248530	10.7545
4	9.242526	9.993262	9.249264	10.7548
5	9.243237	9.993240	9.249998	10.7551
6	9.243947	9.993117	9.250730	10.7498
7	9.244656	9.993195	9.251461	10.7488
8	9.245363	9.993172	9.252191	10.7478
9	9.246070	9.993149	9.252920	10.7468
10	9.246775	9.993127	9.253648	10.7458
11	9.247478	9.993104	9.254374	10.7448
12	9.248181	9.993011	9.255200	10.7444
13	9.248883	9.993059	9.255824	10.7440
14	9.249583	9.993036	9.256547	10.7436
15	9.250282	9.993013	9.257269	10.7432
16	9.250980	9.992990	9.257990	10.7428
17	9.251677	9.992967	9.258710	10.7424
18	9.252373	9.992944	9.259429	10.7420
19	9.253067	9.992921	9.260146	10.7416
20	9.253761	9.992898	9.260863	10.7412
21	9.254453	9.992875	9.261578	10.7408
22	9.255144	9.992852	9.262292	10.7404
23	9.255834	9.992829	9.263005	10.7400
24	9.256523	9.992806	9.263717	10.7396
25	9.257211	9.992783	9.264428	10.7392
26	9.257897	9.992759	9.265138	10.7388
27	9.258583	9.992736	9.265847	10.7384
28	9.259268	9.992713	9.266555	10.7380
29	9.259951	9.992690	9.267261	10.7376
30	9.260633	9.992666	9.267967	10.7372
Co-sine		Sine	Co-tang.	Tang.

Degree 79.

Degree 10.

Sine	Co-sine	Tangent	Co-tang.
6063	9.992666	9.267967	10.732033
61314	9.992643	9.268671	10.731329
61994	9.992616	9.269375	10.730625
62673	9.992596	9.270778	10.729923
63351	9.992572	9.271479	10.729221
64027	9.992549	9.271479	10.728521
64703	9.992525	9.272178	10.727822
65378	9.992501	9.272876	10.727124
66051	9.992478	9.273577	10.726427
66723	9.992454	9.274269	10.725731
67395	9.992430	9.274964	10.725036
68065	9.992406	9.275658	10.724342
68734	9.992382	9.276351	10.723649
69402	9.992358	9.277043	10.722957
70069	9.992335	9.277734	10.722267
70735	9.992311	9.278424	10.721576
71400	9.992287	9.279113	10.720887
72063	9.992263	9.279801	10.720199
72726	9.992239	9.280488	10.719512
73388	9.992214	9.281174	10.718826
74049	9.992190	9.281858	10.718142
74708	9.992166	9.282542	10.717458
75367	9.992142	9.283225	10.716775
76025	9.992118	9.283907	10.716093
76681	9.992093	9.284588	10.715412
77337	9.992069	9.285268	10.714732
77991	9.992045	9.285946	10.714053
78685	9.992020	9.286624	10.713376
79297	9.991996	9.287301	10.712699
79948	9.991971	9.287977	10.712023
80599	9.991947	9.288652	10.711348

Sine | Co-sine | Co-tang | Tangent

Degree 79.

Degree 11

M	Sine	Co sine	Tangent	Co-tang
0	9.280559	9.991947	9.288652	10.71134
1	9.281229	9.991922	9.289326	10.71067
2	9.281897	9.991897	9.289999	10.71000
3	9.282544	9.991873	9.290671	10.70932
4	9.283190	9.991848	9.291342	10.70865
5	9.283836	9.991823	9.292013	10.70798
6	9.284480	9.991799	9.292682	10.70731
7	9.285124	9.991774	9.293350	10.70664
8	9.285766	9.991749	9.294017	10.70597
9	9.286408	9.991724	9.294684	10.70530
10	9.287048	9.991699	9.295349	10.70463
11	9.287688	9.991674	9.296013	10.70396
12	9.288326	9.991649	9.296677	10.70329
13	9.288964	9.991624	9.297339	10.70262
14	9.289600	9.991599	9.298001	10.70195
15	9.290236	9.991574	9.298662	10.70128
16	9.290870	9.991549	9.299322	10.70061
17	9.291504	9.991524	9.299980	10.70000
18	9.292137	9.991498	9.300638	10.69939
19	9.292768	9.991473	9.301295	10.69878
20	9.293399	9.991448	9.301951	10.69817
21	9.294029	9.991422	9.302607	10.69756
22	9.294658	9.991397	9.303261	10.69695
23	9.295286	9.991372	9.303914	10.69634
24	9.295913	9.991346	9.304567	10.69573
25	9.296539	9.991321	9.305218	10.69512
26	9.297164	9.991295	9.305867	10.69451
27	9.297788	9.991270	9.306519	10.69390
28	9.298412	9.991244	9.307168	10.69329
29	9.299034	9.991218	9.307816	10.69268
30	9.299655	9.991193	9.308463	10.69207
Co-sine		Sine	Co-tang.	Tang

Degree 78

Degree 77.

Sine | Co-sine. | | Tangent | Co-tang. |

99655 | 9.9911937 | 19.308463 | 10.691537 | 30

00276 | 9.991167 | 2.309109 | 10.69089 | 29

00895 | 9.991141 | 2.309754 | 10.690246 | 28

01514 | 9.991115 | 2.310399 | 10.689601 | 27

02132 | 9.991090 | 2.311042 | 10.688958 | 26

02749 | 9.991064 | 2.311685 | 10.688315 | 25

03364 | 9.991038 | 2.312327 | 10.687673 | 24

03979 | 9.991012 | 2.312968 | 10.687032 | 23

04593 | 9.990986 | 2.313608 | 10.686392 | 22

05207 | 9.990960 | 2.314247 | 10.685753 | 21

05819 | 9.990934 | 2.314885 | 10.685115 | 20

06430 | 9.990908 | 2.315523 | 10.684477 | 19

07041 | 9.990882 | 2.316159 | 10.683841 | 18

07650 | 9.990855 | 2.316795 | 10.683205 | 17

08259 | 9.990829 | 2.317430 | 10.682570 | 16

08867 | 9.990803 | 2.318064 | 10.681936 | 15

09474 | 9.990777 | 2.318697 | 10.681303 | 14

10080 | 9.990750 | 2.319330 | 10.680670 | 13

10685 | 9.990724 | 2.319961 | 10.680038 | 12

11289 | 9.990697 | 2.320592 | 10.679408 | 11

11899 | 9.990671 | 2.321222 | 10.678778 | 10

12495 | 9.990645 | 2.321851 | 10.678149 | 9

13097 | 9.990618 | 2.322479 | 10.677521 | 8

13698 | 9.990591 | 2.323106 | 10.676894 | 7

14297 | 9.990565 | 2.323733 | 10.676267 | 6

14897 | 9.990538 | 2.324358 | 10.675642 | 5

15495 | 9.990512 | 2.324983 | 10.675017 | 4

16092 | 9.990485 | 2.325607 | 10.674393 | 3

16689 | 9.990458 | 2.326231 | 10.673769 | 2

17284 | 9.990431 | 2.326853 | 10.673147 | 1

17879 | 9.990404 | 2.327475 | 10.672525 | 0

Sine | Co-sine. | | Tangent |

Degree 78.

Degree 12.

M	Sine	Co-sine	Tangent	Co-tang.
0	9.317879	9.990404	9.327475	10.672525
1	9.318473	9.990377	9.328095	10.671905
2	9.319066	9.99035	9.328715	10.671285
3	9.319658	9.990324	9.329334	10.670665
4	9.320250	9.990297	9.329953	10.670045
5	9.320840	9.990270	9.330571	10.669425
6	9.321430	9.990242	9.331187	10.668805
7	9.322019	9.990215	9.331803	10.668185
8	9.322607	9.990188	9.332418	10.667565
9	9.323194	9.990161	9.333033	10.666945
10	9.323780	9.990134	9.333646	10.666325
11	9.324366	9.990107	9.334259	10.665705
12	9.324950	9.990079	9.334871	10.665085
13	9.325534	9.990052	9.335482	10.664465
14	9.326117	9.990025	9.336093	10.663845
15	9.326699	9.989997	9.336703	10.663225
16	9.327281	9.989970	9.337311	10.662605
17	9.327862	9.989942	9.337919	10.661985
18	9.328441	9.989915	9.338527	10.661365
19	9.329020	9.989888	9.339133	10.660745
20	9.329599	9.989860	9.339739	10.660125
21	9.330176	9.989832	9.340344	10.659505
22	9.330753	9.989804	9.340948	10.658885
23	9.331328	9.989777	9.341552	10.658265
24	9.331903	9.989749	9.342155	10.657645
25	9.332478	9.989721	9.342759	10.657025
26	9.333051	9.989693	9.343358	10.656405
27	9.333624	9.989665	9.343958	10.655785
28	9.334194	9.989637	9.344554	10.655165
29	9.334766	9.989609	9.345157	10.654545
30	9.335337	9.989581	9.345755	10.653925
Co-sine		Sine	Co-tang. Tan	

Degree 77.

Degree 76.

Sine	Co-sine	Tangent	Co-tang.
9.989581	10.65424	130	
9.989553	10.653647	129	
9.989525	10.653051	128	
9.989597	10.652455	127	
9.989469	10.651859	126	
9.989441	10.651263	125	
9.989413	10.650671	124	
9.989384	10.650078	123	
9.989356	10.649486	122	
9.989328	10.648894	121	
9.989299	10.648303	120	
9.989271	10.647713	119	
9.989243	10.647124	118	
9.989214	10.646535	117	
9.989185	10.645947	116	
9.989157	10.645360	115	
9.989128	10.644773	114	
9.989100	10.644187	113	
9.989071	10.643602	112	
9.989042	10.643018	111	
9.989014	10.642434	110	
9.988985	10.641851	109	
9.988956	10.641269	108	
9.988927	10.640687	107	
9.988898	10.640107	106	
9.988869	10.639526	105	
9.988840	10.638947	104	
9.988811	10.638369	103	
9.988782	10.637790	102	
9.988754	10.637213	101	
9.988724	10.636636	100	

Sine | Co-sine | Tangent | Co-tang.

Degree 77.

Degree 13.

M	Sine	Co-sine	Tangent	Co-tang.
0	9.352088	9.988724	19.363364	10.636636
1	9.352635	9.988695	9.363940	10.636060
2	9.353181	9.988666	9.364515	10.635485
3	9.353726	9.988636	9.365090	10.634910
4	9.354271	9.988607	9.365664	10.634335
5	9.354815	9.988578	9.366237	10.633760
6	9.355358	9.988548	9.366810	10.633185
7	9.355901	9.988519	9.367382	10.632610
8	9.356443	9.988489	9.367953	10.632035
9	9.356984	9.988460	9.368524	10.631460
10	9.357524	9.988430	9.369094	10.630885
11	9.358064	9.988401	9.369663	10.630310
12	9.358603	9.988371	9.370232	10.629735
13	9.359141	9.988342	9.370799	10.629160
14	9.359679	9.988312	9.371367	10.628585
15	9.350215	9.988282	9.371933	10.628010
16	9.360752	9.988252	9.372499	10.627435
17	9.361287	9.988223	9.373064	10.626860
18	9.361822	9.988193	9.373629	10.626285
19	9.362356	9.988163	9.374193	10.625710
20	9.362889	9.988133	9.374756	10.625135
21	9.363422	9.988103	9.375319	10.624560
22	9.363954	9.988073	9.375881	10.623985
23	9.364485	9.988043	9.376442	10.623410
24	9.365016	9.988013	9.377003	10.622835
25	9.365546	9.987983	9.377563	10.622260
26	9.366075	9.987953	9.378122	10.621685
27	9.366604	9.987922	9.378681	10.621110
28	9.367132	9.987892	9.379239	10.620535
29	9.367659	9.987862	9.379797	10.619960
30	9.368185	9.987832	9.380354	10.619385
Co-sine		Sine	Co-tang.	Tan

Degree 76.

Degree 13.

Sine	Co-sine	Tangent	Co-tang.
68185	9.9878321	19.380354	10.619646130
68711	9.987801	9.380910	10.619090129
69236	9.987771	9.381466	10.618534128
69761	9.987740	9.382021	10.617980127
70285	9.987710	9.382575	10.617425126
70808	9.987679	9.383129	10.616871125
71330	9.987649	9.383682	10.616318124
71852	9.987618	9.384234	10.615766123
72373	9.987588	9.384786	10.615214122
72894	9.987557	9.385337	10.614663121
73414	9.987526	9.385888	10.614112120
73933	9.987496	9.386438	10.613562119
74452	9.987465	9.386987	10.613013118
74970	9.987434	9.387536	10.612464117
75487	9.987403	9.388084	10.611916116
76003	9.987372	9.388631	10.611369115
76519	9.987341	9.389178	10.610822114
77035	9.987310	9.389724	10.610276113
77549	9.987279	9.390270	10.609730112
78063	9.987248	9.390815	10.609185111
78577	9.987217	9.391360	10.608640110
79089	9.987186	9.391907	10.608097109
79601	9.987155	9.392467	10.607553108
80113	9.987124	9.392989	10.607011107
80624	9.987092	9.393531	10.606469106
81134	9.987061	9.394074	10.605927105
81643	9.987030	9.394614	10.605386104
82152	9.986998	9.395154	10.604846103
82661	9.986967	9.395694	10.604306102
83168	9.986935	9.396233	10.603767101
83675	9.986904	9.396771	10.603229100

Degree 76.

Degree 14.

N	Sine	Co-sine	Tangent	Co-tang.
0	9.383675	9.986904	9.396771	10.60322
1	9.384181	9.986873	9.397309	10.60269
2	9.384687	9.986841	9.397846	10.60216
3	9.385192	9.986809	9.398383	10.60163
4	9.385697	9.986778	9.398919	10.60110
5	9.386201	9.986746	9.399455	10.60057
6	9.386704	9.986714	9.399990	10.60004
7	9.387207	9.986683	9.400524	10.59951
8	9.387709	9.986651	9.401058	10.59898
9	9.388210	9.986619	9.401591	10.59845
10	9.388711	9.986587	9.402124	10.59792
11	9.389211	9.986555	9.402656	10.59739
12	9.389711	9.986523	9.403187	10.59686
13	9.390210	9.986491	9.403718	10.59633
14	9.390708	9.986459	9.404249	10.59580
15	9.391206	9.986427	9.404778	10.59527
16	9.391703	9.986395	9.405306	10.59474
17	9.392199	9.986363	9.405836	10.59421
18	9.392695	9.986331	9.406364	10.59368
19	9.393190	9.986299	9.406892	10.59315
20	9.393685	9.986266	9.407419	10.59262
21	9.394179	9.986234	9.407945	10.59209
22	9.394673	9.986201	9.408471	10.59156
23	9.395166	9.986169	9.408996	10.59103
24	9.395654	9.986137	9.409521	10.59050
25	9.396150	9.986104	9.410045	10.58997
26	9.396641	9.986072	9.410569	10.58944
27	9.397131	9.986039	9.411092	10.58891
28	9.397621	9.986007	9.411615	10.58838
29	9.398111	9.985974	9.412137	10.58785
30	9.398600	9.985942	9.412658	10.58732
Co-sine		Sine	Co-tang.	

Degree 75.

Degree 14.

Sine	Co-sine	Tangent	Co-tang.
98600	9.985942	9.412658	10.587342 30
99087	9.985909	9.413179	10.586821 29
99575	9.985876	9.413699	10.586301 28
00062	9.985843	9.414219	10.585781 27
00549	9.985811	9.414738	10.585262 26
01035	9.985778	9.415257	10.584742 25
01520	9.985745	9.415775	10.584225 24
02005	9.985712	9.416293	10.583707 23
02489	9.985679	9.416810	10.583190 22
02972	9.985646	9.417326	10.582674 21
03455	9.985613	9.417842	10.582157 20
03938	9.985580	9.418357	10.581642 19
04420	9.985547	9.418873	10.581127 18
04901	9.985513	9.419387	10.580613 17
05382	9.985480	9.419901	10.580099 16
05862	9.985447	9.420415	10.579585 15
06341	9.985414	9.420927	10.579072 14
06820	9.985380	9.421440	10.578560 13
07299	9.985347	9.421951	10.578048 12
07776	9.985314	9.422463	10.577537 11
08254	9.985280	9.422973	10.577026 10
08731	9.985247	9.423484	10.576516 9
09207	9.985213	9.423993	10.576007 8
09682	9.985180	9.424503	10.575497 7
10157	9.985146	9.425011	10.574989 6
10632	9.985112	9.425518	10.574480 5
11106	9.985079	9.426027	10.573973 4
11579	9.985045	9.426534	10.573466 3
12052	9.985011	9.427041	10.572959 2
12524	9.984977	9.427547	10.572453 1
12996	9.984943	9.428052	10.571947 0

T	Sine	Co-tang	Tangent	M
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Degree 75.

Degree 15.

M	Sine	Co-sine	Tangent	Co-tang
0	9.412996	9.984944	9.428052	10.571948
1	9.413467	9.984910	9.428557	10.571443
2	9.413938	9.984876	9.429062	10.570938
3	9.414408	9.984842	9.429566	10.570433
4	9.414878	9.984808	9.430070	10.569928
5	9.415347	9.984774	9.430573	10.569423
6	9.415815	9.984740	9.431075	10.568918
7	9.416283	9.984706	9.431577	10.568413
8	9.416850	9.984672	9.432079	10.567908
9	9.417217	9.984637	9.432580	10.567403
10	9.417684	9.984603	9.433080	10.566898
11	9.418149	9.984569	9.433580	10.566393
12	9.418615	9.984535	9.434080	10.565888
13	9.419079	9.984500	9.434579	10.565383
14	9.419544	9.984466	9.435078	10.564878
15	9.420007	9.984431	9.435576	10.564373
16	9.420470	9.984397	9.436073	10.563868
17	9.420933	9.984363	9.436570	10.563363
18	9.421395	9.984328	9.437067	10.562858
19	9.421856	9.984293	9.437563	10.562353
20	9.422317	9.984259	9.438059	10.561848
21	9.422778	9.984224	9.439554	10.561343
22	9.423238	9.984189	9.439548	10.560838
23	9.423697	9.984155	9.439543	10.560333
24	9.424156	9.984120	9.440036	10.559828
25	9.424615	9.984085	9.440529	10.559323
26	9.425072	9.984050	9.441022	10.558818
27	9.425530	9.984015	9.441514	10.558313
28	9.425987	9.983980	9.441006	10.557808
29	9.426443	9.983945	9.442497	10.557303
30	9.426899	9.983910	9.442988	10.556798
	Co-sine	Sine	Co-tang.	Tang.

Degree 74.

Degree 15.

Sine	Co-sine	Tangent	Co-tang.
26899	9.98391	19.44298	10.55701
27354	9.98387	9.44347	10.55652
27809	9.98384	9.44396	10.55603
28264	9.98380	9.44445	10.55554
28717	9.98377	9.44494	10.55505
29170	9.98373	9.44543	10.55456
29623	9.98369	9.44592	10.55407
30075	9.98366	9.44641	10.55358
30507	9.98362	9.44689	10.55309
30978	9.98359	9.44738	10.55260
31429	9.98355	9.44787	10.55211
31879	9.98352	9.44836	10.55162
32328	9.98348	9.44884	10.55113
32778	9.98345	9.44932	10.55064
33206	9.98341	9.44980	10.55015
33674	9.98338	9.45029	10.54966
34122	9.98334	9.45077	10.54917
34569	9.98330	9.45126	10.54868
35016	9.98327	9.45174	10.54819
35462	9.98323	9.45222	10.54770
35918	9.98320	9.45270	10.54721
36353	9.98316	9.45318	10.54672
36798	9.98313	9.45366	10.54623
37242	9.98309	9.45414	10.54574
37686	9.98305	9.45462	10.54525
38129	9.98302	9.45510	10.54476
38572	9.98298	9.45558	10.54427
39014	9.98295	9.45606	10.54378
39456	9.98291	9.45654	10.54329
39897	9.98287	9.45701	10.54280
40338	9.98284	9.45749	10.54231
Sine	Co-sine	Tangent	Co-tang.

Degree 74.

Degree 16.

Sine	Co-sine	Tangent	Co-tang.
00.440338	9.982842	12.457496	10.742504
19.440778	9.982805	9.457973	10.542027
29.441218	9.982769	9.458449	10.541551
39.441658	9.982733	9.458925	10.541075
49.442096	9.982696	9.459401	10.540600
59.442535	9.982660	9.459875	10.540125
69.442973	9.982623	9.460349	10.539650
79.443416	9.982587	9.460829	10.539175
89.443848	9.982550	9.461297	10.538700
99.444284	9.982514	9.461770	10.538225
109.444720	9.982477	9.462242	10.537750
119.445155	9.982441	9.462714	10.537275
129.445590	9.982404	9.463186	10.536800
139.446025	9.982367	9.463658	10.536325
149.446459	9.982330	9.464129	10.535850
159.446892	9.982294	9.464599	10.535375
169.447326	9.982257	9.465069	10.534900
179.447759	9.982220	9.465539	10.534425
189.448191	9.982183	9.466008	10.533950
199.448623	9.982146	9.466476	10.533475
209.449054	9.982109	9.466945	10.533000
219.449485	9.982072	9.467413	10.532525
229.449915	9.982035	9.467880	10.532050
239.450345	9.981998	9.468347	10.531575
249.450775	9.981961	9.468814	10.531100
259.451203	9.981923	9.469280	10.530625
269.451632	9.981886	9.469746	10.530150
279.452060	9.981849	9.470211	10.529675
289.452488	9.981812	9.470676	10.529200
299.452915	9.981774	9.471141	10.528725
309.453342	9.981737	9.471605	10.528250
Co-sine	Sine	Co-tang.	Tan

Degree 73.

Degree 16.

Sine	Co-sine	Tangent	Co-tang.
334.9.981737	19.471605	10.528395	35
337.689.981695	9.472068	10.527931	29
341.949.981662	9.472522	10.527468	28
346.199.981624	9.472995	10.527005	27
350.449.981587	9.473457	10.526542	26
354.699.981549	9.473919	10.52608	25
358.949.981512	9.474381	10.525619	24
363.199.981474	9.474842	10.525158	23
367.449.981436	9.475303	10.524699	22
371.699.981398	9.475763	10.524237	21
375.949.981361	9.476223	10.523777	20
380.069.981323	9.476683	10.523317	19
384.279.981285	9.477142	10.522858	18
388.489.981247	9.477601	10.522399	17
392.689.981209	9.478059	10.521941	16
396.849.981171	9.478517	10.521482	15
401.089.981133	9.478975	10.521025	14
405.279.981095	9.479432	10.520568	13
409.469.981057	9.479889	10.520111	12
413.649.981019	9.480345	10.519655	11
417.829.980980	9.480801	10.519199	10
421.999.980942	9.481257	10.518743	9
426.169.980904	9.481712	10.518288	8
430.329.980866	9.482167	10.517833	7
434.489.980827	9.482621	10.517379	6
438.649.980789	9.483075	10.516925	5
442.799.980750	9.483528	10.516471	4
446.949.980712	9.483982	10.516018	3
451.089.980672	9.484434	10.515565	2
455.229.980635	9.484887	10.515113	1
459.339.980596	9.485339	10.514661	0

Sine | Co-sine | Tangent | Co-tang.

Degree 73.

Degree 17.

M	Sine	Co-sine	Tangent	Co-tan
0	9.465935	9.980596	9.485339	10.514661
1	9.466348	9.980558	9.485791	10.514109
2	9.466761	9.980519	9.486242	10.513557
3	9.467173	9.980480	9.486693	10.513005
4	9.467585	9.980441	9.487143	10.512453
5	9.467996	9.980401	9.487591	10.511901
6	9.468407	9.980364	9.488043	10.511349
7	9.468817	9.980325	9.488493	10.510797
8	9.469227	9.980286	9.488941	10.510245
9	9.469637	9.980247	9.489390	10.509693
10	9.469446	9.980208	9.489838	10.509141
11	9.470455	9.980169	9.490286	10.508589
12	9.471863	9.980130	9.490733	10.508037
13	9.471071	9.980091	9.491180	10.507485
14	9.471678	9.980052	9.491627	10.506933
15	9.472086	9.980012	9.492073	10.506381
16	9.472492	9.979973	9.492519	10.505829
17	9.472898	9.979934	9.492964	10.505277
18	9.473304	9.979894	9.493410	10.504725
19	9.473710	9.979855	9.493854	10.504173
20	9.474116	9.979816	9.494299	10.503621
21	9.474519	9.979776	9.494743	10.503069
22	9.474923	9.979737	9.495186	10.502517
23	9.475327	9.979697	9.49563	10.501965
24	9.475730	9.979658	9.496073	10.501413
25	9.476133	9.979618	9.496514	10.500861
26	9.476536	9.979578	9.496957	10.500309
27	9.476938	9.979539	9.497399	10.500757
28	9.477340	9.979499	9.497840	10.500205
29	9.477741	9.979455	9.498282	10.500653
30	9.478142	9.979419	9.498722	10.500101
Co-sine		Sine	Co-tang.	Tan

Degree 72.

Degree 17.

Sine	Co-sine	Tangent	Co-tang.
78142	9.979419	19.498722	10.301278
78342	9.979380	9.499163	10.500837
78942	9.979340	9.499602	10.500398
79342	9.979300	9.500042	10.499958
79741	9.979260	9.500481	10.499519
80140	9.979220	9.500920	10.499080
80538	9.979180	9.501359	10.498641
80936	9.979140	9.501797	10.498203
81334	9.979099	9.502234	10.497765
81731	9.979059	9.502672	10.497328
82128	9.979019	9.503109	10.496891
82525	9.978980	9.503546	10.496454
82921	9.978939	9.503982	10.496018
83316	9.978898	9.504418	10.495582
83711	9.978858	9.504854	10.495146
84106	9.978817	9.505289	10.494711
84501	9.978777	9.505724	10.494276
84895	9.978736	9.506158	10.493841
85289	9.978696	9.506593	10.493407
85682	9.978655	9.507026	10.492973
86075	9.978615	9.507459	10.492540
86467	9.978574	9.507892	10.492107
86859	9.978533	9.508326	10.491674
87251	9.978493	9.508759	10.491241
87642	9.978452	9.509181	10.490809
88033	9.978411	9.509622	10.490377
88424	9.978370	9.510044	10.489946
88814	9.978329	9.510486	10.489515
89204	9.978288	9.510916	10.489084
89593	9.978247	9.511346	10.488654
89982	9.978206	9.511776	10.488225

Sine | Co-tang. | Tangent. | M

Degree 72.

Degree 18.

M	Sine	Co-sine	Tangent	Co-tang.
1	9.489982	9.978206	9.511776	10.488224
2	9.490371	9.978165	9.512206	10.487794
3	9.490759	9.978124	9.512635	10.487365
4	9.491147	9.978083	9.513064	10.486936
5	9.491534	9.978042	9.513493	10.486507
6	9.491922	9.978000	9.513921	10.486078
7	9.492308	9.977959	9.514349	10.485649
8	9.492695	9.977918	9.514777	10.485220
9	9.493080	9.977877	9.515204	10.484791
10	9.493466	9.977835	9.515631	10.484362
11	9.493851	9.977794	9.516057	10.483933
12	9.494236	9.977752	9.516484	10.483504
13	9.494620	9.977711	9.516910	10.483075
14	9.495005	9.977669	9.517335	10.482646
15	9.495388	9.977628	9.517761	10.482217
16	9.495771	9.977586	9.518185	10.481788
17	9.496154	9.977544	9.518610	10.481359
18	9.496537	9.977503	9.519034	10.480930
19	9.496919	9.977461	9.519458	10.480501
20	9.497301	9.977419	9.519882	10.480072
21	9.497682	9.977377	9.520305	10.479643
22	9.498063	9.977335	9.520728	10.479214
23	9.498444	9.977293	9.521151	10.478785
24	9.498824	9.977251	9.521573	10.478356
25	9.499204	9.977209	9.521995	10.477927
26	9.499584	9.977167	9.522417	10.477498
27	9.499963	9.977125	9.522838	10.477069
28	9.500342	9.977083	9.523259	10.476640
29	9.500720	9.977041	9.523679	10.476211
30	9.501099	9.977000	9.524100	10.475782
31	9.501476	9.977956	9.524520	10.475353
Co-sine Sine Co-tang. Tang.				

Degree 71.

Degree 18.

Sine	Co-sine	Tangent	Co-tang
14769.977956	9.524520	10.475484	30
18349.976914	9.524936	10.475060	29
22919.976872	9.525359	10.474641	28
28679.976830	9.525778	10.474224	27
34849.976787	9.526197	10.473805	26
41360.976745	9.526615	10.473385	25
48339.976703	9.527033	10.472967	24
55110.976660	9.527451	10.472549	23
61839.976617	9.527868	10.472134	22
68409.976574	9.528285	10.471714	21
75234.976532	9.528702	10.471298	20
818089.976489	9.529118	10.470881	19
88819.976446	9.529535	10.470465	18
95349.976404	9.529950	10.470049	17
10279.976361	9.530366	10.469634	16
10999.976318	9.530781	10.469219	15
11719.976275	9.531198	10.468804	14
12439.976232	9.531611	10.468389	13
13149.976189	9.532025	10.467975	12
13859.976146	9.532436	10.467561	11
14559.976103	9.532852	10.467147	10
15269.976060	9.533266	10.466734	9
15969.976027	9.533679	10.466321	8
16669.975970	9.534092	10.465908	7
17349.975930	9.534504	10.465496	6
18039.975887	9.534916	10.465084	5
18719.975844	9.535328	10.464672	4
19409.975800	9.535739	10.464261	3
20079.975757	9.536150	10.463849	2
20759.975713	9.536561	10.463439	1
21429.975670	9.536972	10.463028	0

T Sine | Co-tang | Tangent | M

Degree 71.

Degree 19.

M Sine	Co-sine	Tangent	Co-tang
09.512644	9.975670	19.536672	10.463328
19.513009	9.975626	9.537382	10.462618
29.513375	9.975583	9.537792	10.461908
39.513741	9.975539	9.538202	10.461198
49.514107	9.975496	9.538610	10.460488
59.514472	9.975452	9.539020	10.459778
69.514837	9.975408	9.539429	10.459068
79.515202	9.975364	9.539837	10.458358
89.515566	9.975321	9.540245	10.457648
99.515930	9.975277	9.540653	10.456938
109.516294	9.975233	9.541061	10.456228
119.516657	9.975189	9.541468	10.455518
129.517020	9.975145	9.541875	10.454808
139.517382	9.975101	9.542281	10.454098
149.517745	9.975057	9.542688	10.453388
159.518107	9.975013	9.543094	10.452678
169.518468	9.974969	9.543499	10.451968
179.518829	9.974925	9.543903	10.451258
189.519190	9.974880	9.544310	10.450548
199.519551	9.974836	9.544715	10.449838
209.519911	9.974792	9.545119	10.449128
219.520271	9.974747	9.545524	10.448418
229.520631	9.974703	9.545927	10.447708
239.520990	9.974659	9.546331	10.446998
249.521349	9.974614	9.546735	10.446288
259.521707	9.974570	9.547138	10.445578
269.522065	9.974525	9.547540	10.444868
279.522423	9.974480	9.547943	10.444158
289.522781	9.974436	9.548345	10.443448
299.523138	9.974391	9.548747	10.442738
309.523495	9.974346	9.549149	10.442028
Co-sine	Sine -	Co-tang.	Tan

Degree 70.

Degree 19.

Sine.	Co-sine.	Tangent.	Co-tang.
934951	99743461	19 549149	10.45085130
23851	9974302	9.548556	10.45045029
24208	9974257	9.549951	10.45004928
24564	9974212	9.5516352	10.44964827
24920	9974167	9.5530752	10.44924826
25275	9974122	9.5551152	10.44884825
25630	9974077	9.5571552	10.44844824
25984	9974032	9.5591952	10.44804823
26339	9973987	9.5622351	10.44764922
26693	9973942	9.5642750	10.44725021
27046	9973897	9.5663149	10.44695120
27400	9973852	9.5683548	10.44655219
27753	9973807	9.5703946	10.44615318
28105	9973761	9.5724344	10.44575417
28458	9973716	9.5744742	10.44535516
28810	9973671	9.5765139	10.44495615
29161	9973623	9.5785536	10.44455714
29513	9973580	9.5805932	10.44415813
29864	9973535	9.5826329	10.44375912
30214	9973489	9.5846725	10.44336011
30565	9973443	9.5867121	10.44296110
30915	9973398	9.5887517	10.44256209
31265	9973352	9.5907912	10.44216308
31614	9973307	9.5928308	10.44176407
31963	9973261	9.5948702	10.44136506
32312	9973215	9.5969097	10.44096605
32661	9973169	9.5989491	10.44056704
33009	9973123	9.5998885	10.44016803
33357	9973078	9.600279	10.43976902
33704	9973032	9.600673	10.43937001
34052	9972986	9.601066	10.43897100

Sine | Co-sine. | Tangent | Co-tang.

Degree 70.

Degree 26.

M	Sine	Co-fine	Tangenc	Co-fine
00	9.534050	9.970989	9.561061	10.4379
1	9.534395	9.970949	9.561459	10.4378
2	9.534740	9.970909	9.561851	10.4377
3	9.535091	9.970868	9.562244	10.4376
4	9.535437	9.970828	9.562636	10.4375
5	9.535781	9.970787	9.563028	10.4374
6	9.536129	9.970747	9.563419	10.4373
7	9.536474	9.970706	9.563811	10.4372
8	9.536818	9.970665	9.564202	10.4371
9	9.537163	9.970625	9.564592	10.4370
10	9.537507	9.970584	9.564983	10.4369
11	9.537851	9.970543	9.565373	10.4368
12	9.538194	9.970502	9.565763	10.4367
13	9.538537	9.970461	9.566153	10.4366
14	9.538880	9.970420	9.566542	10.4365
15	9.539222	9.970379	9.566932	10.4364
16	9.539565	9.970338	9.567320	10.4363
17	9.539907	9.970297	9.567709	10.4362
18	9.540249	9.970256	9.568097	10.4361
19	9.540590	9.970215	9.568486	10.4360
20	9.540931	9.970174	9.568873	10.4359
21	9.541272	9.970133	9.569261	10.4358
22	9.541612	9.970092	9.569649	10.4357
23	9.541953	9.970051	9.560035	10.4356
24	9.542292	9.970010	9.560423	10.4355
25	9.542632	9.969969	9.560809	10.4354
26	9.542971	9.969928	9.571195	10.4353
27	9.543310	9.969887	9.571581	10.4352
28	9.543649	9.969846	9.571967	10.4351
29	9.543987	9.969805	9.572352	10.4350
30	9.544325	9.969764	9.572748	10.4349
Co-fine Sine Co-tang. Tan-fine				

Degree 69.

Degree 26.

ne	Co-sine	Tangent	Co-tang.
4215	9.971588	9.572738	10.427262
4663	9.971540	9.573173	10.426827
5000	9.971493	9.573507	10.426492
5338	9.971445	9.573892	10.426108
5674	9.971398	9.574276	10.425724
6011	9.971351	9.574660	10.425340
6347	9.971303	9.575044	10.424956
6683	9.971256	9.575427	10.424571
7019	9.971208	9.575810	10.424189
7354	9.971161	9.576193	10.423807
7690	9.971113	9.576576	10.423424
8024	9.971065	9.576958	10.423041
8358	9.971018	9.577341	10.422659
8693	9.970970	9.577723	10.422277
9026	9.970922	9.578104	10.421896
9360	9.970874	9.578486	10.421514
9693	9.970826	9.578867	10.421133
10026	9.970779	9.579248	10.420752
10359	9.970731	9.579628	10.420371
10692	9.970683	9.580009	10.419991
11024	9.970634	9.580389	10.419611
11355	9.970586	9.580769	10.419231
11687	9.970538	9.581149	10.418851
12018	9.970490	9.581528	10.418472
12349	9.970442	9.581907	10.418092
12680	9.970394	9.582286	10.417713
13010	9.970345	9.582665	10.417335
13340	9.970297	9.583043	10.416956
13670	9.970249	9.583422	10.416578
14000	9.970200	9.583800	10.416200
14325	9.970152	9.584177	10.415823

sine | Sine | Co-tang. | Tangent

Degree 69.

Degree 21.

M	Sine	Co-fine	Tangent	Co-tang
	9,554329	9,970152	9,584177	10,4158
1	9,554658	9,970103	9,584551	10,4158
2	9,554987	9,970054	9,584922	10,4158
3	9,555315	9,970006	9,585298	10,4158
4	9,555643	9,969957	9,585680	10,4158
5	9,555971	9,969909	9,586062	10,4158
6	9,556299	9,969860	9,586439	10,4158
7	9,556626	9,969811	9,586811	10,4158
8	9,556953	9,969762	9,587190	10,4158
9	9,557279	9,969713	9,587568	10,4158
10	9,557606	9,969665	9,587941	10,4158
11	9,557932	9,969616	9,588316	10,4158
12	9,558258	9,969567	9,588691	10,4158
13	9,558583	9,969518	9,589066	10,4158
14	9,558909	9,969469	9,589440	10,4158
15	9,559234	9,969419	9,589814	10,4158
16	9,559558	9,969370	9,590188	10,4098
17	9,559883	9,969321	9,590561	10,4098
18	9,560207	9,969272	9,590935	10,4098
19	9,560531	9,969223	9,591308	10,4088
20	9,560855	9,969173	9,591681	10,4088
21	9,561178	9,969124	9,592054	10,4079
22	9,561501	9,969075	9,592426	10,4079
23	9,561824	9,969025	9,592798	10,4072
24	9,562146	9,968976	9,593170	10,4068
25	9,562468	9,968926	9,593542	10,4064
26	9,562790	9,968877	9,593914	10,4060
27	9,563112	9,968827	9,594285	10,4057
28	9,563433	9,968777	9,594656	10,4053
29	9,563754	9,968728	9,595027	10,4050
30	9,564076	9,968678	9,595397	10,4046
Co-fine Sine Co-tang. Tang				

Degree 68.

Degree 21.

Sec	Co-fine	Tangent	Co-tang.
40751	9.968678	19.595397	10.404602
4396	9.968628	19.595768	10.404232
4716	9.968578	19.596138	10.403862
5036	9.968528	19.596508	10.403492
5356	9.968478	19.596878	10.403122
5675	9.968428	19.597247	10.402753
5995	9.968378	19.597616	10.402384
6314	9.968328	19.597985	10.402015
6632	9.968278	19.598354	10.401646
6951	9.968228	19.598722	10.401277
7269	9.968178	19.599091	10.400909
7587	9.968128	19.599459	10.400541
7904	9.968078	19.599827	10.400173
8222	9.968027	19.600194	10.399806
8539	9.967977	19.600562	10.399438
8855	9.967927	19.600929	10.399071
9172	9.967876	19.601296	10.398704
9488	9.967826	19.601662	10.398337
9804	9.967775	19.602029	10.397971
10120	9.967725	19.602395	10.397605
10435	9.967674	19.602761	10.397239
10751	9.967623	19.603127	10.396873
11065	9.967573	19.603493	10.396507
11380	9.967522	19.603858	10.396142
11695	9.967471	19.604223	10.395777
12009	9.967420	19.604588	10.395412
12322	9.967370	19.604953	10.395047
12636	9.967319	19.605317	10.394683
12949	9.967368	19.605681	10.394318
13263	9.967217	19.606046	10.393954
13575	9.967166	19.606409	10.393590
Sec	Sine	Co-tang.	Tangent.

Degree 68.

X

Degree 22.

M	Sine	Co-sine	Tangent	Co-tang
0	9.573575	9.967166	9.606409	10.392591
1	9.573888	9.967115	9.606773	10.392227
2	9.574200	9.967064	9.607136	10.391864
3	9.574512	9.967012	9.607500	10.391500
4	9.574824	9.966961	9.607862	10.391138
5	9.575135	9.966910	9.608225	10.390775
6	9.575447	9.966859	9.608588	10.390412
7	9.575758	9.966807	9.608950	10.390049
8	9.576068	9.966756	9.609312	10.389687
9	9.576379	9.966705	9.609674	10.389324
10	9.576689	9.966653	9.610036	10.388962
11	9.576999	9.966602	9.610397	10.388600
12	9.577309	9.966550	9.610758	10.388238
13	9.577618	9.966499	9.611119	10.387875
14	9.577927	9.966447	9.611480	10.387513
15	9.578236	9.966395	9.611841	10.387151
16	9.578545	9.966344	9.612201	10.386789
17	9.578853	9.966292	9.612561	10.386427
18	9.579161	9.966240	9.612921	10.386065
19	9.579469	9.966188	9.613281	10.385703
20	9.579777	9.966136	9.613641	10.385341
21	9.580084	9.966084	9.614000	10.384979
22	9.580392	9.966032	9.614359	10.384617
23	9.580698	9.965980	9.614718	10.384255
24	9.581005	9.965928	9.615077	10.383893
25	9.581311	9.965876	9.615435	10.383531
26	9.581618	9.965824	9.615793	10.383169
27	9.581923	9.965772	9.616151	10.382807
28	9.582229	9.965720	9.616509	10.382445
29	9.582534	9.965668	9.616867	10.382083
30	9.582840	9.965615	9.617224	10.381721
	Co-sine	Sine	Co-tang.	Tan

Degree 67.

Degree 22.

Sec.	Co-sine	Tangent	Co-tang.
3840	9.965615	19.617224	10.382776
3841	9.96563	19.617581	10.382418
3842	9.965651	19.617938	10.382061
3843	9.96567	19.618295	10.381703
3844	9.965696	19.618652	10.381348
3845	9.965713	19.619008	10.380992
3846	9.9657301	19.619364	10.380635
3847	9.965748	19.619720	10.380279
3848	9.965765	19.620076	10.379924
3849	9.965783	19.620432	10.379568
3850	9.965800	19.620787	10.379213
3851	9.965817	19.621143	10.378858
3852	9.965834	19.621497	10.378503
3853	9.965851	19.621852	10.378148
3854	9.965868	19.622206	10.377793
3855	9.965885	19.622561	10.377439
3856	9.965902	19.622915	10.377085
3857	9.965919	19.623269	10.376731
3858	9.965936	19.623623	10.376377
3859	9.965953	19.623976	10.376024
3860	9.965970	19.624330	10.375670
3861	9.965987	19.624683	10.375317
3862	9.965994	19.625036	10.374964
3863	9.966011	19.625388	10.374612
3864	9.966028	19.625741	10.374259
3865	9.966045	19.626093	10.373907
3866	9.966062	19.626445	10.373555
3867	9.966079	19.626797	10.373203
3868	9.966096	19.627149	10.372850
3869	9.966113	19.627501	10.372499
3870	9.966130	19.627852	10.372148

Sine | Co-sine | Tangent | M

Degree 67.

Degree 23.

M	Sine	Co-sine	Tangent	Co-tang
0	9.591878	9.964026	9.627852	10.372148
1	9.592175	9.963972	9.628203	10.371797
2	9.592473	9.963919	9.628554	10.371446
3	9.592770	9.963865	9.628905	10.371095
4	9.593067	9.963811	9.629255	10.370744
5	9.593363	9.963757	9.629606	10.370393
6	9.593658	9.963703	9.629956	10.370042
7	9.593955	9.963650	9.630306	10.369691
8	9.594251	9.963596	9.630655	10.369340
9	9.594547	9.963542	9.631005	10.368989
10	9.594842	9.963488	9.631354	10.368638
11	9.595137	9.963433	9.631704	10.368287
12	9.595432	9.963379	9.632053	10.367936
13	9.595727	9.963325	9.632401	10.367585
14	9.596021	9.963271	9.632750	10.367234
15	9.596315	9.963217	9.633098	10.366883
16	9.596610	9.963162	9.633447	10.366532
17	9.596903	9.963108	9.633795	10.366181
18	9.597196	9.963054	9.634143	10.365830
19	9.597490	9.962999	9.634490	10.365479
20	9.597783	9.962945	9.634838	10.365128
21	9.598075	9.962892	9.635185	10.364777
22	9.598368	9.962836	9.635530	10.364426
23	9.598660	9.962781	9.635879	10.364075
24	9.598952	9.962726	9.636226	10.363724
25	9.599244	9.962672	9.636572	10.363373
26	9.59953	9.962617	9.636918	10.363022
27	9.599827	9.962562	9.637265	10.362671
28	9.600118	9.962507	9.637610	10.362320
29	9.600409	9.962453	9.637956	10.361969
30	9.600700	9.962398	9.638302	10.361618
Co-sine Sine Co-tang. Tang.				

Degree 66.

Degree 23.

Sine	Co-sine.	Tangent	Co-tang.
600700	9.9623981	19.6383021	10.361698130
600990	9.9623431	9.638647	10.361353129
601280	9.962288	9.638992	10.361007128
601570	9.962233	9.639337	10.360662127
601860	9.962178	9.639682	10.360318126
602149	9.962122	9.640027	10.369973125
602439	9.962067	9.640371	10.359624124
602728	9.962012	9.640716	10.359284123
603017	9.961957	9.641060	10.358940122
603305	9.961902	9.641404	10.358596121
603594	9.961846	9.641747	10.358253120
603882	9.961791	9.642091	10.357909119
604170	9.961735	9.642434	10.357566118
604457	9.961680	9.642777	10.357222117
604745	9.961624	9.643120	10.356980116
605032	9.961569	9.643463	10.356637115
605319	9.961513	9.643806	10.356294114
605606	9.961458	9.644148	10.355952113
605892	9.961402	9.644490	10.355610112
606179	9.961346	9.644832	10.355268111
606465	9.961290	9.645174	10.354926110
606750	9.961235	9.645516	10.3545849
607036	9.961179	9.645857	10.3542428
607322	9.961123	9.646199	10.3538017
607607	9.961067	9.646540	10.3534606
607892	9.961011	9.646881	10.3531195
608175	9.960955	9.647222	10.3527784
608451	9.960899	9.647562	10.3524383
608745	9.960842	9.647903	10.3520972
609029	9.960786	9.648243	10.3517571
609313	9.960730	9.648583	10.3514170

Sine | Co-sine. | Tangent | Co-tang.

Degree 66.

Degree 24.

M	Sine	Co-sine	Tangent	Co-tang.
00	60931319	9607301	9648583	1035141
1	6095971	9606741	9648913	1035107
2	6098861	9606171	9649263	1035077
3	6101631	9605611	9649603	1035047
4	6104461	9605051	9649943	1035017
5	6107291	9604481	9650281	1034987
6	6110121	9603921	9650620	1034957
7	6112941	9603351	9650959	1034927
8	6115761	9602791	9651297	1034897
9	6118581	9602221	9651630	1034867
10	6121401	9601651	9651974	1034837
11	6124211	9601091	9652312	1034807
12	6127021	9600521	9652650	1034777
13	6129831	9599951	9652988	1034747
14	6132641	9599381	9653326	1034717
15	6135451	9598811	9653663	1034687
16	6138251	9598241	9654000	1034657
17	6141051	9597681	9654337	1034627
18	6143851	9597101	9654674	1034597
19	6146651	9596531	9655011	1034567
20	6149441	9595961	9655348	1034537
21	6152231	9595391	9655684	1034507
22	6155021	9594821	9656020	1034477
23	6157811	9594251	9656356	1034447
24	6160601	9593671	9656692	1034417
25	6163381	9593101	9657028	1034387
26	6166161	9592531	9657363	1034357
27	6168941	9591951	9657699	1034327
28	6171721	9591381	9658034	1034297
29	6174501	9590801	9658369	1034267
30	6177271	9590231	9658704	1034237
Co-sine Sine Co-tang. Tangent				

Degree 65.

Degree 24.

Sine	Co-sine	Tangent	Co-tang.
9177279	99590231	9.658704	10.341296
918004	9958965	9.659039	10.340926
918281	9958908	9.659373	10.340527
918558	9958850	9.659708	10.340123
918834	9958792	9.660042	10.339718
919110	9958734	9.660376	10.339314
919386	9958677	9.660710	10.338909
919662	9958619	9.661043	10.338505
919938	9958561	9.661377	10.338101
920213	9958503	9.661710	10.337696
920489	9958445	9.662043	10.337292
920765	9958387	9.662376	10.336888
921041	9958329	9.662709	10.336484
921317	9958271	9.663042	10.336080
921593	9958212	9.663374	10.335676
921869	9958154	9.663707	10.335272
922145	9958096	9.664039	10.334868
922421	9958038	9.664371	10.334464
922697	9957979	9.664703	10.334060
922973	9957921	9.665035	10.333656
923249	9957862	9.665366	10.333252
923525	9957804	9.665697	10.332848
923801	9957745	9.666029	10.332444
924077	9957687	9.666360	10.332040
924353	9957628	9.666691	10.331636
924629	9957570	9.667021	10.331232
924905	9957511	9.667352	10.330828
925181	9957452	9.667682	10.330424
925457	9957393	9.668012	10.330020
925733	9957334	9.668343	10.329616
926009	9957276	9.668672	10.329212

Tan	Sine	Co-tang.	Tangent
Degree 65.			

Degree 25.

M | Sine | Co-sine | Tangent | Co-tang.

0 | 9,625948 | 9,957276 | 9,668672 | 10,33139

1 | 9,626219 | 9,957217 | 9,669002 | 10,33099

2 | 9,626490 | 9,957158 | 9,669332 | 10,33060

3 | 9,626750 | 9,957099 | 9,669661 | 10,33021

4 | 9,627030 | 9,957040 | 9,669990 | 10,33000

5 | 9,627300 | 9,956981 | 9,670320 | 10,32968

6 | 9,627570 | 9,956922 | 9,670645 | 10,32931

7 | 9,627840 | 9,956862 | 9,670977 | 10,32890

8 | 9,628109 | 9,956803 | 9,671306 | 10,32860

9 | 9,628378 | 9,956744 | 9,671634 | 10,32829

10 | 9,628697 | 9,956684 | 9,671963 | 10,32800

11 | 9,628916 | 9,956625 | 9,672291 | 10,32770

12 | 9,629184 | 9,956565 | 9,672619 | 10,32739

13 | 9,629453 | 9,956506 | 9,672947 | 10,32709

14 | 9,629721 | 9,956445 | 9,673274 | 10,32679

15 | 9,629989 | 9,956387 | 9,673603 | 10,32649

16 | 9,630257 | 9,956327 | 9,673929 | 10,32619

17 | 9,630524 | 9,956267 | 9,674256 | 10,32589

18 | 9,630792 | 9,956208 | 9,674584 | 10,32559

19 | 9,631059 | 9,956148 | 9,674910 | 10,32529

20 | 9,631326 | 9,956088 | 9,675237 | 10,32499

21 | 9,631592 | 9,956029 | 9,675564 | 10,32469

22 | 9,631856 | 9,955969 | 9,675890 | 10,32439

23 | 9,632125 | 9,955909 | 9,676216 | 10,32409

24 | 9,632392 | 9,955849 | 9,676543 | 10,32379

25 | 9,632657 | 9,955789 | 9,676869 | 10,32349

26 | 9,632923 | 9,955735 | 9,677194 | 10,32319

27 | 9,633189 | 9,955675 | 9,677520 | 10,32289

28 | 9,633454 | 9,955609 | 9,677845 | 10,32259

29 | 9,633719 | 9,955548 | 9,678171 | 10,32229

30 | 9,633984 | 9,955488 | 9,678496 | 10,32199

| Co-sine | Sine | Co-tang. Tan.

Degree 64.

Degree 25.

Sine	Co-sine	Tangent	Co-tang.
3984	9.955488	19.678496	10.321504
4249	9.955428	19.678821	10.321179
4514	9.955367	9.679146	10.320854
4778	9.955307	9.679471	10.320529
5042	9.955246	9.679795	10.320205
5306	9.955186	9.680120	10.319880
5570	9.955123	9.680444	10.319556
5833	9.955065	9.680768	10.319232
6097	9.955004	9.681092	10.318908
6360	9.954944	9.681416	10.318584
6623	9.954883	9.681740	10.318260
6886	9.954823	9.682063	10.317937
7148	9.954762	9.682386	10.317613
7411	9.954701	9.682710	10.317290
7673	9.954640	9.683033	10.316967
7935	9.954579	9.683356	10.316644
8197	9.954518	9.683678	10.316321
8458	9.954457	9.684001	10.315999
8720	9.954396	9.684324	10.315676
8981	9.954335	9.684646	10.315354
9242	9.954274	9.684968	10.315032
9503	9.954213	9.685290	10.314710
9764	9.954152	9.685612	10.314388
10024	9.954090	9.685934	10.314066
10284	9.954029	9.686255	10.313745
10544	9.954968	9.686577	10.313423
10804	9.953906	9.686898	10.313102
11064	9.953845	9.687219	10.312781
11323	9.953783	9.687540	10.312460
11583	9.953722	9.687861	10.312138
11842	9.953660	9.688182	10.311818

Sine | Co-tang | Tangent | M

Degree 64.

Degree 26.

M	Sine	Co-sine	Tangent	Co-tang
0	9.641842	9.953660	19.688182	10.311818
1	9.642101	9.953598	19.688502	10.311498
2	9.642360	9.953537	19.688823	10.311179
3	9.642618	9.953475	19.689143	10.310860
4	9.642876	9.953413	19.689463	10.310541
5	9.643135	9.953351	19.689783	10.310222
6	9.643393	9.953290	19.690103	10.309903
7	9.643650	9.953228	19.690423	10.309584
8	9.643908	9.953166	19.690743	10.309265
9	9.644165	9.953104	19.691063	10.308946
10	9.644423	9.953042	19.691381	10.308627
11	9.644680	9.952980	19.691700	10.308308
12	9.644936	9.952917	19.692019	10.307989
13	9.645193	9.952855	19.692338	10.307670
14	9.645449	9.952793	19.692656	10.307351
15	9.645706	9.952731	19.692975	10.307032
16	9.645962	9.952668	19.693293	10.306713
17	9.646218	9.952606	19.693612	10.306394
18	9.646473	9.952544	19.693930	10.306075
19	9.646729	9.952481	19.694248	10.305756
20	9.646984	9.952419	19.694566	10.305437
21	9.647239	9.952356	19.694883	10.305118
22	9.647494	9.952294	19.695201	10.304799
23	9.647749	9.952231	19.695518	10.304480
24	9.648004	9.952168	19.695835	10.304161
25	9.648258	9.952105	19.696153	10.303842
26	9.648510	9.952043	19.696470	10.303523
27	9.648766	9.951980	19.696786	10.303204
28	9.648020	9.951917	19.697103	10.302885
29	9.649274	9.951854	19.697420	10.302566
30	9.649527	9.951791	19.697738	10.302247
Co-sine		Sine	Co-tang.	Tang.

Degree 63.

Degree 26.

Co-sine	Tangent	Co-tang.
9527.9 951791	19.697738	10.302264 30
9781.9 951728	9.698052	10.301947 29
0034.9 951665	9.698369	10.301631 28
0287.9 951602	9.698685	10.301315 27
0519.9 951539	9.699001	10.300999 26
0498.9 951476	9.699316	10.300684 25
1044.9 951412	9.699632	10.300368 24
1296.9 951349	9.699947	10.300052 23
1648.9 951286	9.700263	10.299737 22
1800.9 951222	9.700578	10.299422 21
2052.9 951159	9.700893	10.299107 20
2303.9 951095	9.701208	10.298792 19
2554.9 951032	9.701522	10.298477 18
2806.9 950968	9.701837	10.298163 17
3057.9 950905	9.702152	10.297848 16
3307.9 950841	9.702466	10.297534 15
3558.9 950777	9.702782	10.297216 14
3808.9 950714	9.703095	10.296905 13
4059.9 950650	9.703409	10.296591 12
4309.9 950589	9.703722	10.296277 11
4558.9 950522	9.704036	10.295964 10
4808.9 950458	9.704350	10.295650 9
5057.9 950394	9.704663	10.295337 8
5307.9 950330	9.704976	10.295023 7
5556.9 950266	9.705290	10.294710 6
5805.9 950202	9.705603	10.294397 5
6053.9 950138	9.705915	10.294084 4
6303.9 950074	9.706228	10.293771 3
6550.9 950009	9.706541	10.293459 2
6799.9 949945	9.706853	10.293146 1
7047.9 949881	9.707166	10.292834 0

T Co-sine | Sine | Co-tang. | Tangent |

Degree 63.

Degree 27.

M	Sine	Co sine	Tangent	Co
0	9.657047	9.949886	9.707166	10.29
1	9.657295	9.949816	9.707478	10.29
2	9.657542	9.949752	9.707790	10.29
3	9.657790	9.949687	9.708102	10.29
4	9.658037	9.949623	9.708414	10.29
5	9.658284	9.949558	9.708726	10.29
6	9.658538	9.949494	9.709037	10.29
7	9.658777	9.949429	9.709349	10.29
8	9.659024	9.949364	9.709660	10.29
9	9.659271	9.949300	9.709971	10.29
10	9.659517	9.949235	9.710282	10.29
11	9.659763	9.949170	9.710593	10.29
12	9.660009	9.949105	9.710904	10.29
13	9.660255	9.949040	9.711214	10.29
14	9.660500	9.948976	9.711525	10.29
15	9.660746	9.948910	9.711836	10.29
16	9.660991	9.948845	9.712146	10.29
17	9.661236	9.948780	9.712456	10.29
18	9.661481	9.948715	9.712766	10.29
19	9.661726	9.948650	9.713076	10.29
20	9.661970	9.948584	9.713386	10.29
21	9.662214	9.948519	9.713695	10.29
22	9.662459	9.948453	9.714005	10.29
23	9.662702	9.948388	9.714314	10.29
24	9.662947	9.948323	9.714624	10.29
25	9.663190	9.948257	9.714933	10.29
26	9.663433	9.948191	9.715242	10.29
27	9.663677	9.948126	9.715550	10.29
28	9.66392	9.948060	9.715859	10.29
29	9.664163	9.947995	9.716168	10.29
30	9.664406	9.947929	9.716477	10.29
	Co sine	Sine	Co tang.	T

Degree 62.

Degree 27.

Sine	Co-sine.	Tangent	Co-tang.
64406	9.947929	19.716477	10.283523
64648	9.947863	9.716785	10.283215
64891	9.947797	9.717093	10.282907
65133	9.947731	9.717401	10.282598
65375	9.947665	9.717709	10.282290
65617	9.947599	9.718017	10.281983
65858	9.947533	9.718325	10.281673
66100	9.947467	9.718633	10.281367
66341	9.947401	9.718940	10.281060
66583	9.947335	9.719248	10.280752
66824	9.947269	9.719555	10.280445
67065	9.947203	9.719862	10.280138
67305	9.947136	9.720169	10.279831
67546	9.947070	9.720476	10.279524
67786	9.947004	9.720783	10.279217
68025	9.946937	9.721089	10.278911
68266	9.946871	9.721395	10.278604
68506	9.946804	9.721702	10.278298
68746	9.946738	9.722008	10.277991
68986	9.946671	9.722315	10.277685
69225	9.946604	9.722621	10.277379
69464	9.946537	9.722927	10.277073
69703	9.946471	9.723232	10.276768
69942	9.946404	9.723538	10.276462
70181	9.946337	9.723843	10.276156
70419	9.946270	9.724149	10.275851
70657	9.946203	9.724454	10.275546
70896	9.946136	9.724759	10.275240
71134	9.946069	9.725065	10.274935
71372	9.946002	9.725369	10.274630
71609	9.945935	9.725674	10.274326

Sine | Co-sine. | Tangent | M

Degree 62.

Degree 28.

M	Sine	Co-sine	Tangent	Co-tang.
0	9,671690	9,945935	9,725674	10,274326
1	9,671847	9,945868	9,725979	10,274021
2	9,672084	9,945800	9,726282	10,273716
3	9,672321	9,945733	9,726588	10,273411
4	9,672558	9,945666	9,726892	10,273106
5	9,672795	9,945598	9,727197	10,272801
6	9,673032	9,945531	9,727501	10,272496
7	9,673268	9,945463	9,727805	10,272191
8	9,673504	9,945396	9,728109	10,271886
9	9,673741	9,945328	9,728413	10,271581
10	9,673977	9,945261	9,728716	10,271276
11	9,674213	9,945193	9,729020	10,270971
12	9,674448	9,945125	9,729323	10,270666
13	9,674684	9,945058	9,729626	10,270361
14	9,674919	9,944990	9,729929	10,270056
15	9,675154	9,944922	9,730232	10,269751
16	9,675389	9,944854	9,730535	10,269446
17	9,675623	9,944786	9,730838	10,269141
18	9,675859	9,944718	9,731141	10,268836
19	9,676094	9,944650	9,731445	10,268531
20	9,676328	9,944582	9,731746	10,268226
21	9,676562	9,944514	9,732048	10,267921
22	9,676796	9,944446	9,732351	10,267616
23	9,677030	9,944377	9,732653	10,267311
24	9,677264	9,944309	9,732955	10,267006
25	9,677497	9,944241	9,733257	10,266701
26	9,677731	9,944172	9,733558	10,266396
27	9,677964	9,944104	9,733860	10,266091
28	9,678197	9,944036	9,734162	10,265786
29	9,678430	9,943967	9,734463	10,265481
30	9,678663	9,943898	9,734764	10,265176
Co-sine		Sine	Co-tang.	Tang.

Degree 61.

Degree 28.

ne	Co-fine	Tangent	Co-tang.
8663	9,943898	9,734764	10,265236
8895	9,943830	9,735666	10,264934
9128	9,943761	9,735362	10,264633
9360	9,943692	9,735668	10,264332
9592	9,943624	9,735968	10,264031
9824	9,943555	9,736269	10,263731
10056	9,943486	9,736570	10,263430
10288	9,943417	9,736870	10,263130
10519	9,943348	9,737171	10,262829
10750	9,943279	9,737471	10,262529
10982	9,943210	9,737771	10,262229
11213	9,943141	9,738071	10,261929
11443	9,943072	9,738371	10,261629
11674	9,943003	9,738671	10,261329
11904	9,942933	9,738971	10,261029
12135	9,942864	9,739271	10,260729
12365	9,942795	9,739570	10,260430
12595	9,942725	9,739870	10,260130
12825	9,942656	9,740169	10,259831
13055	9,942587	9,740468	10,259532
13284	9,942517	9,740767	10,259233
13514	9,942448	9,741066	10,258934
13743	9,942378	9,741365	10,258635
13972	9,942308	9,741664	10,258336
14201	9,942239	9,741962	10,258038
14430	9,942169	9,742261	10,257739
14658	9,942099	9,742559	10,257441
14887	9,942029	9,742858	10,257142
15116	9,941959	9,743156	10,256844
15343	9,941889	9,743454	10,256546
15571	9,941819	9,743753	10,256248
ne	Sine	Co-tang.	Tangent.

Degree 61.

Degree 29.

M	Sine	Co-sine	Tangent	Co-tang
0	9,68557	9,941819	9,743752	10,2562
1	9,685799	9,941749	9,744050	10,2559
2	9,686027	9,941679	9,744348	10,2556
3	9,686254	9,941609	9,744645	10,2553
4	9,686481	9,941539	9,744943	10,2550
5	9,686709	9,941468	9,745240	10,2547
6	9,686936	9,941398	9,745538	10,2544
7	9,687163	9,941328	9,745835	10,2541
8	9,687389	9,941257	9,746133	10,2538
9	9,687616	9,941187	9,746429	10,2535
10	9,687842	9,941116	9,746726	10,2532
11	9,688069	9,941046	9,747023	10,2529
12	9,688295	9,940975	9,747319	10,2526
13	9,688523	9,940905	9,747616	10,2523
14	9,688747	9,940834	9,747912	10,2520
15	9,688972	9,940763	9,748209	10,2517
16	9,689198	9,940693	9,748505	10,2514
17	9,689421	9,940622	9,748801	10,2511
18	9,689648	9,940551	9,749097	10,2508
19	9,689873	9,940480	9,749393	10,2505
20	9,690098	9,940409	9,749689	10,2502
21	9,690323	9,940338	9,749985	10,2499
22	9,690548	9,940267	9,750281	10,2496
23	9,690772	9,940196	9,750576	10,2493
24	9,690996	9,940125	9,750872	10,2490
25	9,691220	9,940053	9,751167	10,2487
26	9,691444	9,939982	9,751462	10,2484
27	9,691668	9,939911	9,751757	10,2481
28	9,691892	9,939840	9,752052	10,2478
29	9,692115	9,939768	9,752347	10,2475
30	9,692339	9,939697	9,752642	10,2472
1	Co-sine	Sine	Co-tang.	Tan

Degree 60.

Degree 29.

	Co-sine	Tangent	Co-tang.	
339	9.9396971	19.752642	10.247358	30
362	9.939625	9.752937	10.247063	29
378	9.939554	9.753231	10.246769	28
390	9.939482	9.753526	10.246474	27
423	9.939410	9.753820	10.246180	26
453	9.939339	9.754115	10.245885	25
467	9.939267	9.754409	10.245591	24
488	9.939195	9.754703	10.245297	23
512	9.939123	9.754997	10.245003	22
542	9.939051	9.755291	10.244709	21
564	9.938980	9.755584	10.244415	20
576	9.938908	9.755878	10.244122	19
607	9.938835	9.756172	10.243828	18
629	9.938763	9.756465	10.243535	17
640	9.938691	9.756759	10.243241	16
671	9.938619	9.757052	10.242948	15
682	9.938547	9.757345	10.242655	14
713	9.938475	9.757648	10.242362	13
734	9.938402	9.757931	10.242069	12
754	9.938330	9.758224	10.241776	11
774	9.938257	9.758517	10.241483	10
795	9.938185	9.758810	10.241190	9
815	9.938112	9.759102	10.240898	8
835	9.938040	9.759395	10.240605	7
854	9.937967	9.759687	10.240313	6
874	9.937895	9.759979	10.240021	5
893	9.937822	9.760271	10.239728	4
913	9.937749	9.760564	10.239436	3
932	9.937676	9.760856	10.239144	2
951	9.937603	9.761147	10.238852	1
970	9.937531	9.761439	10.238561	0
	Sine	Co-tang.	Tangent.	M

Degree 60.

Z

Degree 30.

M	Sine	Co-sine	Tangent	Co-tan
0	9.698970	9.937531	9.761439	10.238561
1	9.699189	9.937458	9.761731	10.238371
2	9.699407	9.937385	9.762023	10.238181
3	9.699626	9.937312	9.762314	10.237991
4	9.699844	9.937238	9.762606	10.237801
5	9.700062	9.937165	9.762897	10.237611
6	9.700280	9.937092	9.763188	10.237421
7	9.700498	9.937019	9.763479	10.237231
8	9.700716	9.936945	9.763770	10.237041
9	9.700933	9.936872	9.764061	10.236851
10	9.701151	9.936799	9.764352	10.236661
11	9.701367	9.936725	9.764643	10.236471
12	9.701585	9.936652	9.764933	10.236281
13	9.701802	9.936578	9.765224	10.236091
14	9.702019	9.936505	9.765514	10.235901
15	9.702236	9.936431	9.765805	10.235711
16	9.702452	9.936357	9.766095	10.235521
17	9.702669	9.936284	9.766385	10.235331
18	9.702885	9.936210	9.766675	10.235141
19	9.703101	9.936136	9.766965	10.234951
20	9.703317	9.936062	9.767255	10.234761
21	9.703533	9.935988	9.767545	10.234571
22	9.703748	9.935914	9.767834	10.234381
23	9.703964	9.935840	9.768124	10.234191
24	9.704179	9.935766	9.768413	10.234001
25	9.704395	9.935692	9.768703	10.233811
26	9.704610	9.935618	9.768992	10.233621
27	9.704825	9.935543	9.769281	10.233431
28	9.705040	9.935469	9.769570	10.233241
29	9.705254	9.935395	9.769859	10.233051
30	9.705469	9.935320	9.770148	10.232861
Co-sine		Sine	Co-tan	Tan

Degree 59.

Degree 30.

Co-sine	Tangent	Co-tang.
9.933320	9.770148	10.22985230
9.933246	9.770437	10.22956320
9.933171	9.770726	10.22927428
9.933097	9.771015	10.22898527
9.933022	9.771303	10.22869726
9.932948	9.771592	10.22840825
9.932873	9.771880	10.22812024
9.932798	9.772168	10.22783223
9.932723	9.772456	10.22754322
9.932649	9.772745	10.22725521
9.932574	9.773033	10.22696720
9.932499	9.773321	10.22667919
9.932424	9.773608	10.22639118
9.932349	9.773896	10.22610417
9.932274	9.774184	10.22581616
9.932199	9.774471	10.22552915
9.932123	9.774759	10.22524114
9.932048	9.775046	10.22495413
9.931973	9.775333	10.22466612
9.931897	9.775621	10.22437911
9.931822	9.775908	10.22409210
9.931747	9.776195	10.22380509
9.931671	9.776482	10.22351808
9.931596	9.776768	10.22323207
9.931520	9.777055	10.22294506
9.931444	9.777342	10.22265805
9.931369	9.777628	10.22237204
9.931293	9.777915	10.22208503
9.931217	9.778201	10.22179902
9.931141	9.778487	10.22151301
9.931065	9.778774	10.22122600

Co-sine | Sine | Co-tang. | Tangent

Degree 59.

Degree 31.

	Sine	Co-sine	Tangent	Co-tang.
0	9.711839	9.933065	19.778774	10.221226
1	9.712049	9.932990	9.779060	10.221140
2	9.712259	9.932914	9.779346	10.221054
3	9.712469	9.932838	9.779632	10.220968
4	9.712679	9.932761	9.779918	10.220882
5	9.712889	9.932685	9.780203	10.220796
6	9.713098	9.932609	9.780489	10.220710
7	9.713308	9.932533	9.780775	10.220624
8	9.713517	9.932457	9.781060	10.220538
9	9.713726	9.932380	9.781346	10.220452
10	9.713935	9.932304	9.781631	10.220366
11	9.714144	9.932227	9.781916	10.220280
12	9.714352	9.932151	9.782202	10.220194
13	9.714561	9.932074	9.782488	10.220108
14	9.714769	9.931998	9.782771	10.220022
15	9.714977	9.931921	9.783056	10.219936
16	9.715186	9.931845	9.783341	10.219850
17	9.715394	9.931768	9.783626	10.219764
18	9.715601	9.931691	9.783910	10.219678
19	9.715809	9.931614	9.784195	10.219592
20	9.716017	9.931537	9.784479	10.219506
21	9.716224	9.931460	9.784764	10.219420
22	9.716431	9.931383	9.785048	10.219334
23	9.716639	9.931306	9.785332	10.219248
24	9.716846	9.931229	9.785616	10.219162
25	9.717053	9.931152	9.785900	10.219076
26	9.717259	9.931075	9.786184	10.218990
27	9.717466	9.930998	9.786468	10.218904
28	9.717672	9.930920	9.786751	10.218818
29	9.717879	9.930843	9.787036	10.218732
30	9.718085	9.930766	9.787319	10.218646
	Co-sine	Sine	Co-tang.	Tang.

Degree 58.

Degree 31.

Sine	Co-sine	Tangent	Co-tang.
71888	9.930766	19.787319	10.212681
71891	9.930688	9.787603	10.212397
71897	9.930611	9.787826	10.212114
71893	9.930533	9.788170	10.211830
71892	9.930456	9.788453	10.211547
719114	9.930378	9.788736	10.211264
19320	9.930300	9.789019	10.210981
19525	9.930223	9.789302	10.210698
19730	9.930145	9.789585	10.210415
19935	9.930067	9.789868	10.210132
20140	9.929989	9.790151	10.209849
20345	9.929911	9.790433	10.209565
20549	9.929833	9.790716	10.209284
20754	9.929755	9.790999	10.209001
20958	9.929677	9.791281	10.208719
21162	9.929599	9.791563	10.208436
21366	9.929521	9.791846	10.208154
21570	9.929442	9.792128	10.207872
21774	9.929364	9.792410	10.207590
21978	9.929286	9.792692	10.207308
22181	9.929207	9.792974	10.207024
22385	9.929129	9.793256	10.206744
22588	9.929050	9.793538	10.206462
22791	9.928972	9.793819	10.206180
22994	9.928893	9.794101	10.205899
23197	9.928814	9.794383	10.205617
23400	9.928736	9.794664	10.205336
23603	9.928657	9.794945	10.205054
23806	9.928578	9.795227	10.204773
24007	9.928499	9.795508	10.204492
24210	9.928420	9.795789	10.204211
Sine	Co-sine	Tangent	Co-tang.

Degree 58.

Degree 31.

M	Sine	Co-sine	Tangent	Co-tang.
0	9,724210	9,928420	9,795789	10,204210
1	9,724412	9,928341	9,796070	10,204399
2	9,724614	9,928262	9,796351	10,204588
3	9,724816	9,928183	9,796632	10,204777
4	9,725017	9,928104	9,796913	10,204966
5	9,725219	9,928025	9,797194	10,205155
6	9,725420	9,927946	9,797474	10,205344
7	9,725622	9,927867	9,797755	10,205533
8	9,725823	9,927787	9,798036	10,205722
9	9,726024	9,927708	9,798316	10,205911
10	9,726225	9,927628	9,798596	10,206100
11	9,726426	9,927549	9,798877	10,206289
12	9,726626	9,927469	9,799157	10,206478
13	9,726827	9,927390	9,799437	10,206667
14	9,727027	9,927310	9,799717	10,206856
15	9,727228	9,927231	9,799997	10,207045
16	9,727428	9,927151	9,800277	10,207234
17	9,727628	9,927072	9,800557	10,207423
18	9,727828	9,926992	9,800836	10,207612
19	9,728027	9,926912	9,801116	10,207801
20	9,728227	9,926832	9,801396	10,207990
21	9,728427	9,926752	9,801675	10,208179
22	9,728626	9,926672	9,801955	10,208368
23	9,728825	9,926592	9,802234	10,208557
24	9,729024	9,926512	9,802513	10,208746
25	9,729223	9,926432	9,802792	10,208935
26	9,729422	9,926352	9,803072	10,209124
27	9,729621	9,926272	9,803351	10,209313
28	9,729820	9,926192	9,803630	10,209502
29	9,730018	9,926112	9,803908	10,209691
30	9,730216	9,926032	9,804187	10,209880
Co-sine Sine Co-tang. Tan				

Degree 57.

Degree 32.

Sine	Co-sine	Tangent	Co-tang.
30216	9,926029	19,804187	10,195813
30415	9,925949	9,804466	10,195534
30613	9,925868	9,804745	10,195255
30811	9,925787	9,805023	10,194977
31009	9,925707	9,805302	10,194698
31206	9,925626	9,805580	10,194420
31404	9,925545	9,805859	10,194141
31601	9,925464	9,806137	10,193863
31799	9,925384	9,806415	10,193585
31996	9,925303	9,806693	10,193309
32193	9,925222	9,806971	10,193028
32390	9,925141	9,807249	10,192751
32587	9,925060	9,807527	10,192473
32784	9,924978	9,807805	10,192195
32980	9,924897	9,808083	10,191917
33177	9,924816	9,808361	10,191639
33373	9,924735	9,808638	10,191362
33569	9,924653	9,808916	10,191084
33765	9,924572	9,809193	10,190807
33961	9,924491	9,809471	10,190529
34157	9,924409	9,809748	10,190252
34353	9,924328	9,810025	10,189975
34548	9,924246	9,810302	10,189697
34744	9,924164	9,810580	10,189420
34939	9,924083	9,810857	10,189143
35134	9,924001	9,811134	10,188866
35330	9,923919	9,811410	10,188589
35525	9,923837	9,811687	10,188313
35719	9,923755	9,811964	10,188036
35914	9,923673	9,812241	10,187759
36109	9,923591	9,812517	10,187483
Sine	Co-sine	Tangent	Co-tang.

Degree 57.

Degree 33.

Mt	Sine	Co-sine	Tangent	Co-tang
0	9,736109	9,923591	9,812517	10,187482
1	9,736309	9,923509	9,812794	10,187195
2	9,736497	9,923427	9,813070	10,186908
3	9,736692	9,923345	9,813347	10,186621
4	9,736886	9,923263	9,813623	10,186334
5	9,737080	9,923180	9,813899	10,186047
6	9,737274	9,923098	9,814173	10,185760
7	9,737467	9,923016	9,814452	10,185473
8	9,737661	9,922933	9,814728	10,185186
9	9,737854	9,922851	9,815004	10,184899
10	9,738048	9,922768	9,815279	10,184612
11	9,738241	9,922686	9,815555	10,184325
12	9,738434	9,922603	9,815831	10,184038
13	9,738627	9,922520	9,816107	10,183751
14	9,738820	9,922438	9,816383	10,183464
15	9,739013	9,922355	9,816658	10,183177
16	9,739205	9,922272	9,816933	10,182890
17	9,739398	9,922189	9,817209	10,182603
18	9,739590	9,922106	9,817484	10,182316
19	9,739783	9,922023	9,817759	10,182029
20	9,739975	9,921940	9,818035	10,181742
21	9,740167	9,921857	9,818310	10,181455
22	9,740359	9,921774	9,818585	10,181168
23	9,740550	9,921691	9,818860	10,180881
24	9,740742	9,921607	9,819135	10,180594
25	9,740934	9,921524	9,819410	10,180307
26	9,741125	9,921441	9,819684	10,180020
27	9,741316	9,921357	9,819959	10,179733
28	9,741507	9,921274	9,820234	10,179446
29	9,741698	9,921190	9,820508	10,179159
30	9,741889	9,921107	9,820783	10,178872
Co-sine		Sine	Co-tang.	Tan

Degree 56.

Degree 33.

	Co-sine	Tangent	Co-tang.	
889	9.921107	9.820783	10.179217	30
080	9.921023	9.821057	10.178943	29
271	9.920939	9.821332	10.178668	28
461	9.920855	9.821606	10.178394	27
652	9.920772	9.821880	10.178120	26
842	9.920688	9.822154	10.177846	25
032	9.920604	9.822429	10.177571	24
223	9.920520	9.822703	10.177297	23
412	9.920436	9.822977	10.177023	22
602	9.920352	9.823250	10.176739	21
792	9.920268	9.823524	10.176476	20
82	9.920184	9.823798	10.176202	19
71	9.920099	9.824072	10.175928	18
61	9.920015	9.824345	10.175655	17
50	9.919931	9.824619	10.175381	16
39	9.919846	9.824892	10.175108	15
28	9.919762	9.825166	10.174834	14
17	9.919677	9.825439	10.174560	13
06	9.919593	9.825713	10.174287	12
94	9.919508	9.825986	10.174014	11
83	9.919424	9.826259	10.173741	10
71	9.919339	9.826532	10.173468	9
59	9.919254	9.826805	10.173195	8
48	9.919169	9.827078	10.172922	7
36	9.919084	9.827351	10.172649	6
24	9.918999	9.827624	10.172376	5
11	9.918915	9.827897	10.172103	4
99	9.918830	9.828170	10.171830	3
87	9.918744	9.828442	10.171558	2
74	9.918659	9.828715	10.171285	1
62	9.918574	9.828987	10.171012	0

	Sine	Co-tang.	Tangent.
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Degree 56.

A a

Degree 34.

M	Sine	Co-sine	Tangent	Co-tang
	09.747562	9.918574	19.828987	10.171013
1	9.747749	9.918489	9.829260	10.170740
2	9.747936	9.918404	9.829532	10.170467
3	9.748123	9.918318	9.829805	10.170194
4	9.748310	9.918233	9.830077	10.169921
5	9.748497	9.918147	9.830349	10.169648
6	9.748683	9.918062	9.830621	10.169375
7	9.748870	9.917976	9.830893	10.169102
8	9.749056	9.917891	9.831165	10.168829
9	9.749242	9.917805	9.831437	10.168556
10	9.749429	9.917719	9.831709	10.168283
11	9.749615	9.917634	9.831981	10.168010
12	9.749801	9.917548	9.832253	10.167737
13	9.749986	9.917462	9.832525	10.167464
14	9.750172	9.917376	9.832796	10.167191
15	9.750358	9.917290	9.833068	10.166918
16	9.750543	9.917204	9.833339	10.166645
17	9.750729	9.917118	9.833611	10.166372
18	9.750914	9.917032	9.833882	10.166099
19	9.751099	9.916945	9.834154	10.165826
20	9.751284	9.916859	9.834425	10.165553
21	9.751469	9.916773	9.834696	10.165280
22	9.751654	9.916686	9.834967	10.165007
23	9.751838	9.916600	9.835238	10.164734
24	9.752023	9.916514	9.835509	10.164461
25	9.752207	9.916427	9.835780	10.164188
26	9.752392	9.916340	9.836051	10.163915
27	9.752576	9.916254	9.836322	10.163642
28	9.752760	9.916167	9.836593	10.163369
29	9.752944	9.916080	9.836864	10.163096
30	9.753128	9.915994	9.837134	10.162823

Co-sine | Sine | Co-tang | Tang

Degree 55.

Degree 34.

Sine	Co-sine	Tangent	Co-tang.
53128	9.915994	9.837134	10.162866
53312	9.915907	9.837405	10.162595
53496	9.915820	9.837675	10.162325
53679	9.915733	9.837946	10.162054
53862	9.915646	9.838216	10.161784
54046	9.915559	9.838487	10.161513
54229	9.915472	9.838757	10.161243
54412	9.915385	9.839027	10.160973
54595	9.915297	9.839297	10.160702
54778	9.915210	9.839568	10.160432
54960	9.915123	9.839838	10.160162
55143	9.915035	9.840108	10.159892
55325	9.914948	9.840378	10.159622
55508	9.914860	9.840647	10.159352
55690	9.914773	9.840917	10.159083
55872	9.914685	9.841187	10.158813
56054	9.914597	9.841457	10.158543
56236	9.914510	9.841728	10.158273
56418	9.914422	9.841998	10.158004
56600	9.914334	9.842268	10.157734
56781	9.914246	9.842538	10.157465
56963	9.914158	9.842808	10.157195
57144	9.914070	9.843078	10.156926
57326	9.913982	9.843348	10.156657
57507	9.913894	9.843618	10.156387
57688	9.913806	9.843888	10.156118
57869	9.913718	9.844158	10.155849
58049	9.913630	9.844428	10.155580
58230	9.913541	9.844698	10.155311
58411	9.913453	9.844958	10.155042
58591	9.913364	9.845227	10.154774

Sine | Co-tang. | Tangent | M

Degree 55.

Degree 35.

M	Sine	Co-sine	Tangent	Co-tangent
0	9.758391	9.913364	9.845227	10.154773
1	9.758772	9.913276	9.845496	10.154504
2	9.758952	9.913187	9.845764	10.154236
3	9.759132	9.913099	9.846033	10.153968
4	9.759312	9.913010	9.846302	10.153700
5	9.759492	9.912921	9.846570	10.153432
6	9.759572	9.912833	9.846839	10.153164
7	9.759851	9.912744	9.847107	10.152896
8	9.760031	9.912655	9.847376	10.152628
9	9.760210	9.912566	9.847644	10.152360
10	9.760390	9.912477	9.847913	10.152092
11	9.760569	9.912388	9.848181	10.151824
12	9.760748	9.912299	9.848449	10.151556
13	9.760927	9.912210	9.848717	10.151288
14	9.761106	9.912121	9.848985	10.151020
15	9.761285	9.912030	9.849254	10.150752
16	9.761464	9.911942	9.849522	10.150484
17	9.761642	9.911853	9.849789	10.150216
18	9.761821	9.911763	9.850057	10.149948
19	9.761999	9.911674	9.850325	10.149680
20	9.762177	9.911584	9.850593	10.149412
21	9.762356	9.911495	9.850861	10.149144
22	9.762534	9.911405	9.851128	10.148876
23	9.762712	9.911315	9.851396	10.148608
24	9.762889	9.911226	9.851664	10.148340
25	9.763067	9.911136	9.851931	10.148072
26	9.763245	9.911046	9.852199	10.147804
27	9.763422	9.910956	9.852466	10.147536
28	9.763599	9.910866	9.852731	10.147268
29	9.763777	9.910776	9.853001	10.147000
30	9.763954	9.910686	9.853268	10.146732
Co-sine		Sine	Co-tang.	

Degree 54.

Degree 35.

Sine	Co-sine	Tangent	Co-tang.
53954	9.9106861	9.853268	10.1466732
53954	9.910596	9.853532	10.146465
53954	9.910506	9.853802	10.146198
53954	9.910415	9.854069	10.145970
53954	9.910325	9.854336	10.145664
53954	9.910235	9.854603	10.145397
53954	9.910144	9.854870	10.145130
53954	9.910054	9.855137	10.144863
53954	9.909963	9.855404	10.144596
53954	9.909873	9.855671	10.144329
53954	9.909782	9.855937	10.144063
53954	9.909691	9.856204	10.143795
53954	9.909601	9.856471	10.143529
53954	9.909510	9.856737	10.143268
53954	9.909419	9.857004	10.142996
53954	9.909328	9.857270	10.142730
53954	9.909237	9.857537	10.142463
53954	9.909146	9.857803	10.142197
53954	9.909055	9.858069	10.141931
53954	9.908964	9.858336	10.141664
53954	9.908873	9.858602	10.141398
53954	9.908781	9.858868	10.141132
53954	9.908690	9.859134	10.140866
53954	9.908599	9.859400	10.140600
53954	9.908507	9.859666	10.140334
53954	9.908416	9.859932	10.140068
53954	9.908324	9.860198	10.139802
53954	9.908233	9.860464	10.139536
53954	9.908141	9.860730	10.139270
53954	9.908049	9.860995	10.139003
53954	9.907958	9.861261	10.138739

Sine | Co-sine | Tangent | Co-tang.

Degree 54.

Degree 36.

M	Sine	Co-sine	Tangent	Co-tang.
	9,769229	9,9079581	9,861261	10,1377
1	9,769392	9,907866	9,861527	10,1378
2	9,769566	9,907774	9,861792	10,1379
3	9,769740	9,907682	9,862058	10,1380
4	9,769913	9,907590	9,862323	10,1381
5	9,770087	9,907498	9,862589	10,1382
6	9,770260	9,907406	9,862854	10,1383
7	9,770433	9,907314	9,863119	10,1384
8	9,770606	9,907223	9,863385	10,1385
9	9,770779	9,907129	9,863650	10,1386
10	9,770952	9,907037	9,863915	10,1387
11	9,771125	9,906945	9,864180	10,1388
12	9,771298	9,906852	9,864445	10,1389
13	9,771470	9,906760	9,864710	10,1390
14	9,771643	9,906667	9,864975	10,1391
15	9,771815	9,906574	9,865240	10,1392
16	9,771987	9,906482	9,865505	10,1393
17	9,772159	9,906389	9,865770	10,1394
18	9,772331	9,906296	9,866035	10,1395
19	9,772503	9,906203	9,866300	10,1396
20	9,772675	9,906111	9,866564	10,1397
21	9,772847	9,906018	9,866829	10,1398
22	9,773018	9,905925	9,867094	10,1399
23	9,773190	9,905832	9,867358	10,1400
24	9,773361	9,905738	9,867623	10,1401
25	9,773533	9,905645	9,867887	10,1402
26	9,773704	9,905552	9,868152	10,1403
27	9,773875	9,905459	9,868416	10,1404
28	9,774046	9,905365	9,868680	10,1405
29	9,774217	9,905272	9,868945	10,1406
30	9,774388	9,905179	9,869209	10,1407
Co-sine Sine Co-tang. Tan				

Degree 53.

Degree 36.

Sine	Co-sine	Tangent	Co-tang.
74388	9,905179	9,869209	10,13079130
74558	9,905085	9,869773	10,13052729
74729	9,904992	9,869337	10,13026328
74899	9,904898	9,870001	10,12999927
75070	9,904804	9,870265	10,12973526
75240	9,904711	9,870529	10,12947125
75410	9,904617	9,870793	10,12920724
75580	9,904523	9,871057	10,12894323
75750	9,904429	9,871321	10,12867922
75920	9,904335	9,871585	10,12841521
76090	9,904241	9,871849	10,12815120
76259	9,904147	9,872112	10,12788819
76429	9,904053	9,872376	10,12762418
76598	9,903959	9,872640	10,12736017
76768	9,903864	9,872903	10,12709716
76937	9,903770	9,873167	10,12683315
77106	9,903676	9,873430	10,12657014
77275	9,903581	9,873694	10,12630613
77444	9,903486	9,873957	10,12604312
77613	9,903392	9,874220	10,12578011
77781	9,903298	9,874484	10,12551610
77950	9,903203	9,874747	10,1252539
78119	9,903108	9,875010	10,1249908
78287	9,903013	9,875273	10,1247277
78455	9,902919	9,875536	10,1244646
78623	9,902824	9,875799	10,1242015
78792	9,902729	9,876063	10,1239374
78960	9,902634	9,876326	10,1236743
79129	9,902539	9,876589	10,1234112
79295	9,902444	9,876851	10,1231491
79463	9,902349	9,877114	10,1228850

Tan. Sine | Sine | Co-tang. | Tangent M

Degree 53.

Degree 37.

M	Sine	Co-sine.	Tangent	Co-tang.
	9,779463	9,902349	9,877114	10,1221
1	9,779631	9,902253	9,877377	10,1220
2	9,779798	9,902158	9,877640	10,1219
3	9,779965	9,902063	9,877903	10,1218
4	9,780133	9,901967	9,878165	10,1217
5	9,780300	9,901872	9,878428	10,1216
6	9,780467	9,901776	9,878691	10,1215
7	9,780634	9,901681	9,878953	10,1214
8	9,780801	9,901585	9,879216	10,1213
9	9,780968	9,901488	9,879478	10,1212
10	9,781134	9,901391	9,879741	10,1211
11	9,781301	9,901298	9,880003	10,1199
12	9,781467	9,901202	9,880265	10,1197
13	9,781634	9,901106	9,880528	10,1196
14	9,781800	9,901010	9,880790	10,1195
15	9,781966	9,900914	9,881052	10,1184
16	9,782132	9,900818	9,881314	10,1183
17	9,782298	9,900722	9,881576	10,1182
18	9,782464	9,900626	9,881839	10,1181
19	9,782630	9,900529	9,882101	10,1179
20	9,782796	9,900433	9,882363	10,1178
21	9,782961	9,900337	9,882625	10,1177
22	9,783127	9,900240	9,882886	10,1176
23	9,783292	9,900144	9,883148	10,1175
24	9,783457	9,900047	9,883410	10,1174
25	9,783623	9,899951	9,883672	10,1173
26	9,783788	9,899854	9,883934	10,1172
27	9,783953	9,899757	9,884195	10,1171
28	9,784118	9,899660	9,884457	10,1170
29	9,784282	9,899563	9,884719	10,1169
30	9,784447	9,899467	9,884980	10,1168
	Co-sine	Sine	Co-tang.	Tan

Degree 52.

Degree 37.

Co-fine	Tangent	Co-tang.
479.899267	9.884980	10.115020 30
109.899370	9.885242	10.114758 29
769.899273	9.885503	10.114497 28
419.899175	9.885765	10.114235 27
059.899078	9.886029	10.113974 26
699.898981	9.886288	10.113712 25
339.898884	9.886549	10.113451 24
919.898784	9.886810	10.113190 23
619.898689	9.887072	10.112928 22
259.898592	9.887333	10.112667 21
889.898494	9.887594	10.112406 20
529.898397	9.887855	10.112145 19
169.898299	9.888116	10.111884 18
799.898201	9.888377	10.111623 17
429.898104	9.888638	10.111362 16
099.898006	9.888899	10.111101 15
199.897908	9.889160	10.110840 14
329.897810	9.889421	10.110579 13
959.897712	9.889682	10.110318 12
579.897614	9.889943	10.110057 11
209.897519	9.880204	10.109796 10
839.897418	9.890965	10.109535 9
459.897320	9.890725	10.109275 8
089.897222	9.890986	10.109014 7
709.897123	9.891247	10.108753 6
329.897025	9.891507	10.108493 5
949.896926	9.891768	10.108232 4
569.896828	9.892028	10.107972 3
189.896729	9.892289	10.107711 2
809.896631	9.892549	10.107451 1
429.896532	9.892810	10.107190 0
Sine	Co-tang.	Tangent

Degree 52.

B b

Degree 38.

M	Sine	Co-sine	Tangent	Co-tang
0	9.789342	9.896532	9.892810	10.1071
1	9.789504	9.896433	9.893070	10.1069
2	9.789665	9.896335	9.893330	10.1067
3	9.789827	9.896236	9.893591	10.1065
4	9.789988	9.896137	9.893851	10.1063
5	9.790149	9.896038	9.894111	10.1061
6	9.790310	9.895939	9.894371	10.1059
7	9.790471	9.895840	9.894632	10.1057
8	9.790632	9.895741	9.894892	10.1055
9	9.790793	9.895641	9.895152	10.1053
10	9.790954	9.895542	9.895412	10.1051
11	9.791115	9.895443	9.895672	10.1049
12	9.791275	9.895343	9.895932	10.1047
13	9.791436	9.895244	9.896192	10.1045
14	9.791596	9.895144	9.896452	10.1043
15	9.791756	9.895045	9.896712	10.1041
16	9.791917	9.894945	9.896971	10.1039
17	9.792077	9.894846	9.897231	10.1037
18	9.792237	9.894746	9.897491	10.1035
19	9.792397	9.894646	9.897751	10.1033
20	9.792557	9.894546	9.898010	10.1031
21	9.792716	9.894446	9.898270	10.1029
22	9.792876	9.894346	9.898530	10.1027
23	9.793035	9.894245	9.898789	10.1025
24	9.793195	9.894145	9.899049	10.1023
25	9.793354	9.894046	9.899308	10.1021
26	9.793513	9.893946	9.899568	10.1019
27	9.793673	9.893845	9.899827	10.1017
28	9.793832	9.893745	9.900086	10.1015
29	9.793991	9.893645	9.900346	10.1013
30	9.794149	9.893544	9.900605	10.1011

| Co-sine | Sine | | Co-tang. | Tang. |

Degree 51.

Degree 38.

ne	Co-sine	Tangent	Co-tang.
149	9.893444	9.900605	10.099395
1308	9.893444	9.900864	10.099135
1467	9.893343	9.901124	10.098876
1626	9.893243	9.901383	10.098617
1784	9.893142	9.901642	10.098358
1942	9.893041	9.901991	10.098099
2101	9.892940	9.902160	10.097839
2259	9.892839	9.902419	10.097580
2417	9.892738	9.902678	10.097321
2575	9.892637	9.902937	10.097062
2733	9.892536	9.903196	10.096803
2891	9.892435	9.903455	10.096544
3049	9.892334	9.903714	10.096285
3206	9.892233	9.903973	10.096027
3364	9.892132	9.904232	10.095768
3521	9.892030	9.904491	10.095509
3678	9.891928	9.904750	10.095250
3836	9.891827	9.905008	10.094991
3993	9.891726	9.905267	10.094733
4150	9.891624	9.905526	10.094474
4307	9.891522	9.905784	10.094215
4467	9.891421	9.906043	10.093957
4621	9.891319	9.906302	10.093698
4777	9.891217	9.906510	10.093440
4934	9.891115	9.906819	10.093181
5091	9.891013	9.907077	10.092923
5247	9.890911	9.907336	10.092664
5403	9.890809	9.907594	10.092406
5560	9.890707	9.907852	10.092147
5716	9.890605	9.908111	10.091889
5872	9.890503	9.908369	10.091631

Sine Co-tang. Tangent

Degree 51.

B b 2

Degree 39.

M	Sine	Co-sine	Tangent	Co-tang
	09.798872	9.890503	19.908369	10.091631
1	9.799028	9.890400	9.908627	10.091373
2	9.799184	9.890298	9.908886	10.091114
3	9.799336	9.890195	9.909144	10.090856
4	9.799495	9.890093	9.909402	10.090597
5	9.799651	9.889990	9.909660	10.090339
6	9.799806	9.889888	9.909918	10.090081
7	9.799961	9.889785	9.910176	10.089823
8	9.800117	9.889682	9.910435	10.089565
9	9.800272	9.889579	9.910693	10.089307
10	9.800427	9.889476	9.910951	10.089049
11	9.800582	9.889374	9.911209	10.088791
12	9.800737	9.889271	9.911467	10.088533
13	9.800892	9.889167	9.911724	10.088275
14	9.801047	9.889064	9.911982	10.088017
15	9.801201	9.888961	9.912240	10.087759
16	9.801356	9.888858	9.912498	10.087501
17	9.801510	9.888755	9.912756	10.087243
18	9.801665	9.888651	9.913014	10.086985
19	9.801818	9.888548	9.913271	10.086727
20	9.801973	9.888444	9.913529	10.086469
21	9.802127	9.888341	9.913787	10.086211
22	9.802282	9.888237	9.914044	10.085953
23	9.802435	9.888133	9.914302	10.085695
24	9.802589	9.888030	9.914560	10.085437
25	9.802743	9.887926	9.914817	10.085179
26	9.802897	9.887822	9.915075	10.084921
27	9.803050	9.887718	9.915332	10.084663
28	9.803204	9.887614	9.915590	10.084405
29	9.803357	9.887510	9.915847	10.084147
30	9.803510	9.887406	9.916104	10.083889
Co-sine		Sine	Co-tang	Tang

Degrée 50.

Degree 39.

Sine	Co-sine	Tangent	Co-tang.
803510	9.887406	9.916104	10.083895
803664	9.887302	9.916362	10.083638
803817	9.887198	9.916619	10.083381
803970	9.887093	9.916876	10.083123
804123	9.887009	9.917134	10.082866
804276	9.886884	9.917391	10.082609
804428	9.886780	9.917648	10.082352
804581	9.886675	9.917905	10.082094
804734	9.886561	9.918162	10.081837
804886	9.886456	9.918420	10.081580
805038	9.886361	9.918677	10.081323
805191	9.886257	9.918934	10.081066
805343	9.886152	9.919191	10.080809
805495	9.886047	9.919448	10.080552
805647	9.885942	9.919705	10.080295
805799	9.885837	9.919962	10.080038
805951	9.885732	9.920219	10.079781
806103	9.885627	9.920476	10.079524
806254	9.885521	9.920733	10.079267
806406	9.885416	9.920990	10.079010
806557	9.885311	9.921247	10.078753
806709	9.885205	9.921503	10.078496
806860	9.885100	9.921760	10.078240
807011	9.884994	9.922017	10.077983
807162	9.884889	9.922274	10.077726
807314	9.884783	9.922530	10.077469
807464	9.884677	9.922787	10.077213
807615	9.884572	9.923044	10.076956
807766	9.884466	9.923300	10.076699
807917	9.884360	9.923557	10.076443
808067	9.884254	9.923813	10.076186
Sine	Co-sine	Tangent	Co-tang.

Degree 50.

Degree 40.

M	Sine	Co-sine	Tangent	Co-tang
0	9,808067	9,884254	9,923813	10,076187
1	9,808218	9,884188	9,924070	10,075930
2	9,808368	9,884049	9,924327	10,075673
3	9,808519	9,883936	9,924583	10,075416
4	9,808669	9,883829	9,924839	10,075159
5	9,808819	9,883723	9,925096	10,074902
6	9,808969	9,883617	9,925352	10,074645
7	9,809119	9,883510	9,925609	10,074388
8	9,809269	9,883404	9,925865	10,074131
9	9,809419	9,883297	9,926121	10,073874
10	9,809569	9,883191	9,926378	10,073617
11	9,809718	9,883084	9,926634	10,073360
12	9,809868	9,882977	9,926890	10,073103
13	9,810017	9,882871	9,927147	10,072846
14	9,810166	9,882764	9,927403	10,072589
15	9,810316	9,882659	9,927659	10,072332
16	9,810465	9,882550	9,927915	10,072075
17	9,810614	9,882443	9,928171	10,071818
18	9,810763	9,882336	9,928427	10,071561
19	9,810912	9,882228	9,928683	10,071304
20	9,811061	9,882121	9,928940	10,071047
21	9,811210	9,882014	9,929196	10,070790
22	9,811358	9,881907	9,929452	10,070533
23	9,811506	9,881799	9,929708	10,070276
24	9,811655	9,881692	9,929964	10,070019
25	9,811804	9,881584	9,930219	10,069762
26	9,811952	9,881477	9,930475	10,069505
27	9,812100	9,881369	9,930731	10,069248
28	9,812248	9,881261	9,930987	10,068991
29	9,812396	9,881153	9,931243	10,068734
30	9,812544	9,881045	9,931499	10,068477
Co-sine		Sine	Co-tang	Tang

Degree 49.

Degree 40.

Sine	Co-sine	Tangent	Co-tang.
9,881045	10,931499	10,068501	30
9,880937	9,931755	10,068245	19
9,880829	9,932010	10,067989	18
9,880721	9,932266	10,067734	27
9,880613	9,932522	10,067478	16
9,880505	9,932778	10,067222	25
9,880397	9,933033	10,066967	14
9,880289	9,933289	10,066711	23
9,880180	9,933545	10,066455	22
9,880072	9,933800	10,066200	21
9,879963	9,934056	10,065944	20
9,879855	9,934311	10,065688	19
9,879746	9,934567	10,065433	18
9,879637	9,934822	10,065177	17
9,879529	9,935078	10,064922	16
9,879420	9,935333	10,064666	15
9,879311	9,935589	10,064411	14
9,879202	9,935844	10,064156	13
9,879093	9,936100	10,063900	12
9,878984	9,936355	10,063645	11
9,878875	9,936610	10,063389	10
9,878766	9,936866	10,063134	9
9,878656	9,937121	10,062879	8
9,878547	9,937376	10,062623	7
9,878438	9,937632	10,062368	6
9,878328	9,937887	10,062113	5
9,878219	9,938142	10,061858	4
9,878109	9,938397	10,061602	3
9,877999	9,938653	10,061347	2
9,877890	9,938908	10,061092	1
9,877780	9,939163	10,060837	C

Sine | Co-sine | Tangent | Co-tang.

Degree 49.

Degree 41.

M	Sine	Co-sine.	Tangent	Co-tang.
0	9,816943	9,877780	9,939163	10,060837
1	9,817088	9,877670	9,939418	10,060582
2	9,817233	9,877560	9,939673	10,060327
3	9,817378	9,877450	9,939928	10,060072
4	9,817523	9,877340	9,940183	10,059817
5	9,817668	9,877230	9,940438	10,059562
6	9,817813	9,877120	9,940693	10,059307
7	9,817958	9,877009	9,940948	10,059052
8	9,818103	9,876899	9,941203	10,058797
9	9,818247	9,876789	9,941458	10,058542
10	9,818392	9,876678	9,941713	10,058287
11	9,818536	9,876568	9,941968	10,058032
12	9,818681	9,876457	9,942223	10,057777
13	9,818825	9,876347	9,942478	10,057522
14	9,818969	9,876236	9,942733	10,057267
15	9,818113	9,876125	9,942988	10,057012
16	9,819257	9,876014	9,943243	10,056757
17	9,819401	9,875904	9,943498	10,056502
18	9,819545	9,875793	9,943753	10,056247
19	9,819689	9,875682	9,944008	10,055992
20	9,819833	9,875571	9,944263	10,055737
21	9,819976	9,875459	9,944518	10,055482
22	9,820119	9,875348	9,944773	10,055227
23	9,820263	9,875237	9,945028	10,054972
24	9,820406	9,875125	9,945283	10,054717
25	9,820549	9,875014	9,945538	10,054462
26	9,820693	9,874903	9,945793	10,054207
27	9,820836	9,874791	9,946048	10,053952
28	9,820979	9,874679	9,946303	10,053697
29	9,821122	9,874568	9,946558	10,053442
30	9,821264	9,874456	9,946813	10,053187

| Co-sine | Sine | | Co-tang. | Tan

Degree 48.

Degree 47.

Sine	Co-sine	Tangent	Co-tang.
9.874456	10.053192	9.945808	10.053192
9.874444	10.053208	9.947063	10.053208
9.874432	10.053224	9.947317	10.053224
9.874420	10.053240	9.947572	10.053240
9.874408	10.053256	9.947826	10.053256
9.874396	10.053272	9.948081	10.053272
9.874384	10.053288	9.948335	10.053288
9.874372	10.053304	9.948590	10.053304
9.874360	10.053320	9.948844	10.053320
9.874347	10.053336	9.949099	10.053336
9.874335	10.053352	9.949353	10.053352
9.874323	10.053368	9.949607	10.053368
9.874310	10.053384	9.949862	10.053384
9.874298	10.053400	9.950116	10.053400
9.874285	10.053416	9.950370	10.053416
9.874272	10.053432	9.950625	10.053432
9.874259	10.053448	9.950879	10.053448
9.874246	10.053464	9.951133	10.053464
9.874234	10.053480	9.951388	10.053480
9.874221	10.053496	9.951642	10.053496
9.874208	10.053512	9.951896	10.053512
9.874194	10.053528	9.952150	10.053528
9.874181	10.053544	9.952404	10.053544
9.874168	10.053560	9.952659	10.053560
9.874155	10.053576	9.952913	10.053576
9.874141	10.053592	9.953167	10.053592
9.874128	10.053608	9.953421	10.053608
9.874114	10.053624	9.953675	10.053624
9.874101	10.053640	9.953929	10.053640
9.874087	10.053656	9.954183	10.053656
9.874073	10.053672	9.954437	10.053672

Sine | Co-sine | Tangent. M

Degree 48.

C c

Degree 42.

M	Sine	Co-sine	Tangent	Co-tang
0	9.825511	9.871073	19.954437	10.045563
1	9.825651	9.870960	9.954591	10.045409
2	9.825791	9.870846	9.954745	10.045255
3	9.825931	9.870732	9.954899	10.045101
4	9.826071	9.870618	9.955053	10.044947
5	9.826211	9.870504	9.955207	10.044793
6	9.826351	9.870390	9.955361	10.044639
7	9.826491	9.870271	9.955515	10.044485
8	9.826631	9.870161	9.955669	10.044331
9	9.826770	9.870047	9.955823	10.044177
10	9.826910	9.869933	9.955977	10.044023
11	9.827049	9.869818	9.956131	10.043869
12	9.827189	9.869704	9.956285	10.043715
13	9.827328	9.869589	9.956439	10.043561
14	9.827467	9.869474	9.956593	10.043407
15	9.827606	9.869360	9.956747	10.043253
16	9.827745	9.869245	9.956901	10.043099
17	9.827884	9.869130	9.957055	10.042945
18	9.828023	9.869015	9.957209	10.042791
19	9.828162	9.868900	9.957363	10.042637
20	9.828301	9.868785	9.957517	10.042483
21	9.828439	9.868670	9.957671	10.042329
22	9.828578	9.868555	9.957825	10.042175
23	9.828716	9.868439	9.957979	10.042021
24	9.828855	9.868324	9.958133	10.041867
25	9.828993	9.868209	9.958287	10.041713
26	9.829131	9.868093	9.958441	10.041559
27	9.829269	9.867978	9.958595	10.041405
28	9.829407	9.867862	9.958749	10.041251
29	9.829545	9.867747	9.958903	10.041097
30	9.829683	9.867631	9.959057	10.040943
Co-sine Sine Co-tang. Tang.				

Degree 47.

Degree 42.

Co-fine	Tangent	Co-fang.
9.867631	19.962052	10.037947
9.867515	9.962306	10.037694
9.867399	9.962560	10.037440
9.867283	9.962813	10.037187
9.867167	9.963067	10.036933
9.867051	9.963320	10.036680
9.866935	9.963574	10.036426
9.866819	9.963827	10.036173
9.866703	9.964081	10.035919
9.866586	9.964335	10.035665
9.866470	9.964588	10.035412
9.866353	9.964842	10.035158
9.866237	9.965098	10.034905
9.866120	9.965348	10.034652
9.866004	9.965602	10.034398
9.865887	9.965855	10.034144
9.865770	9.966109	10.033891
9.865653	9.966362	10.033638
9.865536	9.966616	10.033384
9.865419	9.966869	10.033131
9.865302	9.967122	10.032878
9.865185	9.967376	10.032624
9.865068	9.967629	10.032371
9.864950	9.967883	10.032117
9.864833	9.968136	10.031864
9.864716	9.968389	10.031611
9.864598	9.968643	10.031357
9.864480	9.968895	10.031104
9.864363	9.969146	10.030851
9.864245	9.969403	10.030597
9.864127	9.969656	10.030344

Sine | Co-fang. | Tangent | M

Degree 47.

Degree 42.

M	Sine	Co-sine	Tangent	Co-tang
0	9.833783	9.864127	9.969636	10.030364
1	9.833912	9.864010	9.969909	10.030091
2	9.834034	9.863892	9.970162	10.029838
3	9.834182	9.863774	9.970416	10.029584
4	9.834324	9.863656	9.970669	10.029331
5	9.834460	9.863537	9.970923	10.029077
6	9.834595	9.863419	9.971178	10.028823
7	9.834730	9.863301	9.971432	10.028569
8	9.834865	9.863183	9.971687	10.028315
9	9.834999	9.863064	9.971943	10.028061
10	9.835134	9.862946	9.972198	10.027807
11	9.835269	9.862827	9.972454	10.027553
12	9.835393	9.862709	9.972709	10.027299
13	9.835538	9.862590	9.972965	10.027045
14	9.835672	9.862471	9.973221	10.026791
15	9.835806	9.862353	9.973477	10.026537
16	9.835941	9.862234	9.973733	10.026283
17	9.836075	9.862115	9.973989	10.026029
18	9.836209	9.861996	9.974245	10.025775
19	9.836343	9.861877	9.974501	10.025521
20	9.836477	9.861757	9.974757	10.025267
21	9.836611	9.861638	9.974973	10.025013
22	9.836745	9.861519	9.975229	10.024759
23	9.836878	9.861399	9.975485	10.024505
24	9.837012	9.861280	9.975741	10.024251
25	9.837146	9.861161	9.975997	10.023997
26	9.837279	9.861041	9.976253	10.023743
27	9.837412	9.860921	9.976509	10.023489
28	9.837546	9.860802	9.976765	10.023235
29	9.837679	9.860682	9.976997	10.022981
30	9.837812	9.860562	9.977253	10.022727
Co-sine Sine Co-tang Tangent				

Degree 46.

Degree 43.

Sine	Co-sine	Tangent	Co-tang.
878129.860662		19.97728010.022750130	
879459.860448		9.97740210.02249729	
880789.860322		9.97775610.02224228	
882119.860202		9.97800910.02199127	
883449.860082		9.97826210.02173826	
884779.859962		9.97851510.02148525	
886099.859842		9.97876810.02123224	
887429.859721		9.97902110.02097923	
888759.859601		9.97927410.02072622	
890059.859480		9.97952710.02047321	
891409.859360		9.97978010.02022020	
892729.859239		9.98003310.01996719	
894059.859118		9.98028510.01971418	
895389.858998		9.98053810.01946117	
896689.858877		9.98079110.01920816	
898009.858756		9.98104410.01895515	
899329.858635		9.98129710.01870214	
900649.858514		9.98155010.01844913	
901969.858392		9.98180310.01819712	
903289.858272		9.98205610.01794411	
904599.858150		9.98230910.01769110	
905919.858029		9.98256210.0174389	
907219.857908		9.98281410.0171858	
908549.857786		9.98306710.0169327	
909859.857665		9.98332010.0166806	
911169.857543		9.98357310.0164275	
912479.857421		9.98382610.0161744	
913789.857300		9.98407910.0159213	
915099.857178		9.98433110.0156682	
916409.857056		9.98458410.0154151	
917719.856934		9.98483710.0151620	

Sine | Co-sine | Tangent | M

Degree 46.

Degree 44.

M. Sine		Co-sine	Tangent	Co-tang
0		9,841771	9,856934	10,984817
1	9,841901	9,856811	9,985060	10,01401
2	9,842033	9,856690	9,985143	10,01415
3	9,842163	9,856568	9,985226	10,01429
4	9,842294	9,856445	9,985308	10,01443
5	9,842424	9,856323	9,985391	10,01457
6	9,842555	9,856201	9,985474	10,01471
7	9,842685	9,856078	9,985557	10,01485
8	9,842815	9,855956	9,985640	10,01499
9	9,842945	9,855833	9,985723	10,01513
10	9,843076	9,855710	9,985806	10,01527
11	9,843206	9,855588	9,985889	10,01541
12	9,843336	9,855465	9,985972	10,01555
13	9,843465	9,855342	9,986055	10,01569
14	9,843595	9,855218	9,986138	10,01583
15	9,843725	9,855096	9,986221	10,01597
16	9,843855	9,854973	9,986304	10,01611
17	9,843984	9,854850	9,986387	10,01625
18	9,844114	9,854727	9,986470	10,01639
19	9,844243	9,854603	9,986553	10,01653
20	9,844372	9,854480	9,986636	10,01667
21	9,844502	9,854356	9,986719	10,01681
22	9,844631	9,854233	9,986802	10,01695
23	9,844760	9,854109	9,986885	10,01709
24	9,844889	9,853986	9,986968	10,01723
25	9,845018	9,853862	9,987051	10,01737
26	9,845147	9,853738	9,987134	10,01751
27	9,845276	9,853614	9,987217	10,01765
28	9,845404	9,853490	9,987300	10,01779
29	9,845533	9,853366	9,987383	10,01793
30	9,845662	9,853242	9,987466	10,01807
Co-sine		Sine	Co-tang.	Tang.

Degree 45.

Degree 44.

Sine	Co-sine.	Tangent	Co-tang.
9,56619,8332421		9,991420	10,007580130
9,57099,853118		9,991673	10,007328129
9,57519,8532994		9,991923	10,007075128
9,58047,8531869		9,993178	10,006822127
9,58175,8532745		9,993430	10,006569126
9,58304,8532620		9,993683	10,006317125
9,58433,843496		9,993936	10,006064124
9,58560,8532371		9,994189	10,005811123
9,58688,8532240		9,994441	10,005559122
9,58816,8532122		9,994694	10,005306121
9,58944,8531997		9,994947	10,005053120
9,59071,8531872		9,995199	10,004801119
9,59199,8531747		9,995452	10,004548118
9,59327,8531622		9,995701	10,004295117
9,59454,8531497		9,995957	10,004043116
9,59582,8531372		9,996210	10,003790115
9,59709,8531246		9,996463	10,003537114
9,59836,8531121		9,996715	10,003285113
9,59964,8530996		9,996968	10,003032112
9,60091,8530870		9,997220	10,002779111
9,60218,8530745		9,997473	10,002527110
9,60345,8530619		9,997726	10,002274109
9,60472,8530493		9,997979	10,002021108
9,60599,8530367		9,998231	10,001769107
9,60726,8530242		9,998484	10,001516106
9,60852,8530116		9,998737	10,001263105
9,60979,8499990		9,998989	10,001011104
9,61106,849864		9,999242	10,001758103
9,61232,849737		9,999495	10,000505102
9,61359,849611		9,999747	10,000253101
9,61485,849485		10,000000	10,000000100

Sine | Co-sine. | Tangent | Co-tang. | M

Degree 45.

1.22

1742

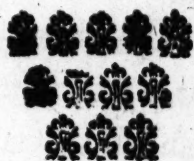
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THE
Young Gentleman's
MECHANICKS:

CONTAINING

the more Useful and Easy
ELEMENTS of *Mechanicks*,
more properly so called, of *Sta-*
ticks, and *Hydrostaticks*.

EDWARD WELLS, D. D.
Rector of *Cotesbach* in *Leicester-*
shire.



L O N D O N,
Printed for *James Knapton*, at the *Crown*
St. Paul's Church-Yard. 1713.

THE

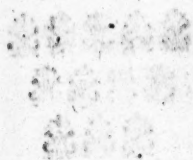
Young Gentlemen's

MECHANICS

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tionary and hydraulic.

EDWARD WELLS, D.D.
Professor of Divinity in King's



LONDON:
Printed by James Knapton, at the Green
in St. Paul's Church-Yard, 1713.

THE
PREFACE.

Nothing more needs be said, to
shew the great Usefulness of
the Science, denoted by the
Name of Mechanicks, than
teaches, and explains in a
rational Manner, those Principles,
on which is founded the Power or
Use of the several Machines or En-
gines made use of either in Civil or
Military Affairs; and also that it ex-
plains in like manner the various Mo-
tions of heavy Bodies, consider'd either
in the Air or in the Water. The bare
Use of Machines is indeed an illi-
beral servile Employ, and fit only
for the hands of the meaner Sort; whence
many-craft Persons are some-
times called, by way of Degradation,

The Preface.

Mechanicks. But the Knowledge of the Principles, whereon depend mechanical Arts or Trade, is justly esteem'd a Liberal Science, not below the Study of Persons of the highest Ability and Rank. Forasmuch as this Science both gives a very considerable sight into the Works of Nature; not only with respect to Sublunary Bodies, but even to the Frame, Order, and Preservation of the Celestial System, and also may be infinitely serviceable to the Concerns of Humane Life, by the Invention of new Machines and Instruments: especially if it be cultivated by Persons, who have both the Ability of Parts to invent, and the Facility of Pocket actually to execute their Inventions, and by this means to compleat and perfect them. It is to be fear'd, that many an Invention has unfortunately miscarried, because the Inventer has not a good Purse, as well as a good

THE
Young Gentleman's
MECHANICKS.

CHAP. I.

in are explain'd such Terms as
ate to *Mechanicks* in general.

THAT Art or Science, which
teaches how to move any
given Weight, by any gi-
ven Power, we call in one
(†) *Mechanicks*; because it is
serviceable to the contriving of
Machines or Engines, which are us'd

Mechanicks,
what, and
why so cal-
led.

The Word *Mechanicks* is deriv'd from the Greek
μηχανη; from which is made likewise the corré-
Latin Word *Machina*; and from this is form'd
the Word *Machine*. From the same original Greek
deriv'd also the Word *Mechanism*, i. e. the Arti-
trivance of a Thing.

(A 3)

in

in the Concerns of Life, whether
or Military.

2. By a *Weight* is understood in
*A Weight, and a Pow-
er, and Mo-
tion, what
in Mecha-
nicks.* nicks any heavy Body; by a *Power*
whatever can move an heavy
and by *Motion*, Local Motion or
Change of Place.

3. The *Axis of Motion* is that right
*The Axis
and Center
of Motion,
what.* round which a Body being mov'd,
Point of the Body describes
whose Centers are all in the said
Line; and the Mid-point of the
called *the Center of Motion*. Thus
the Sphere or Bowl *A D B E*, being com-
to move round the right Line *A B*
said *A B* will be the Axis, and the
the Center of its Motion.

4. That right Line, wherein any
*The Direc-
tion of Mo-
tion, what.* Power endeavours to move, is call'd
Line of Direction, or simply, the
on of the Motion of the respective
or Power. And if a Body move
Curve Line, then the Direction of
tion in each Point of the Curve
Tangent of the said Point. Thus
A B is the Direction of the *Weight*
and *B C* the Direction of the *Power*

(*) Hence any Weight or heavy Body is or
steem'd a Power, in reference to any other Wei-
vy Body, which it do's or can move.

Mechanicks.

2

Fig. 3. the Tangents TA, TB, TC, respectively the several Directions of mov'd round the Curve ABC, at several Points A, B, and C.

Force, which is in Bodies mov'd, whereby they continually move, or your to move, is call'd their *Momentum*, and arises from the Weight of Quantity of Matter in the Body, and the Velocity or Swiftness with it moves.

5.
The Momentum of a Body, what.

The different Weight of Bodies arises from the different Quantity of Matter in Bodies. Whence the Quantity of Matter in any Body may be estimated by its Weight. For instance, if a cubical Inch of Lead be six times heavier than a cubical Inch of Wood, it may thence be infer'd, that the Quantity of Matter in a Piece of Lead is six times as much as the Quantity of Matter in a like Piece of Wood.

6.
The Weight of Bodies is proportional to their Matter.

Specific Gravity, which arises from the more or less Compactness of Bodies naturally belonging to the several Sorts of Bodies, is called their *Specific Gravity*. Thus, although a Pound of Feathers be equal in Weight to a Pound of Lead, yet Lead is said to be *specifically* heavier than Feathers, because there is not so much Matter, nor consequently so much Weight, in a Feather,

7.
Specific Gravity, what.

(A 4)

ther,

ther, as in a Piece of Lead of the Bulk with the Feather.

8.

Centrum
Gravium,
what.

Gravity or Weight being that, causes in Bodies a Tendency to move not hinder'd by some external Force downwards, or towards the Center of the Earth; hence the Center of the Earth is call'd *Centrum Gravium*, or the Center to which heavy Bodies tend.

9.

The Center
of Gravity,
what.

The *Center of Gravity* in any Body is that Point, through which a Plane being drawn divides the Body into two Segments or Parts of equal Weight. It is this Point the *Center of Gravity*, which is of chief Use in Bodies, a Body being not properly said to descend or ascend, but only when its *Center of Gravity* descends or ascends.

10.

Velocity,
what.

Velocity (which is the other Element, that together with Weight makes the Momentum of a Body) is that Quantity of Motion, which is measured by comparing together the Length and Time of Motion. Thus *Equal Velocity* is that whereby equal Length is pass'd over in equal Time: *Greater Velocity* is that whereby either a greater Length is pass'd over in equal Time, or an equal Length in less Time: *Less Velocity*, where the contrary is true. Further, a Body that pass'd an hundred Yards, may be said to move with *double* the Velocity of a Body

but fifty Yards in the same Time ;
with *triple* or thrice the Velocity of
her Body, that moves but thirty-
Yards and one third in the same
; and with *quadruple* or four-
the Velocity of a Body that moves
twenty-five Yards in the same Time.
So on.

The Momentum of a Body, arising (as
seen observ'd §. 5,) from its Weight
Velocity, may be known by multi-
g one of its Ingredients into the o-
And consequently the different Mo-
ments of different Bodies may be
n by multiplying the Weight of
Body into its respective Velocity.
Suppose the Weight of a Body A to
be four Pound ; and the Velocity of
be five-times as much as that of A.
Momentum of A will be 10 ; viz.
ound, the Weight of A, being mul-
into 1 for its Velocity, (the Velo-
f A to B being suppos'd as 1 to 5,)
product will be 10 for the Momen-
A. And in like manner, 4 Pound,
eight of B, being multiply'd into 5
Velocity of B, (for the Velocity of
is suppos'd as 5 to 1) the Product
e 20 for the Momentum of B.
it appears that the Momentum of
B is

II.
*The Mo-
mentum of
a Body,
how to be
known.*

12.

The Fundamental
Theorem
of Mechanicks.

B is double to that of A, being as 20

Hence is deduced the following
rem, which may be stiled the Funda-
tal Theorem of Mechanicks, *viz.*
*Bodies have their Velocities reciprocal-
proportional to their Weights, their Mo-
tum's will be equal.* Let the Weight
of a great Body A be 500 Pound,
the Weight of a little Body B be 10
Pound; and let their respective Ve-
locities be reciprocally proportional, (as
the Weight of A is to that of B as 10
so let the Velocity of B be to that of A
10 to 1.) It will hence follow, that the
Momentum of B will be just equal to
that of A. Namely, 500 Weight $\times$ 1
Velocity = 500 the Momentum of A;
10 Weight $\times$ 10 Velocity = 500 the
Momentum of B.

13.

The general End
and Effect
of Mechanical En-
gin's.

Hence it appears, not only that the
little *may have* its Momentum equal to
that of any great Body mov'd with a
given Velocity; but what Method is to be
taken, in order to make it *actually have*
so; namely, by contriving that the Ve-
locity of the Body may be so much greater
than the Weight of the Body to be mov'd,
that the Velocity is greater (or somewhat
equivalent to) of the Power. On which
it is, that the foremention'd Theorem

ly esteem'd the Fundamental The-
of Mechanicks ; forasmuch as there-
founded the principal Mechanism
intrivance of Machin's or mechanical
s, made use of to draw or raise
Bodies ; the whole End and Ef-
these being to give such a Veloci-
the Power, or (which comes to
me) so to diminish the Velocity of
eight or heavy Body, as that the
ntum of the Power may be equal,
ewhat exceed, the Momentum of
dy so to be drawn or rais'd.

this is what will be illustrated in
following Chapters, in reference
fix simple and therefore primary
s, or (as they are otherwise cal-
mechanical Powers ; to some one or
of which may be reduc'd all o-
mechanical Engin's. And I shall
of them in the Order, wherein
re follow (*) reckon'd up, viz.

14.
*The simple
mechanical
Powers, six
in Number.*

I Vectis

reas some reckon but five simple Machines or
Powers, comprehending the Balance under
and others that reckon six simple Machines, u-
the Balance as the first, and the Leaver as the
have judg'd it more proper to agree with the
reckoning six simple or primary Machines, and
so far with the former, as to reckon the Leaver
and the Balance as the second simple Machine,
the Leaver is a more simple Machine than the
Balance ;

1. *Velis* or the *Leaver*.
2. *Libra* or the *Balance*.
3. *Axis in Peritrochio* or the *Wheel*.
4. *Trochlea* or the *Pulley*.
5. *Cochlea* or the *Screw*.
6. *Cuneus* or the *Wedge*.

Balance; and the Balance is no other than a Kind of Leaver. In like manner, whereas some call the Wedge as the fifth, and the Screw as the sixth Machine, I have rather follow'd them, who have the said Order, forasmuch as the Screw partakes the Faculty of the Leaver than the Wedge.

CHAP. II.

Of the Leaver.

I.
A Leaver,
what.

THE *Leaver* is so call'd for the principal Use thereof, which is to *levare*, i. e. to lift or raise up heavy bodies. For the more easy explanation of the Mechanism thereof, it is here call'd as a *Line*, which will not bend, but may be turn'd round about an unmovable Point; which is therefore the *Centre*.

otion, and rests upon somewhat
call'd the *Fulcrum*, i. e. Prop of
eaver. Thus *Fig. 4*, AB is the Lea-
C the Center of its Motion, and F
lcrum or Prop.

2.
Theorem
the first.

The main Doctrine of the Leaver may
be comprised under two Theorems, where-
the first is this: *The Space (or Arch)*
describ'd by each Point of a Leaver, and
proportionally the Velocity of each Point of a
Leaver, is, as its Distance from the Ful-
crum or Prop. For instance, the Leaver
(*Fig. 4.*) being mov'd from ACB to
the Point A will describe the Arch
Aa; and the Point B will describe the
Bb; and by reason of the like
Triangles ACA and BCB, Aa is to Bb as AC
is to BC, that is, the Spaces describ'd by
the Points A and B are as their Distances
from the Center of Motion, or (which
amounts to the same) from F the Fulcrum.
Powers being apply'd to the Points
A and B, which draw the Arms CA and
CB perpendicular to the Leaver AB, the
Spaces describ'd by them will be (not
as the Arms Aa and Bb, but (the Perpen-
diculars AD and EB, these being the
Distances of the Progress made by the
Points according to their respective
Directions. But the Triangles ACD
and BCE being equiangular, therefore
(*) AD

(*) AD is to BE as AC to BC or bC , that is, the Lengths gone over the Powers according to their respective Directions, are as their Distances from C the Center of Motion, or (which comes to the same) from F the Fulcrum. Now Velocity being (according to §. 10) that Affection of Motion which is measur'd by comparing together Length and Time, and consequently (Sort of) greater Velocity being whereby a greater Length is past in equal Time, as in the Case before, hence it follows, that the Velocity of the Point B; or of the Power apply'd thereto, is so much greater than the Velocity of the Point A or the Power apply'd thereto; (as the Arch Bb or Line BE is greater than the Arch AD; and consequently so much greater) as BC or bC is than AC; that is, the Velocity of each Point or Leaver, or of any Power apply'd thereto is as its Distance from (C the Center of Motion, or from) F the Fulcrum.

(*) By Theorem 9, of the Young Gentlemen's Geometry.

(†) For the Sake of such as may not readily see the foregoing Geometrical Demonstration of the former, the same is sensibly demonstrated in Fig. 4, by equally dividing BC, bC , Bb, and BE into six equal Parts of the same Length or Compass as AC, aC , Aa, and respectively.

The Truth of the first Theorem being illustrated and apprehended, it will be easy to apprehend the Truth of the second Theorem, which is this: In a Lever, the Power, which is to the Weight, as the Distance of the Weight (according to its Line of Direction) from the Fulcrum is to the Distance of the Power (according to its Line of Direction) from the Fulcrum, will counterbalance or hold up the Weight; and therefore, if a little increas'd, will raise the Weight.

For it has been shewn under Theorem 1, that the Spaces describ'd by the Powers apply'd to each End of the Lever, i. e. by the Power apply'd to one End and the Weight apply'd to the other, are proportional to their Distances from the Fulcrum; and consequently that their Velocities, being proportional to the said Squares, are also proportional to the said Distances.

Wherefore if (Fig. 5) CA the Distance of the Weight from the Fulcrum, be to CB the Distance of the Power from the Fulcrum, as the Power P is to the Weight W, it will follow, that the Velocity of the Weight

will

Fig. 5, Bb the Line of Direction of the Power from C to Aa, the Line of the Weight's Di-

will be to the Velocity of the Power as the Power is to the Weight. And consequently the Momentum of the Power will (by the Fundamental Theorem 1. §. 12) be equal to the Momentum of that Weight; and therefore the Power will be able to sustain the Weight, if it be but a little increas'd, (either by the Addition of some new Force, or by increasing its Distance from the fulcrum) it will be able to raise a greater Weight.

4.
Theorem
the second
illustrated
by an Ex-
ample.

An Example will illustrate the Theorem. Let W the Weight of the Body rais'd be 120 Pound, and the Force of the given Power P be equivalent to 20 Pound, and consequently the Weight be to the Power as 6 to 1. Where the Power being so plac'd at B (P), and W the Weight at A , as that BC be six times as long as AC , in such a Position the Power will have a Force sufficient to counterpoise, and so hold the Weights. For the Velocity of P to that of W being proportional to their Distances from C , will be in this Case as 6 to 1; and consequently the Momentum of P , viz. 20 Pound $\times$ 6 Velocity = 120 Pound $\times$ 1 Velocity, the Momentum of W . Wherefore the Power P (having a little new Force added to its own) being remov'd a little farther

C, viz. to *b*, and so having its Velocity a little more increas'd, it will raise Weight. For supposing *bC* to be as 7 to 1, the Momentum of *P* will Pound $\times$ 7 Velocity = 140; which is considerably greater than the Momentum of *W* at *A*, this being (as afore-
but 120.

ing thus shewn the Truth of the foregoing Theorems, and these being applicable to the other following mechanical Powers, as well as to other Cases of the Leaver, it may be observed here, that the Import of the second Theorem here laid down will hereafter be express'd in short thus; $CW : CP$, that is, As much Force of the Power *P* is less than Weight *W*, so much less must be the Distance of the Weight from the Fulcrum, than *CP* the Distance of the Power from the Fulcrum.

5.
Theorem the 2d express'd in short by Letters.

As this has been shewn to hold in respect of the Leaver (as it is called) of the first Kind, that is, when the Fulcrum is between the Power and Weight; so does it hold good in respect of the Leaver of the second Kind when the Weight is between the Fulcrum and the Power; and also in the third Kind, when the Power is between the Weight and the Fulcrum.

6.
The Kinds of Leavers.

(B)

crum.

crum. For in a Leaver of the Kind, the Weight W at D (*Fig.* (as is obvious) just the same Effect would have on the other Side of the crum and at the same Distance *viz.* at E . And in like manner the er P at D (*Fig. 7.*) has just the effect, as it would have at E , CE be equal to CD . Wherefore the Le the second and third Kind being effect no other than that of the first Mechanism of these depends on the Theorem or Rule, as the Mechan that, *viz.* $P : W : CW : CP$.

7.
Scissers,
Pinchers,
&c. Kinds
of Leavers.

To the Leaver of the first Kind ferr'd Scissers, Pinchers, Snuffers such-like Instruments, they consist it were of two such Leavers joined together, but acting contrary Ways; be easily apprehended by *Fig. 8*. To the Leaver of the second Kind ferr'd the Oars of a Boat, as a Cutting-Knives as are fix'd at one To the Leaver of the third Kind referr'd a Ladder, lifted up between two Ends, in order to rear it against a Wall. Lastly, an Hammer driving a Nail is referr'd to a fourth Kind call'd a Bended Leaver. For thus as the Weight at one End A , the Hand of him that draws the Nail the Power at the other End B of

and the Point C (Fig. 10) is as the
 m. And this fourth Kind of Lea-
 likewise reducible to the First, the
 or Nail at A having the same Ef-
 if it were at a, Fig. 10.

Weight carried on a Pole or Stick
 on two Persons may also be refert'd
 lever of the second Kind, so it may
 good Use to observe, that agreea-
 the foremention'd Theorem P :
 CW : CP, the Weight may be so
 as that the Burden thereof shall
 portion'd to the different Strengths
 two Persons ; Namely, by taking
 note the Strongest, W the Weak-
 C the Weight. For then the Im-
 the said Theorem will be this :
 as the Strength of the Strongest
 greater than the Strength of the
 W, so much must CW the Di-
 of the Weight from the Weakest,
 ter than CP the Distance of the
 from the Strongest. For Exam-
 ppose the Lever or Stick PW
 to be divided into 18 equal
 and the Person at P to be twice as
 the other at W, then C the Bo-
 e carried must be plac'd at 6. For
 the Distance CW will contain 12 of
 al Parts, into which the Stick is
 and the Distance CP will con-
 6 of them ; and so $CW = 2CP$,

8.

*How to
 place a
 Weight or
 Body on a
 Stick or
 the like; so
 as to make
 the Burden
 proportio-
 nal to the
 different
 Strengths
 of them
 that carry
 the Stick.*

(B 2)

and

and consequently the weakest Person W will sustain but half so much as the strongest at P. In like manner, if the Body c were placed at 3, then the Person P would sustain 5 times so much as the other at W; because then the Proportion of the Distances would be as 5 to 3, cW containing 15 of the Parts, whereof cP would contain 9. Lastly, if the Body c were placed at the Mid-point of the Staff, that is, in the Mid-point of the Staff Pole, then each Person P and W would bear equal Burden, because the Distance $9P =$ Distance $9W$.

9.
The like
explain'd
as to drawing
any
Weight.

And the same Theorem holds in respect of Drawing (as well as Carrying) any Burden. For (Fig. 12) let V represent the Pole of any Waggon or Coach, and AB the Cross-bar, at whose Extremities are Spring-trees DE and to which are to be fasten'd the Horses or the like. Because A and B are equidistant from C , therefore the Horses at A and B will draw equal Weight. When one of the Spring-trees be fasten'd to 1, then the said Horse would draw a fourth Part more of the Weight W , than the other Horse at B ; forasmuch as the Distance $C1$ is a fourth Part less than the Distance CB . And so if one Horse be fasten'd to 2, he would draw twice so much as the other at B ; because

the Half of CB. And so

the Mechanism of the Leaver may account for the Reason, why it is difficult to lift up a Staff (or the Arm) of any Length, at or near one of its Ends, than nearer the Middle: Namely, because the Momentum of any Thing increases proportionably to the Distance from its Fulcrum or Prop. The same is the Reason, why it is difficult to lift up a long Staff or Arm, at Arm's Length, or keeping the Arm from Hand to Shoulder extended, than when we bend the Arm at the Elbow. Namely, because in the former Case the Shoulder is the Fulcrum or Prop, in the latter Case the Elbow is the Fulcrum or Prop, and therefore in the former the Distance of the Weight from the Prop, is greater than in the latter. And so much of the Leaver.

10.
Other Particulars sol'd.

(B 3)

CHAP.

C H A P. III.

Of the Balance.

1.
The Beam
of a Ba-
lance no o-
ther than
a Sort of
Leaver.

THE Beam AB (Fig. 13 and the principal Part of a Balance and is no other than a Leaver of the same Kind, which (instead of resting on a Fulcrum at C the Center of Motion) is held up from above by a Cord what fastened to C its Center of Motion.

2.
The Me-
chanism
of the Ba-
lance ex-
plain'd in
general.

Hence the Mechanism of the Balance depends on the same Theorem as the Leaver, viz. $P : W :: C$. Where, taking P to denote the known Weight, W the unknown Weight, C the Center of the Balance's Motion. The Import of the Theorem is this : as the known Weight is less than the unknown Weight, (i. e. the Weight of the Body weigh'd) so much will the Distance of the unknown Weight from the Center of Motion be less than the Distance of the known Weight from the Center of Motion, where the said two Weights will poise one the other ; and consequently the known Weight shew the Quantity of the unknown Weight.

3.

The Mechanism of the Roman Balance or Steel-yard particularly explain'd.

Instance, on the (*) Roman Balance or Steel-yard, (*Fig. 13*) the unknown Weight or Body to be weigh'd be apply'd to A, and the known Weight mov'd up and down, nearer and (from the Point C) upon the Arm and being found at the Distance 5 interpoise W the unknown Weight, it follows, (*viz.* because the Distance CP is 5 times greater than the Distance CW, or which is the same, CA) the Quantity of the unknown Weight is 5 times as much as the Quantity of the known Weight. And therefore, supposing P to be one Pound Weight, W is five Pound Weight; or supposing P to be two or three Pound Weight, W is respectively ten or fifteen Pound Weight.

Now, because in a common Balance (†) Pair of Scales, (*Fig. 14*) the Arms CA and CB of the Beam AB are brought to be) always of an equal Length; hence the Quantity of the

4.

The Mechanism of the common Balance or of a Pair of Scales, explain'd.

Sort of Balance is call'd the Roman Balance, from which us'd at Rome. And it is commonly call'd a Yard, as being a Sort of Yard made of Steel. The Latins call this *Libra* or Balance by the name of *Balanx* (namely *a binis Lancibus*, i. e. two Scales belonging thereto) whence is made the Word *Balance*.

(B 4)

known

known Weight P in one Scale must self be equal to the Quantity of the known Weight W put in the other. And therefore the Quantity of the known Weight on this Sort of Balance found out, (not as on the Steel-Yard moving *one* and the same Weight or farther from C the Center of Motion but) by putting in *various* Weights known Quantity, 'till the known Weight counterpoises the unknown; and by shews the Quantity of the unknown Weight.

5.
Bare
Weight is
strictly true
Weight.

For it is to be observed, that the known Weight then shews the *true* Quantity of the unknown Weight when the one counterpoises the other. For the usual Custom of making the Weight of the Thing somewhat less than counterpoise the known Weight which it is weigh'd, (even so as to the Scale, wherein the Thing is put, to the Ground or the like) has come from Tradesmen being willing to please Customers, by allowing them somewhat less than strictly true, or (as it is commonly (*) properly enough call'd) *bare* Weight. And consequently, when we

(*) Because hereby is denoted true Weight barely as to Weight, without any respect to

man, who is more free than ordi-
nary what he allows over bare Weight,
he makes good Weight, or better
than another, that makes only
Weight; thereby is to be under-
stood not that the Weight he makes is
truer than the other's, in respect
of intrinsic Quantity; but that it is
better than the other's, in respect
of Advantage accruing to the Buyer,
that is allow'd over bare or true
Weight.

Also not to be omitted, that as one
is said to counterpoise (or to be of
Weight with) another, when they
severally apply'd to the two diffe-
rent Arms of the Balance, the Beam lies
horizontally or equally level; so this
is said in our common Speech (not on-
ly of Weight for the Reason afore as-
signed but also) *standing Weight*, foras-
much as in this Case the Beam stands e-
ven neither Arm ascending or descend-
ing more than the other; and for the
Reason the Bodies in this Case
are by the Learned to be in *Æquili-*

6.
*Standing
Weight, and
to be in Æ-
quillibrio,
what.*

is shewn by the Piece of Iron CE, call'd the
being in a Line or directly between TX and

Lastly,

7.

How to discover a false Balance or Pair of Scales.

Lastly, it is well to be observ'd, the Truth or Exactness of (a Balance or) a Pair of Scales depending on its two Arms being of equal Length, as well as of equal Weight themselves, hence it follows, that if one Arm be longer than the other, it will shew a false Balance, or not shew the Quantity of the unknown Weight (which is the same) the true Weight of the Thing weigh'd. For instance, suppose *Fig. 14*, the Arm AC to be divided into ten equal Parts, and the Arm BC to contain but nine such Parts; and consequently AC to be longer than BC by a tenth Part. It will follow by the Fundamental Theorem (C. §. 12, or which comes to the same in this Theorem, $P : W :: CW : CP$), that a known Weight of nine Pounds apply'd to A, will have its Momentum equal to a Body of ten Pound Weight apply'd to B; for $9 \text{ Pound} \times 10 \text{ Velocity} = 90 \text{ Momentum} = 10 \text{ Pound} \times 9 \text{ Velocity}$, and consequently will counterpoise one the other in such a false Balance, though their Weights be not equal to themselves. The Way to discover false Balances, is by changing the known and unknown Weight into the other Scales. For upon such a Change, the equality of the Weights will manifest itself.

appear ; whereas in a true Balance
 of Scales, such a Change of the
 will make no Difference, there be-
 no Difference in the Length of the
 , and consequently no Difference in
 Velocity of the known or unknown
 ht, to which ever Arm they be ap-

Namely, the Body being of 10 Pound Weight in it
 when apply'd to A, its Velocity being in respect
 Velocity of the known Weight of 9 Pound in it self,
 9, the Momentum of the said Body will be $(10 \times 10 \text{ Velocity}) = 100$; whereas the Momentum of
 own Weight will be $(9 \text{ Pound} \times 9 \text{ Velocity}) = 81$.
 Consequently the known Weight will not counterpoise
 by a great deal put in the Scale of the shorter
 though it did so in the Scale of the longer Arm

C H A P. IV.

Of the Axle in the Wheel.

THIS Machine is so called, as con-
 sisting principally of a Wheel BGHI,
 a Cylinder or Axle ADEF. A-
 which Axle goes the Rope, which
 the Weight W, when the Axle is
 round by means of the Wheel ; as

I.
*This Ma-
 chine, why
 so called.*

A

2.

It is in effect no other than a Leaver, capable of being perpetually turn'd round its Fulcrum.

As the Balance is no other than a Leaver, particularly apply'd to finding the Quantity of an unknown Weight, this mechanical Power is no other than a Leaver, apply'd to the same Use as Leavers are, (*viz.* to the raising of great Weights) with this particular advantage added thereunto: Namely, whereas in the Leaver it self the Motion continu'd only for so short a Space (*Fig. 4 and 5*) as is answerable to a little Distance CA between the Fulcrum and the Weight; in this Invention the Inconvenience is remedy'd, forasmuch as by continual turning round the Weight and so (together with it) the Axle may be rais'd to any Height Occasion shall require.

3.

Its Mechanism explain'd.

As this Machine is no other than a Leaver AB capable of being perpetually turn'd round, so the Fulcrum or Center of its Motion is C, and the Point B is that to which the Power P is apply'd, and A the other End, to which is to be apply'd the Weight W to be rais'd. Hence the Mechanism of this Machine depends on the same Theorem as that of the Leaver, *viz.* $P : W :: CP : AP$; that is with particular reference to this Machine; If as much as the Power P is less in it self than the Weight W, so the Radius of the Axle be less than the

of the Wheel, (and consequent-
much the Circumference of the Axle
than the Circumference of the
; and consequently so much the
velocity of the Weight apply'd to
le be less than the Velocity of the
apply'd to the Wheel) by the Fun-
tal Rule the Momentum of the
will be equal to that of the
, and consequently the Power will
poise and so hold up the Weight;
efore the Power being a little in-
will raise the Weight.

Momentum of the Power thus in-
g according to the Disproportion
in the Circumference of the Wheel,
the Circumference of the Axle;
it follows, that the Line of the
Direction must always touch the
ference of the Wheel, so as to
(*)right Angle with the Ray, that
same Distance between the Pow-
the Center of Motion, and conse-
the same Momentum of the Pow-
be every where alike preserv'd ;

4.
*An Obser-
vation.*

the Weight, as is evident from the Make of this
is rais'd up no more than is answerable to the
the Rope that goes round the Axle in one turn-
of the Wheel.

is, so as to be the Tangent of the Point of the
ence it touches, according to *Chap. 1. S. 4.*

which

which otherwise would not be so, supposing (*Fig. 16*) the Power P so apply'd to any Spoke, viz. G , the Line of its Direction be GH , the Distance of the Power is to be IC , and so less than BC , and consequently the Momentum of the Power so much lessen'd, as IC is less than BC . Whereas if the Line of the Power's direction were GC , then the Momentum of the Power at C would be the same as at B .

5.
*Machines
and Instru-
ments refe-
rable
thereunto.*

To this third simple Machine is refer'd the Crane *Fig. 17*, and all Engines which consist of Wheels with Teeth, *Fig. 18*, and also the Machine represented *Fig. 19*, and the several other Instruments represented *Fig. 20, 21, 22, 24* and *25*. In each of which A represents the Place of the Weight, B the Place of the Power, and C the Center of Motion or Fulcrum.

CHAP. V.

Of the Pulley.

THE *Pulley* is a Machine consisting of one or more little Wheels, a- which a Rope being put and (*) at one End, the said Rope makes said Wheels turn round upon their Axles; and thereby at the same moves the Weight or Body to be or rais'd, as *Fig. 26, 27, 28.*

1.
A Pulley,
what.

The Pulley it self be fasten'd up to Place or Mark H, and the Weight apply'd to one End of the Rope, the Power P to the other, (as *Fig.* when it is evident, that as much as weight W ascends, just so much the P descends; and consequently that both move with the same Velocity. fore in this Case the Force of the must in it self be equivalent to the of the Body rais'd, in order to

2.
An upper
Pulley,
what, and
its Use ex-
plain'd.

Effect of this Machine being thus produc'd by Rope, hence it takes the Name of the *Pulley* a-

make

make its Momentum equal to the momentum of the Body. And hence follows, that such a Pulley does not conduce to the increasing of the Momentum of the Power, or (which comes to the same) to the decreasing the Momentum of the Body or Weight to be rais'd only to the keeping of the Cord from fretting; and so to the making it move more easily than otherwise would. And, because when there is occasion to apply several Pulleys together such as are of this Sort, (or where Ropes go over,) are plac'd upper and lower, hence these are distinguish'd by the name of *Upper Pulleys*.

3.
A lower
Pulley;
what, and
its Use ex-
plain'd.

But if (not the Pulley it self, but the End of the Rope be fasten'd to another Hook or the like, and the other End be led by the Power P , and the Weight hangs on to the Pulley, (as Fig. 3.) then it is evident, that in order to raise the Weight W one Foot, each Part Aa and Bb of the Rope must be shortened one Foot, (reckoning downwards from the Hook H and its opposite Point I) consequently that in the same Time the Power P must move two Foot. Therefore in this Case the Velocity of the Power will be double to that of the Weight, and consequently if the Power be double to the Weight, that is, as

Momentum will be equal to that of Weight, and so will sustain the Weight. And therefore if the Power be increased, it will be able to raise eight. And the same holds when there are two Wheels or Pulleys, one above and one Lower, as *Fig. 28.*

As *Fig. 29*) there be three Wheels, the Rope goes from Wheel to Wheel three times, *viz.* from A to B, and from B to D, and from E to F; and presently in order to raise the Weight W one Foot, each of the three Segments AB, CD, and EF of the Rope must be shorten'd one Foot, which is done without the Power P moving forward three Foot in the same Time. In this Case the Velocity of the Power will be triple or thrice as much, as the Velocity of the Weight. And though the Power be to the Weight as 1 to 3, yet its Momentum will be equal to the Momentum of the Weight, and so will sustain it; and if the Power be but a little increased, will raise eight.

4.
Further of
the same.

In the same manner it is evident from *Fig. 30.* if there be four Wheels, and so the Rope goes four times from Wheel to Wheel, then, while the Weight W is raised one Foot, the Power P will move four Foot; and consequently

5.
The same
yet further
exempli-
fy'd.

(C)

(by

(by the fundamental Theorem) er P, which is to the Weight W to 4. will have its Momentum the Momentum of the Weight therefore being a little increas'd, will it.

6.

The general Theorem relating to the Pulley.

Hence the Mechanism of the Pulley depends on this universal Theorem. If a Power is to the Weight, as the Number of the Ropes (*i. e.* of the of the Rope, *viz.* AH and Bh, and 28; and AB, CD, EF, *Fig. 29* AB, CD, EF, GH, *Fig. 30*.) applied to the lower Pulleys, then the Power will be able to hold up the Weight; and therefore being a little increas'd, will raise the Weight.

7.

Examples.

For Instance, Suppose the Weight be rais'd 360 Pound, and the Power itself to be equivalent only to 180 (*i. e.* the Power to be to the Weight to 2.) therefore one lower Pulley together with, as *Fig. 29* or without (per Pulley) will render the Momentum of the Power equal to that of the Weight, namely, by rendering the Velocity of the Power double to that of the Weight. For $180 \text{ p.} \times 2 \text{ Velocity} = 360 \text{ p.} \times 1 \text{ Velocity}$. If the Power be to the Weight as 1 to 3, equivalent only to 120 Pound, there must be three Wheels, that so the

the Power may be triple to that Weight; Namely, $120 \text{ p.} \times 3 \text{ Ve-}$
 $= 360 \text{ Momentum} = 360 \text{ p.} \times 1$
 y. And so on.

CHAP. VI.

Of the Screw.

THE Screw, which makes here the fifth simple mechanical Power, is a Cylinder, having several Risings or Ridges alternately winding round in a spiral manner. It consists properly of two Parts, one call'd the *outward* and the other the *inward*; namely, the former receives the latter in. Whence the inward Screw is often call'd the *Male*, and the outward the *Female* Screw. The Male or is denoted *Fig. 31*, by MS, the outward by TS.

This Machine is chiefly us'd to squeeze Things, and by that Means, in Cases, to break Things. It is also used to raise up any Weight, or thrust it forward.

1.
The Screw,
what's

2.
Its Uses.

(C 2)

For

3.
*This in
some sort a
compound
Machine.*

For the more easie Use of this Machine, (i. e. for the more easie turning of the Male Screw through the Female along the Male) it is to be apply thereto an Handle or round Rod AB; and so to the Power of the Axle to adjoin also the Power of the Axle to the Wheel: The Handle or Stick being turned round, supplying the Power to a Wheel, and the Cylinder of the Machine being as the Axle to the said Wheel, that this Machine is in some sort a compound Machine.

4.
*The funda-
mental
Theorem
particularly
apply'd
to this Ma-
chine.*

Now the Effect of this Machine depends upon the same fundamental Theorem, as the other; which fundamental Theorem particularly apply'd to the Construction of this Machine, thus: If, as the Compass describes the Power in one Turn of the Screw, the Interval or Distance between any two consecutive spiral Windings (measur'd according to the Length of the Screw) so is the Power or Resistance to the Power; then the Power and the Resistance will be equivalent to the other, and consequently the Power being a little increased will move the Resistance.

5.
*The same
further il-
lustrated or
prov'd.*

For it is evident from the Construction of this Machine, that in one Turn of the Screw, the Weight P (Fig. 1) is so much lifted up, or the Resistance

and 32) is so much remov'd, or
 ing to be press'd is squeez'd so
 closer together, as is EG the Di-
 between two immediate Spirals;
 the same Time the Power (ap-
 A or B) to be mov'd so much,
 the Compass AB, describ'd by the
 Power in one Turn of the Screw.
 the Velocity of the Weight (or
 answers thereto) will be to the
 of the Power, as is the said Di-
 between the Spirals to the Com-
 scrib'd by the Power, in one Re-
 or Turning round of the Screw.
 therefore by the fundamental Theo-
 as the Power is to the Weight, so
 the Distance between the Spirals to the
 describ'd by the Power, the
 will have its Moment equal to
 the Moment of the Weight or Re-
 And therefore the Power, be-
 come increas'd, will overcome the

C H A P. VII.

Of the Wedge.

I.
A Definition
of a
Wedge,
and its se-
veral
Parts.

THE Wedge is commonly made of Iron or some harder Sort of Matter, in Shape of a Prism not very long, whose opposite Bases are Isoscelar Angles. The Height of either of the Angles is esteem'd the Height of the Wedge, and the Basis of either is esteem'd the Thickness of the Wedge, and the right Line which joins the Vertexes of both the Triangles, is call'd the Edge of the Wedge; and the parallelogram which joins together the Bases of the two Triangles, is call'd the Back of the Wedge.

2.
Its Effect
accounted
for by the
fundamen-
tal Theo-
rem.

The Effect of this Machine is likewise upon the same Foundation as the former; which may be particularly apply'd hereto with this Theorem: *If the Power directly applied to the Back of the Wedge be to the Resistance overcome by the Wedge, as the Thickness of the Wedge is to its Height; then the Power will be equivalent to the Resistance, and therefore being increas'd will overcome it.*

The same
further il-
lustrated, or
prov'd.

Tenaciousness or Firmness, where-
Parts of the Wood (or the like) one to the other, is the Resistance overcome by the Wedge. Now it is evident, that while the Wedge is drove into the Wood, the Way or Length it has gone according to its own direction, is (Fig. 34) BA; and in the same manner DC is the Way or Length in the same Time by the Impediment, *i. e.* the Parts C and D of the Wood are so far divided asunder. And accordingly as the Wedge is drove down further and further along its Height, so the Parts C and D of the Wood are divided more and more along the Thickness of the Wedge; and in the whole Proportionably, as is evident from the Nature of a Triangle. Whence it may be concluded, that if as the Thickness of the Wedge (*i. e.* the Way of the Impediment, and consequently its Velocity) is increased to the Height of the Wedge (*i. e.* the Way, and consequently the Velocity of the Power,) so the Power to the Impediment or Resistance, then the Motion of the Power and the Impediment will be equal the one to the other, and consequently the Power increased will overcome the Resist-

4.
Other In-
struments
reducible to
the Wedge.

To the Wedge may be refer'd
Edge-Tools, and Tools that have
sharp Point, in order to cut, or
split, chop; pierce, bore, or the like.
Knives, Hatchets, Swords, Bores,
&c. And thus I have gone thro' the
six simple Machines, or primary me-
chanical Powers, so far forth as be-
quisite to the Design of this
tise.

5.
Mechanicks
what, in the
more re-
strain'd
Sense of
the Word.

It remains only to observe here
as the Word *Mechanicks* in its
Acceptation comprehends the whole
Doctrine or Science of Local Motion
in a restrain'd Sense it is taken parti-
cularly to denote the Doctrine of Motion
apply'd to Machines or mechanic
engines, the more simple of which
are here describ'd.

C H A P. VIII.

Of Staticks.

THE Word *Staticks* denotes in the Greek Language the Science or Do- of Weights, and consequently in the largest Acceptation, is of the same Extent with *Mechanicks* in the largest Sense of, both comprehending the whole Science of Motion with reference to the Weights of Bodies; and so synonymous Words, or Words of the same Import, But as the Word *Mechanicks* in a restrain'd Sense is taken to denote more particularly the Doctrine of Motion and Weights in reference to Mechanical Engines; so the Word *Staticks* in a restrain'd Sense is taken to denote especially that Part of the Doctrine of Motion, which arises from the Weight of solid Bodies consider'd in themselves compar'd together, and which consequently has not at least so immediate a Relation to mechanical Engines. In this Sense therefore I shall take notice of Particulars as relate to *Staticks* in its restrain'd Sense, and are agreeable to the Design of this Treatise.

I.
Staticks,
what.

It

2.

*The Motion
of heavy
Bodies
down-
wards is
uniformly
accelera-
ted.*

It is then observable in the first that the natural Motion of heavy Bodies (*i. e.* That Motion of them downwards which arises from the natural Principle of their Gravity or Weight) is found by Experience to be a *Motion uniformly accelerated*, *i. e.* a Motion which acquires equal Times equal Degrees of Velocity. For when an heavy Body descends under the same Gravity, which gave it a Motion downwards at first, will all along continue to act alike upon it, and so the Motion in the second Instant of Time will be equal to what it gave it at the first, and again in the third Instant or Minute it will likewise be a Motion equal to that in the first. So that at the third Minute the Sum of the whole Motion will be the Triple of the first; and so at the fourth Minute the Sum of the whole Motion will be Quadruple to what it was at the first. And the Degrees of Motion, or Velocity of the Body moved, will always increase as it does the Time wherein it moves.

3.

*The Spaces
thro' which
Bodies fall,
are as the
Squares of
the Time
wherin
they fall.*

Hence it comes to pass, that the Spaces, through which Bodies descend in their Fall, are as the Squares of the Time they take up in Falling, always increasing from the Beginning of the Fall. For Instance, if a Body be ten Minutes in Falling, and the first Minute it falls the second Minute it will have fallen

and the third Minute nine Miles; and
 According to which Proportion at
 tenth Minute, the Body will have
 an hundred Miles. Whence it ap-
 pears, that if the Times be taken in the
 arithmetical Progression of natural Num-
 bers, viz. 1, 2, 3, 4, 5, &c. the Spa-
 ces describ'd in those Times, reckoning
 from the Beginning of the Motion, will
 be 1, 4, 9, 16, 25, &c. This is wont
 to be demonstrated or at least illustrated,
 considering (*Fig. 35.*) AB to repre-
 sent the first equal Part of Time, and BC
 to represent the first Degree of Velocity
 describ'd in the first Part of Time: And
 the line BD ($=AB$) to represent the se-
 cond equal Part of Time, and FE ($=BC$)
 to represent the second Degree of Velocity, ac-
 describ'd in the second Part of Time, and e-
 ven it self to that Degree of Velocity
 describ'd in the first Part of Time: and con-
 sequently AD to represent two equal Parts
 of Time, and DE to represent two equal
 Degrees of Velocity. Wherefore the Tri-
 angle ABC will represent the Space gone
 thro' in AB, the first equal Part of Time,
 with the Velocity BC; and the Triangle
 ADE will represent the Space gone thro'
 in two such equal Parts of Time, with
 the Velocity DE (the Double of BC.)
 The said similar Triangles ABC and
 ADE are (by *Theor. 10 of Young Gen-
 tleman's*

elementary Geometry) as the Squares of their homologous Sides AB and AD, that is, the Spaces gone through in Times AB and AD are as the Squares of the said Times. Thus (Fig. 35.) AD is actually divided into four Parts, each equal to ABC.

4. The Spaces describ'd by the Fall of heavy Bodies, consider'd in each equal Part of Time distinctly by it self.

Hence it is obvious, that the Spaces describ'd or gone through by a Body in its Fall, in each (equal Part or) Minute of Time, are according to the Series of the natural Numbers, 1, 3, 5, 7, 9, &c. these being the Differences of the Squares 1, 4, 9, 16, &c. Thus if a Body fall one Mile in the first Minute, and three Miles in the second Minute, it will therefore, during the second Minute, fall double as far as it did in the first, consider'd distinctly from the first, fall four Miles. And in like manner, if a Body fall at the End of two Minutes six Miles, and at the End of three Minutes nine Miles, it will, during the third Minute consider'd by it self, fall five Miles, and so five Times as far as it did the first Minute.

5. How to find, what Space a Body will go thro' in a given Time.

Hence it is obvious, that the Space gone through in a determinate Time of any Body being known, thereby may be found out, what Space it will go through in a given Time; viz. by finding a fourth Proportional. For example, suppose a Body to fall twenty

in one Minute, and it be requir'd
How far the same Body will fall
in the same Medium in Three Minutes;
the Answer will be, 216 Foot. For as 1
(i. e. as the Square of one Minute
to the Square of three Minutes) so is
the Space gone through in the first
(i. e. to 216, which therefore is the
Space the Body will go through in three
Minutes.

In like Manner, the Time being known,
in an heavy Body descends through
an infinite Space, it is obvious to find,
how long Time it will descend thro' an-
y given Space, viz. by finding a fourth
Proportional. For Example, suppose a
Body has taken up one Minute in falling
through four Foot, and it be requir'd to
find what Time it will take up in falling
through 84 Foot in the same Medium; the An-
swer will be three Minutes. For as 24
(i. e. as the first Space given is to
the second Space given) so is 1 the
Time of the given Time to 9 the Square
of the Time requir'd, which therefore is
3 Minutes.

A Body in falling acquires equal
Degrees of Velocity in equal Times, so
contrary, in rising it loses equal
Degrees of Velocity in equal Times. For
the Velocity of the Body thrown up con-
tinually drawing it downwards, its Moti-
on

6.

To find,
what Time
a Body will
take up in
descending
thro' a gi-
ven Space.

7.

Of the Af-
cent of Bo-
dies.

on upwards will continually decrease in proportion to the Force downwards, being reduced in equal Times by the Gravity of the Body. But it has been shewn (§. 2.) that the Motion downwards is uniformly accelerated; and therefore the Motion upwards must be *uniformly retarded*. Whence it follows, that the Body goes through the same Space in equal Times, in rising as it does in falling, but in an inverted Order. Name the Body be five Seconds in rising to the Height of twenty-five Foot, and the Body ascended through the first Second of Time be nine Foot, the said Body will in the second Second of Time, will go through a Space of seven Foot; in the third Second a Space of five Foot; in the fourth a Space of three, and in the fifth and last a Space of one Foot; so that it will be as it were in *Æquilibrium*, the Impetus upwards being now equal to the Impetus downwards. The Body will neither rise nor fall for any Time. After which it will begin to fall in the like inverse Proportion, so that the first Second it will fall three Foot, the second three Foot, the third five Foot, the fourth seven, and the fifth and last nine Foot, thus taking up five Seconds to descend twenty five Foot, as it took the same Time to ascend twenty-

*Why Bodies
rise up a-
gain to the
same
Height,
from which
they fell.*

the same Principles it comes to
that the Force which a Body ac-
in falling, will make it rise up a-
to the same Height which it fell
For Instance, suppose (Fig. 36)
Pendulum, i. e. the Body or
fasten'd to one End A of the
AB, whose other End is fasten'd
fix'd Point C, as the Center of its
: Suppose, I say, the Body to
D to A, it will rise again to E,
is of an equal Height with D. For
DA into any Number of equal
suppose three, markt *a*, *b*, *c*, and
as many markt *d*, *e*, *f*, E. By
going Principles it is obvious,
whatever Force or Degree of Velo-
Body acquires by its Gravity in
ing from D to *a*, it will acquire
much in descending from *a* to *b*,
as much in descending from *b*
with which triple Force it will be-
scend from *c* towards *d*. But in
g from *c* to *d* the Body will by
ity drawing downwards lose one
ree acquir'd Degrees of Velocity
; and in ascending from *d* to *f*
se two of the said acquir'd De-

So call'd from the Weight's hanging on the
Wire, to which it is fasten'd; the Latin Word
signifying any Thing that thus hangs.

grees

grees, the Force of Gravity down at f being double to its Force at d , so destroying two of the acquir'd Degrees of Velocity or Force, wherewith the Body at c began to ascend. And like E , the Force of Gravity downward be triple to that at d , and so destroy the three acquir'd Degrees of Velocity wherewith the Body began at c to ascend: And therefore the Body will ascend no higher, but begin to fall downwards again towards c or A .

9.
The Resistance of the Air not consider'd in the foregoing Cases.

But now it is to be observ'd, that this and the foregoing Cases, the Resistance of the Air, wherein the Body is conceiv'd to move, is not consider'd, which is the Cause why the foregoing Theorems will not exactly agree with Experiments, and particularly with the Pendulum, which, by means of the Resistance of the Air, does not return exactly to the same Height from which it fell, and consequently have not a continual Vibration or Motion forward and backwards, but stand still in some

10.
Pendulums ascend and descend thro' equal Spaces in equal Times, &c.

Abstracting from or setting aside the Resistance of the Air, it follows from the foremention'd Principles, that the Pendulum does ascend and descend thro' the equal Spaces DA and AE in equal Times. To which I shall here add, worth remarking, that the Lo

pendulums are as the Squares of the
times, wherein they perform their Vibra-

Gravity is that natural Principle
which causes Bodies to descend, so no
Body will descend, but when its Center
of Gravity can descend. Thus the in-
clined Body ABDE, (Fig. 37.) which is
in the Horizontal Plane HP, cannot
descend toward the Part D, to which it in-
clines, because by such a Change of Situ-
ation its Center of Gravity C would rise;
which may be known by describing from A
(the Center) the Arch CF, which is
the same, as C the Center of Gravity
would make about the Point A, if the
Body ABDE could fall; for it is evident
that one Part of that Arch rises above
the Point C, and consequently the Cen-
ter of Gravity in such a Case must for
some Time ascend of its own Accord,
which is contrary to the Nature of heavy

II.
*How the
Fall of Bo-
dies de-
pends on
their Cen-
ter of Gra-
vity.*

on the contrary, the inclin'd Body
(Fig. 38) must of necessity fall
toward the Part D, which it inclines to,
because its Center of Gravity C may de-
scend in such a Situation; as will appear
(as before) from A through C
the Arch CF, which is the same that will
be describ'd by C the Center of Gravity
about A, when the Body ABED falls :)
(D) For

II.
*The same
further il-
lustrated.*

For all the Points of the said Arch below the Point C.

13.
Of Bodies
standing
firmly.

Hence it appears, that to have a Body keep firm upon any Thing, that supports it, and is not itself inclin'd, the Line CE drawn from the Center of Gravity in the said Body toward the Center of the Earth, and wherein the said Body endeavours to descend (i. e. in the Line of Direction) must necessarily fall in some Part of the Base or Foot of the said Body, as Fig. 37. Other-
wise if the Line of Direction CG falls without the Basis, the Body will necessarily fall down, as in Fig. 38.

14.
Further of
the same.

Whence it follows, that by how little the Basis of a Body is, even though it be not inclin'd, so much more easily will it be mov'd out of its Place; because the lesser Change of Position is capable to make the Line of Direction be without the Basis or Foot. Which is the Reason why a Bowl rolls easily upon a Plane, and that a Needle will not stand upon a Point. It is obvious, that agreeable to what has been said, it follows also, that the wider the Foot of a Body is, the more firmly will it stand, because the greater Change is necessary to cause the Line of Direction to fall out the Foot of the said Body.

appears also from what has been
that if the Plane OP, which sustains
Body ABDE (Fig. 39) be inclin'd,
Body will slide, when its Line of
Direction CG falls upon any Part of its
AD. And that a Body *abde* will fall,
if its Line of Direction *cg* falls with-
the said Base *ad*.

15.
Of the slid-
ding and of
falling up-
wards or
downwards.

Hence it follows, that a Bowl set up-
on an inclining Plane, as the Roof of an
e, will roll off it, because its Line
of Direction not being perpendicular to
the Plane, (but to the Horizon,) can-
not pass through its Foot where it touches
the Plane, it being almost an indivisible

16.
Further of
the same.

is remarkable, that we naturally
use this Law of Staticks, we are
speaking of, to keep our selves from
falling. Thus, when we would rise from
a Seat, we bend our Body, by thrust-
ing forward our Head and Back HB,
and putting backwards our Feet and Legs
(Fig. 40) so as the Line of Directi-
on of our Center of Gravity may pass
through our Footing F or Basis. And it
is obvious, that if we bend not enough,
we fall backwards or towards B; but if
we bend too much, we fall forwards or
towards F or K.

17.
Why a Man
bends,
when he ris-
es from a
Seat.

18.

*Why a Man
leans for-
ward when
he goes up
Stairs.*

In like Manner, when we go up Stairs, as we lift one Foot up, so we bend our Body forward, that we may (both easier, and also) may preserve ourself from falling backwards, by having a Line of Direction of our Centre of Gravity too far from our Footing, in this Case is chiefly the Foot up upon the Stair, when we are going up.

19.

*Other com-
mon Pos-
tures ac-
counted for.*

On the same Account it is, that a Man carries a Burthen on his back; he leans forward; but if he carries a Burthen before him, he leans backward. If he carries it with his right Hand, he leans to his Left; if with his left Hand, he leans to his Right. Namely, hereby he (may not only more easily carry the Burden, but also) may preserve himself from falling that way, in which the Burden he carries, is.

20.

*The like
Rules ob-
serv'd by
irrational
Creatures.*

And that we learn this, not from Reason, but rather from natural Instinct, is evident, not only from Mens doings, but also from irrational Creatures doing like. For a Goose going through a Door, or other Door, be it never so low, does thrust forth, and so downwaards his Head, not because he is afraid of

...aint what is so much above it, but)
conformity to this Law of Staticks.
ely, at a Barn Door there is usually
reshold or the like, to be gone o-
Wherefore the Goose, having put
Foot on the Threshold, thrusts
ard his Head, that his Center of
ity may not be too far behind his
and so pull him backwards; but
by thrusting his Head and Neck so
is requisite beyond the Threshold,
Direction of his Center of Gravity
e brought so near to his Footing,
at he may go over the Threshold
easily, and without falling either
ward or forward. So that it appears,
oose is not to be laugh'd at for so
but rather they, who neither
the Reason of his so doing, nor at
that he does no other than they do
selves in like Cases. And this is suf-
to our Design, to have taken no-
concerning Staticks, so call'd in a
restrain'd or proper Sense.

C H A P. IX.

Of Hydrostaticks.

I.
Hydrosta-
ticks, what.

TH O' the Word *Staticks*, both its own literal Import, and all its largest Acceptation, denotes the ence of the Weights of Bodies in g^ral, whether fluid (or liquid) or noⁱid, and whether weigh'd in the Water ; yet it is usual to restrain *Staticks* in a more appropriated Sense to denote Science of the Weights only of solid (not fluid) Bodies, and that too weigh'd in the Air ; and to give the peculiar Name of (*) *Hydrostaticks* to that Part of *Staticks* largely taken, which treats of the Weight of fluid or liquid Bodies, especially of Water, and of solid Bodies put into (†) liquid Bodies especially into Water.

(*) It is a Greek Word, compounded of *statos*, Science of Weights, and *hydor*, Water.

(†) There is this Difference between a *fluid* and a *solid* Body. A *Fluid* is a Body, whose Parts are easily separated, and being separated join together immediately.

The primary Property of heavy Fluids are these; that if an heavy Fluid (Fig. 41) be, either not press'd or equally press'd from above; its Surface AB will lie horizontal or

And if the said Fluid be disturb'd it will by its own Gravity return to same Level of its upper Surface. For lower Particles of the Fluid will not, reason of their Gravity, ascend up of themselves, to raise any Part of said Surface above the other; nor the upper Particles of the Fluid descend, since there is no Room for them, the lower Part of the Vessel, it being up by other Particles of equal weight. And therefore if there be no pressure at all from above, or an equal pressure, then there is nothing to disturb the Level of the upper Surface. If it be disturb'd, the fluid will return to its Level, because the higher Part (Fig. 41) being heavier, will partly press the Particles under it, and will run down into the lower Part;

same, Water, Oil, and other Liquors. A Liquid is whose Parts are also easily separated, and again together immediately, and withal will continually spread themselves, till their upper Surface becomes as Water, Oil, but not Flame. Hence it appears, Liquids are Fluids, but all Fluids are not Liquids.

(D 4)

and

and that so long, as any one Part Surface is higher than the others.

3.
Further of
the same.

If the Fluid (*Fig. 42*) be from unequally press'd, it is obvious, the Part thereof AE, which is most press'd, will descend, the Particles so press'd thrusting out of their Places the Particles, that are either not press'd at all, or less press'd; which therefore ascend to HI in proportion to the Ascent FG of the Particles press'd. Namely, as the Part press'd AE is to the Part not or less press'd E, so the Ascent EH or BI will be equal to the Descent AF or EG.

What has been said of the upper Surface AB, holds good of any other parallel Surface within the Fluid, as in *Fig. 43*. Namely, if it be equally press'd from the upper Part of the Fluid, and not by any Thing else swimming either at the Top or within the Fluid, it will retain its horizontal Situation or Equilibrium. But if it be any where press'd more than in other Parts of it, there it will descend, the Parts of it which are less press'd ascending as that descends. And all that has been hitherto said, are included in the following Propositions, as follows the Corollaries.

A heavy Body EFHB (Fig. 44.)
upon a Fluid AB, be of an equal
Weight with the Air that takes up an e-
qual Space AHEG, the Surface AB of the
Fluid will retain its Level, as being eve-
ry where equally press'd.

The Body EFIK (Fig. 45) be lighter
than the Air which takes up the like
Space, then the said Body, and the Por-
tion of the Fluid under it, will ascend,
till the Aggregate (of the Body IKEF and
the Parts EFHB of the Fluid so as-
cended, viz.) IHBK be of equal Weight
with the Air, that takes up the like Space
AHEG. For then the Surface AB will be
equally press'd every where, both in AH

4.
*Corollary
the first.*

5.
*Corollary
the second.*

The Body EFAB, (Fig. 46,) be hea-
vier than the Air of a like Bulk, then
it will swim in the Fluid, de-
scending so far into it, 'till the Aggre-
gate of the Air GEIK and the Fluid
(viz.) AHEG, which take up to-
gether an equal Space with the said Body, be
of equal Weight with the Body. For
then the Surface AB will become equally
press'd both in AH and HB.

6.
*Corollary
the third.*

The Body EGDF (Fig. 47) be hea-
vier not only than the Air, but also
than the Water (or other Fluid) that
takes up a like Space HCGE, then the
Body will sink down quite to the Bottom

7.
*Corollary
the fourth.*

CD.

CD, there being nothing to counter or bear it up, till it comes to the bottom. For the Body being supposed put on the upper Surface AB, and upon the Part IB thereof, it being heavier than a like Bulk of Air, the the Fluid IBDE will be more thereby, than the other Part of the Fluid AIEC by the Air, and therefore Particles in IBDE will descend in like Manner when the Body is under GF, it being heavier also than the Bulk AHGI of Water, it will therefore cause the Parts of the fluid Water that are those that are under GF, therefore will cause the Parts under GF to still to give way, till it comes to the bottom CD.

8.

Corollary
the fifth.

Upon the same Principles, if a Body GHK (Fig. 48) be immerg'd in a Fluid, and be (of equal Weight) much EFGH of the Fluid as takes up like Space, *i. e.* in short, be) of the same specifick Gravity with the Fluid, the said Body will stay where it is in the Fluid, without either rising or sinking. For the Surface EI being equally press'd all along, the said Body will not rise. And the Surface FK being equally press'd, neither can the Body sink.

(†) Gravity with the like Bulk of EFGH, the Surface EK will be press'd, both in FH, and HK; and fore the Bucket of Water can't but is held up by the Water and consequently the Weight of more felt, than is a Weight counterpois'd by an equal Weight a Balance. And the same holds while the Bucket is drawing up Surface AB. Where it, and th in it, coming into the Air so much lighter than the Water or &c. of the Bucket, the Air can it, and so the Weight of it maintain'd then by him that draws Bucket.

10.
Why the
Depths of
some Seas
cannot be
fathom'd.

On the same Principles the why one cannot fathom the Depth of Sea in some Places, is this: Because the Plummets or Leads made use of are specifically heavier than Water, yet to which the Plummets are fasten'd (in this Case) specifically lighter than

(†) The Water in the Bucket is certainly of specific Gravity with the Rest of the Water. Bucket, if all of Wood, is much lighter. And wife, the specific Gravity of the Wood is the specific Gravity of the Iron about the Bucket to an *Equilibrium* with the Water.

Wherefore when the Depth is that such a Quantity of Line is as that the Weight of the Line together is no greater than the of a like Bulk of Water, then the Plummets will sink no deeper; consequently will not shew the Depth in that Place.

According to the same Principles we may tell, why one Liquor will swim on another, or remain at Top without sinking, if it be pour'd on gently; as Oil on Water; and Water in Mercury. Namely, because it is specifically lighter than Water, and than Quicksilver.

likewise it ceases to be a Wonder, that a Ship, which has sail'd in the Sea, has sunk and been lost in the Mouth of a River of fresh Water; namely, because Sea-water is much heavier than fresh Water. And therefore though the Ship with its Burden was lighter than the Bulk of Salt-water, and so was kept afloat by the Salt-water in the Sea, yet it is heavier than a like Bulk of fresh Water, and therefore sunk in the River. It is obvious, that for the same Reason, a Ship or Boat will draw more Water (that is, though it does not sink to the Bottom, yet will sink deeper) in fresh Water than in Salt-water.

II.

Why some Liquors swim upon others.

I 2.

Why Ships, that sail in the Ocean, sink in fresh Water.

13.

*Why Wood,
that will
swim for
some time,
sinks after-
wards.*

Moreover the Reason, why a Wood, that has been swimming time upon Water, will sink at last, is, because such a Piece of Wood may be of the same or greater Gravity than Water, filling the Pores of the Wood; but by reason of the Pores, the Air which fills the Pores, and the Wood together, make a Whole lighter than an equal Bulk of Water, and therefore the Wood will swim at first. But after some Time the Air being got into the Pores, and excluded, then the Water in the Pores and the Wood make up one Whole, which is heavier than the Water of a like Bulk, so must sink according to the Principle of Hydrostaticks aforementioned.

14.

*Why hollow
Vessels of
Brass or Iron
will swim, when
Lumps of
the same
Metal will
sink.*

From which Principles it follows that although a Lump of Brass or other Metal will sink in Water being specifically heavier; yet a Lump of the like of Brass or Iron (&c.) will sink but swim; because the Air contained in its Hollow, makes one Whole, which is much lighter than an equal Bulk of Water.

15.

*A Body will
weigh less
in Water,
than in Air.*

It follows also, that a Body will weigh less in Water than in Air, by as much as is the Weight of an equal Bulk of Water. Whence it comes to pass, that two Pieces of Metal of different

suppose one of Gold and the Silver, which shall be of equal in the Air, will not be so in the Water. That Metal whose specific Gravity is greatest, (viz. the Gold) takes up the Room of a less Water.

Fig. 49.) a Fluid, particularly Quicksilver contain'd in the Tube CD presses on the Part C of the Surface AB, more than the Air presses on the other Parts, C will descend, and the Fluid will run down out of the Tube, till the Part CI in the Tube presses C, as much as the other Parts are press'd by the Air. And then no more will run out of the Tube, because of the equal Pressure in all Parts of the Surface AB. It is to be noted, that the Weight of the Quicksilver CI is equivalent to the Weight of a Column of Air, extended from the Surface AB up to the Top of the Sphere, and of the same Basis and Height as the Tube CD.

It is observable (Fig. 50) that Quicksilver will rise up just to the same Height in the oblique or sloping Tube, as it does in the upright Tube. Though the Quick-silver EF in the sloping Tube be more, and consequently heavier,

16.

Why a Fluid in a Tube will stand up higher than the same Fluid without the Tube.

17.

Why a Fluid will rise to the same Height in a sloping Tube, as in an upright Tube.

heavier, than the Quicksilver C
 Tube CD. The Reason whereof
 that as much as the Quicksilver
 more than the Quicksilver CI,
 greater is the Basis E than the
 (this being equal to the Basis of
 linder EK, wherein the Quickfil
 will be found to be just so muc
 Quicksilver EF, by reason of
 Tubes EK and EG being Cyli
 Equal Height upon the same Ba
 therefore Equal one to the other.
 it is obvious that supposing the B
 be Twice as big as the Basis
 consequently the Quicksilver E
 Tube EK (or the Quicksilver E
 Tube EG) to be Twice as muc
 Quicksilver CI in the Tube CD
 dently follows that as the Q
 CI do's equiponderate to a C
 Air of the same Basis C, so th
 silver EH (or EG) which is t
 ble Quantity of CI, do's but
 derate to a Double Quantity
 i. e. to a Column of Air, wh
 E is the Double of the Basis C.

18.

*Further of
 the same.*

Since according to the Rule
 ticks, Bodies gravitate or we
 vier in a Perpendicular, than
 Oblique or sloping Situation,
 be ask'd, why the Quicksilver
 tating or pressing upon the Bas

And

do's the Quicksilver EF, (that be-
 perpendicular to E, this oblique,)
 Quicksilver do's not descend lower in
 Tube EK, and ascend higher in the
 EG. The Reason then is this,
 as much as EH presses downwards
 than EF, so much do's the Force
 which (arises from the Pressure of
 on the other Parts of the Surface
 and) sustains the Quicksilver in each
 press upwards more in the up-
 than in the oblique Tube; and
 for the same Reason, *viz.* because
 Pressure, whether upward or down-
 wards in the Tube EK perpendicular,
 as in the Tube EG it is oblique,
 therefore not so great. Now the
 at E, which holds up the Quick-
 in the upright Tube, being as to
 so much greater than the Force at
 holds up the Quicksilver in the
 as the Weight of the Quick-
 in the upright Tube, is greater
 the Weight of the other; it fol-
 lows that the said Force at E acting
 according to the Perpendicular
 is able to sustain the Quicksilver
 in the upright Tube, as is the same
 acting upwards according to the
 Line EF to sustain the same
 of Quicksilver in the oblique
 And therefore the Quicksilver in
 (E) the

the upright Tube will not descend by Running any of it out of the Tube, nor will the Quicksilver oblique Tube ascend any higher by any more Running into it: but the Quicksilver in both Tubes will keep equal Height.

19.
The Shape
of the Vessel
makes
no Difference
as to
the Rising
of the
Fluid.

And the same will hold as to the other Tube (or Vessel) of any Shape: Namely, the Height of the Quicksilver will be the same in any Vessel it is in a Cylinder of the same Height and Basis with the Vessel. The Instance, *Fig. 51*, the Height of the Quicksilver is the same, both in the round-headed Tube *DEHF*, and in the sharp-headed *KLB*, as it is in the Cylinder inscrib'd in the former, and in the Cylinder *BLOP*, circumscrib'd about the latter. For as to the round-headed Tube *DEHF*, as much Quicksilver as lies without the Cylinder *CI*, is sustain'd not so much by the Parts *MT* and *NS* of the Tube which are under them, and not by the Quicksilver is properly or directly sustain'd by *C*, than what lies within the Cylinder *CI*. And consequently the Height will be the same, as if the Quicksilver were put in the Cylinder *CI*.

to the sharp-headed Vessel L BK, 20.
 e Cylinder B L O P, the Quicksilver *Further of*
 likewise rise as high in the one as *the same.*
 ter. For as to so much of the
 fel, as allows a free Ascent from
 face A B, the Quicksilver will there
 its just Height C I, for the same
 as it will rise to the same Height
 Cylinder B L O P. As to the other
 of the said Vessel, where the
 ver is hinder'd by the Sides of
 fel to rise up to the Height C I,
 as is there wanting in the Weight
 Quick-silver, which is over the
 re subjacent Parts of the Surface
 much is supply'd by the Sides of
 fel. For although the Sides of
 fel do not press downwards as a
 Force, yet they keep the Quick-
 om being thrust Higher by the
 at presses upwards. And conse-
 the several Parts of the Sides
 look'd on as so many Impedi-
 which are equivalent to the Weight
 such Quicksilver, as would be
 between the respective Parts of
 , and the Parallel to I. And so
 ce A B will be equally prest all
 der the Vessel B.

21.

Why the
Fluid rises
higher in a
Tube at the
Bottom,
than at the
Top of a
Mountain.

The Pressure of the Air being which makes the Quicksilver rise in the Tube; it follows, that the greater Pressure of the Air, the higher will the Quicksilver rise; which is the Reason that the Quicksilver will rise higher in the same Tube at the Bottom of a Mountain or considerable Hill, than at the Top. Namely, because the Column of Air pressing the Surface AB will be longer at the Bottom, than at the Top of the Mountain, as is the Height of the Mountain; and consequently the Column containing so much more Air will press so much more.

22.

Of the
Weather-
Glass.

So as to the (*) Barometer or Weather-Glass, the Quicksilver rises and falls in the Tube, as the Air is heavier or lighter, and so more or less pressure is made on the Quicksilver that is in the Well (or Bottom) of the Barometer. And this is agreed by all: but what it is that causes the Air to be sometimes heavier and sometimes lighter, is not so easily known. That the Vapours do not, (as is commonly suppos'd,) increase the Gravity of the Air, seems more

(*) It is so call'd as being a Measure of the Weight of the Air, the Word *Balanz* signifying Weight, and *Barometre*, in the Greek Tongue.

on this Account: Namely, that the Vapours are in the lower Region of the Air, as in rainy Weather, the Air is lightest, as appears by the falling of the Mercury (or Quick-silver) in the Barometer. And when the Vapours are in the middle Region of the Air, when the Clouds are high,) do not increase the Pressure of the Air, for although the Air be heavier it is not because the Clouds are high, but the Clouds are high, because the Air is heavy. For when the Air is more dense than usual, it becomes heavier than the Vapours, which therefore must ascend, and settle in that Region of the Air, where it is of the same Gravity with them. If the Vapours were the Cause of increasing the Air's Gravity, there would be as many Vapours in the Air at a given Height as are equal in Weight to three Parts of Mercury, for so much we find the Mercury rises or falls in the Weather-Barometer. Now Mercury is about 14 Times heavier than Water, and consequently there must be in the Air at once so many Parts of Water as are equal in Weight to a Part of Mercury of 42 Inches in Height, whose Basis is equal to the Surface of the Earth; which is much more than falls in Rain, during a whole Year.

(E 3)

For

For a whole Year's Rain: do's no Vessel above 14 or 15 Inches high observ'd in the *History of the Royalty at Paris.*

23.
The probable Cause of the Rising and Falling of the Mercury in a Weather-Glass.

The Reason then, why the heavier at one Time than another more probably from there being Air on that Part of the Earth's Surface when the Air grows heavier. As proceeds from Winds. For Example the Wind, which is nothing but a Mass of Air, should blow on any Place the Air thus mov'd should be heaped up at that Place by Mountains or Hills. If two contrary Winds should blow on the same Place; in either Case the Air will be heaped up in the Middle; consequently there being more Air, Gravity will be increas'd. But in the aforesaid Circumstances, or the contrary, it will not happen in any particular Place, then the Air which is over it, will be less in Quantity, and consequently lighter. Whence it is probable, that Winds are the Causes of the Variation of the Air's Gravity.

24.
Of the Siphon, or Instrument us'd to draw off Wine or other Liquors out of Vessels.

It was afore (§. 16.) intim'd that what has been said in that and following Paragraphs concerning Gold or Quicksilver, holds true likewise in respect of other Fluids. But the mention'd Affections have been

particularly as to Quicksilver, foras-
 much as it is that which is us'd in Wea-
 thers, wherein the said Affections
 are frequently seen by Us: It be-
 comes the Design of this Treatise by the
 Principles of Mechanicks to ex-
 plain such Things as more fre-
 quently occur in common Use. On
 Account I shall add here the Ex-
 position of the Effect of the Siphon, (or
 what is us'd by *Vintners*, &c. in
 drawing off Wine, or the like,) accord-
 ing to the forementioned Principles of
 Mechanicks, or more particularly of
 Statics. It is then obvious, that
 (1.) the Air being suck'd out of
 the Vessel at E, the Wine (or other Li-
 quor) in the Vessel ABFG will be thrust
 up by the Pressure of the Air upon the
 Surface AB, into the other End H of the
 Siphon apply'd to the said Surface. And
 the Wine will be thrust upwards in the
 Siphon till the Weight thereof comes
 to Equilibrium with the Pressure of
 external Air, suppose 'till it comes
 to the Height CI. If therefore the Top
 of the Siphon be not higher than I,
 the Wine will rise to the said Top of it;
 and finding a Vent or Passage down
 the lower Leg DE of the Siphon, it will
 run away, and so run out at E; con-
 sequently so to do, the Causes still conti-
 nuing;

nuing, 'till the Vessel is emptied. is to be observ'd, that the Mouth of the Siphon must be lower than the Mouth H. For else, E and H being equally press'd by the Atmosphere, Leg DE be but of an equal Length DH, and consequently the Fluid of equal Gravity, with the other; the Fluid would stay in the Siphon, not moving one Way or other, without some other external Force beside the Air. And by Parity of Reason, if DE be shorter than DH, the Fluid contain'd in DE of less Weight than that in DH, the Fluid would (not from H to E, but) from DH to E, the Air coming up at E, and pushing the Fluid forward the contrary Way. This would happen, except at the Mouth of the Siphon be so wide, as that the Fluid may ascend by the Sides of the Siphon, and the Fluid it self descends in DE.

25.
The Mechanism of a common Pump, explain'd.

Proceed we next to explain the Mechanism of a Common Pump (Fig. 1) by the Principles of *Hydrostatics*. The Handle KL being thrust down, the Piston GF is drawn upwards from E, and with it the Air that lies between E and GF. Wherefore the Water at the Bottom of the Siphon, being without the Hollow of the Piston, is press'd by the Air, but the Hollow of the Pump at C being

last, not so much) press'd by the
will therefore ascend from C to D,
thrusting open the Valve E, (as ha-
no Weight or Pressure upon it,) will
d still higher to the Bottom of the
as meeting with no Pressure from
and being continually press'd up-
from Beneath. The Water ha-
thus fill'd the hollow Part EF of
ump, and the Sucker FG (by lifting
the Handle KL) being forced down-
do's force also downwards the
under it between F and E, and
is Means forces down and keeps
down the Valve E. Wherefore the
between E and F being thus
by the Sucker; and having no
downwards through E, it lifts up
valve G of the Sucker FG, this be-
the only Way it can make for it self.
Water thus arising above the Sucker,
ether with it (the Valve G being
down by the Weight of the Water
upon it, so that the Water can't
back that way again; and the Han-
being thrust downwards again)
upwards; where finding an open
e, it runs out at the Mouth H of
out, other Water ascending up in
can while through D, (as afore,)
the Sucker is drawn up. And thus
ually, as long as the Handle is
lifted

lifted up and down, and consequently the Sucker is moved up and down the same Causes being thus continued.

26.

Why some
Wells will
not be made
Pump-
Wells.

It is obvious from the Principles of Hydrostatics, that the Distance between the Water at the Well, and the Valve E, (or Bottom of the Sucker when at the Lowest, E,) must not be greater than the Height, where the Pressure of the Water is sufficient to make the Water rise, which is found by Experience to be about 34 Foot. Hence such Wells, as have Water lying so deep, as that a Sucker can't be made, but the Distance is greater than the aforesaid Altitude of the Pump Wells, but must be drawn up by a Bucket and Rope, and not by a Pump, but by a Bucket and Rope.

27.

The Tide
explain'd
by the Prin-
ciples of
Hydrosta-
tics.

I shall conclude this Chapter, shewing how that the Rising and Falling of the Sea Water, which is the Tide, is and which has been so long observ'd, but is by none of the old Philosophers, as I know of, rably accounted for, may be naturally accounted for by the Principles of Hydrostatics, after such manner as is very easy to be comprehended.

Why the Tide always comes to Us from the South.

The Moon's Orbit being over those of the terraqueous Globe, which between the Tropicks, and where are the largest Seas, as she passes over Seas, she presses (those Particles of Water which are next under Her, and the next underneath, and so the intermediate Air, and thereby at the Water of the Sea, and so causes the Water to rise, on each Side of Part of the Sea which lies under her that is, toward the North and Parts of the World. Hence to us live in the northern Parts of the World, the Tide always comes from the South, because the Moon's Orbit is South of them. And on the like Account, the Tide comes from the North, to those live in the southern Parts of the World, because the Moon's Orbit is North of them. And hence it is evident that the Tide must come so much sooner or later to any Place, as it lies more or less distant from the Tropicks, in that Tract of the Sea which is under the Moon's Orbit.

The Tide being thus caused by the Motion of the Moon, it plainly follows, that because the Moon comes every Day to the Meridian of any Place fifty Minutes later than the Day before; therefore the Tide likewise must fall out fifty Minutes

Why the Tide comes every Day fifty Minutes later than the Day before.

Minutes later every Day, than the before, in Respect of any particular Place.

30.

Why the Tide is six Hours coming in, and six Hours going out.

Also, because the Moon is six Hours in coming from the Horizon of any Place to its Meridian, therefore (it is obvious, that) the Tide must be six Hours in coming in. And in like manner, because the Moon is six Hours in going from the Meridian to the Horizon of any Place, therefore the Tide must be the same Time in going out. Where it is obvious, that as the Pressure of the Moon begins in respect of any particular Place, so soon as she comes to its Horizon her Pressure continually increases till she comes to the Meridian of that Place, consequently the Tide rises still higher and higher, till she comes to the Meridian. Which as the Moon goes again, so her Pressure decreases, consequently the Tide sinks lower and lower.

31.

Why the Tides are Bigger at the Change and Full of the Moon, than at other Parts of the Month.

Moreover it being agreeable to the Laws of Staticks, (as is found by Experiments,) for heavy Bodies to gravitate so much more, as they are nearer to the Center of the Earth; hence the Reason why the Tides are Bigger at the Change and Full Moons, than at the Quarter Moons, is easily to be assign'd; namely, the Moon's being at her Change and

to the Earth, than at her Quar-

in it is observ'd, that as the Tides

32.

Change and Full of the Moon are

Why the Tides at the Change and Full of the Moon about the Equinox's are bigger, than at other Parts of the Year.

than at any other Time of the

so the Tides at the Change and

of the Moon about the Equinox's

bigger, than those at any other Time

Year. Which may be accounted

by the Moon's being then over the

Part of the Ocean, which is un-

der the Celestial Equator, and conse-

quently by its Pressure thereon making

the Quantity of Water recede to

Sides, viz. Northward and South-

ward than when she presses on one Side

the Equator, and so not in the Middle

Ocean.

It remains to be observ'd, that it is

33.

strange (†) by the Principles of

Why there be Two Tides in every twenty-five Hours.

that the Moon do's cause (the

swell, or in one Word) the Tide,

only in that Part of the Sea which

is over, but also in the Part opposite

And hence it comes to pass,

as would have a more accurate Account of the

him consult *Newton's Phys. Mathem. Lib. 3.*

37, and Numb. 16. of the *Philosoph. Transact.*

as also *Gregory's Astron. Phys. and Geom. Lib.*

I have here contented my self with a more

account, as being more Easy to be under-

that

that there be two Tides every five Hours; namely, because Time the Moon going from the meridian, returns to it again; and consequently causes one Tide, while she is in the upper Hemisphere, and another while she is in the lower Hemisphere.

34.

And thus I have taken Notice of much of *Mechanicks* (in general, including *Mechanicks*, *Statics*, and *Hydrostatics* properly so called,) answerable to the Design of this

work.

And thus I have taken Notice of much of *Mechanicks* (in general, including *Mechanicks*, *Statics*, and *Hydrostatics* properly so called,) answerable to the Design of this

F I N I S.

Fig. 1.

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Fig.

D
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Fig. 7

Fig.

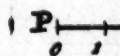


Fig. 12

W. —

Mechan. Plate. 2.

Fig. 6



Fig. 7

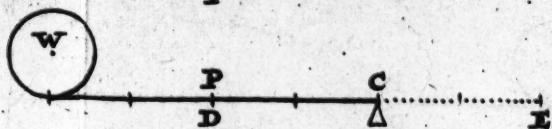


Fig. 8

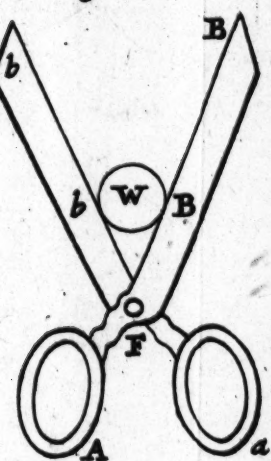


Fig. 9

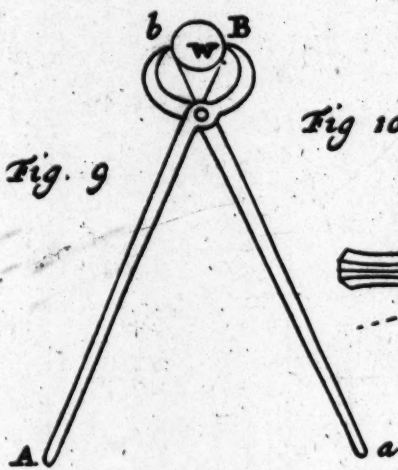


Fig. 10

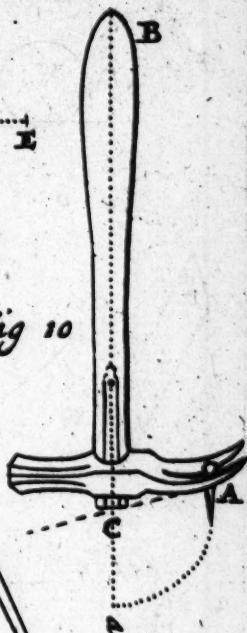


Fig. 11

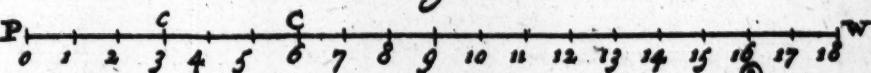


Fig. 12

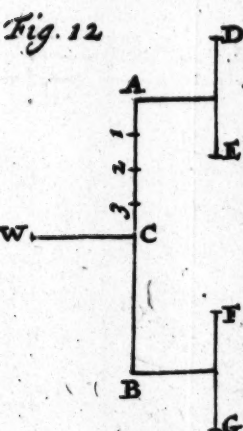


Fig. 13

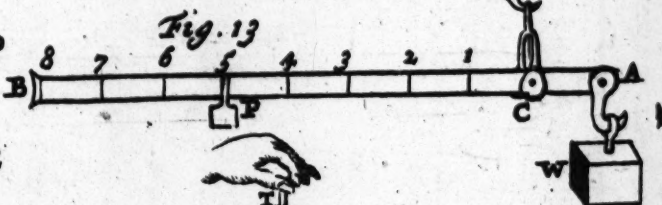


Fig. 14

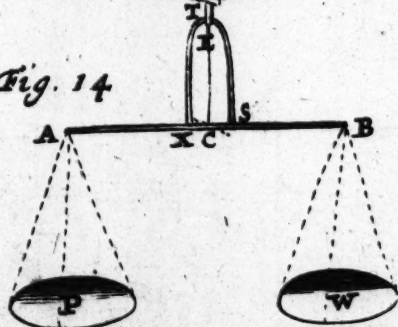




Fig. 1.



Fig. 15

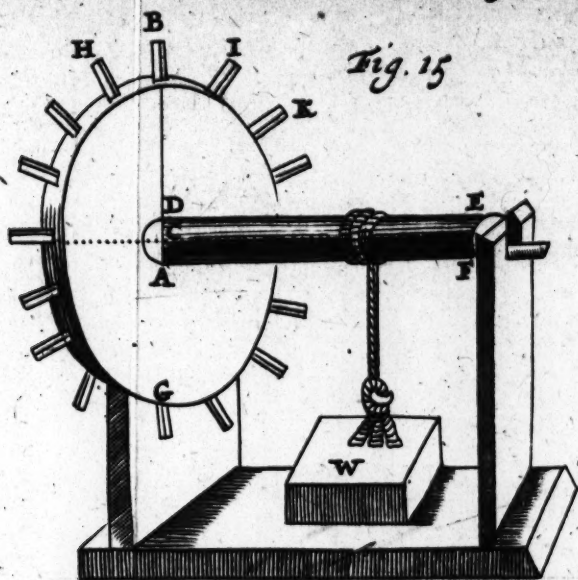


Fig. 16.

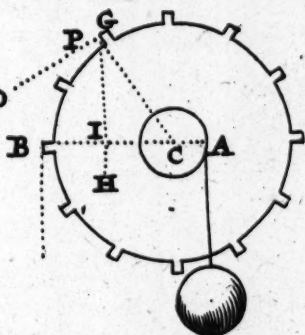
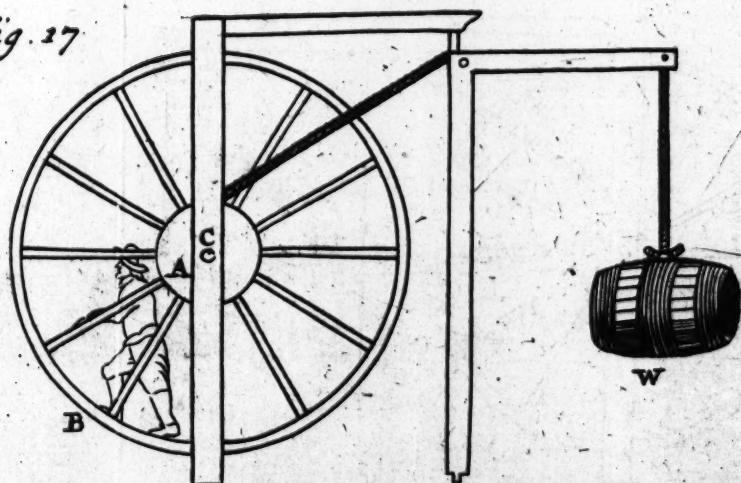


Fig. 17



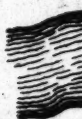


Fig. 18.

Mechan. Plate 4.

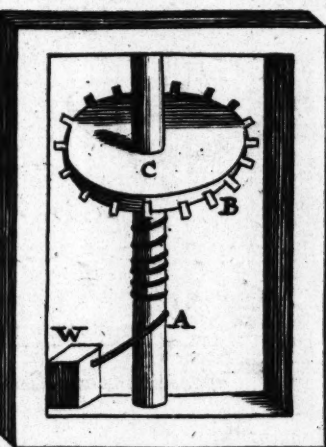
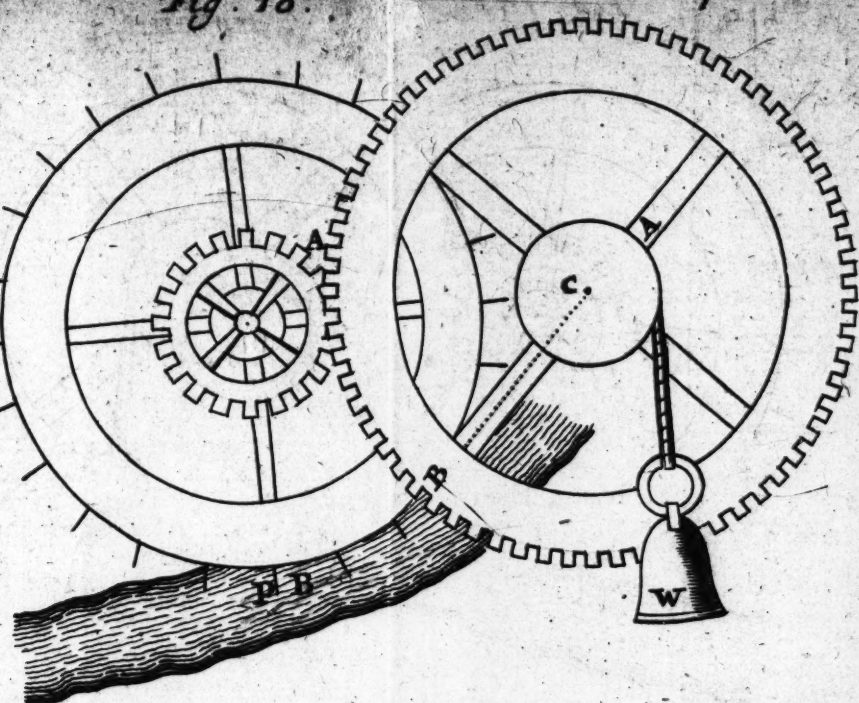


Fig. 19

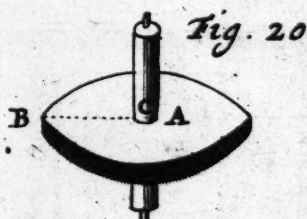


Fig. 20

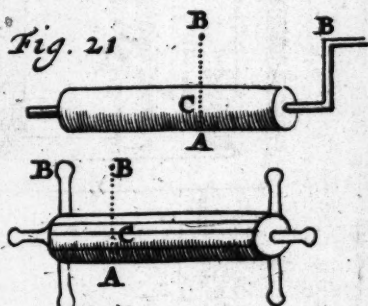


Fig. 21



Fig. 22

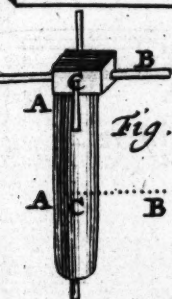


Fig. 23



Fig. 24

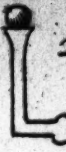


Fig. 2

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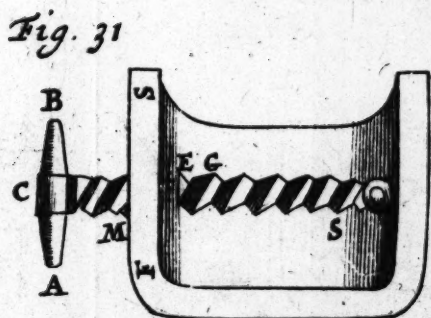
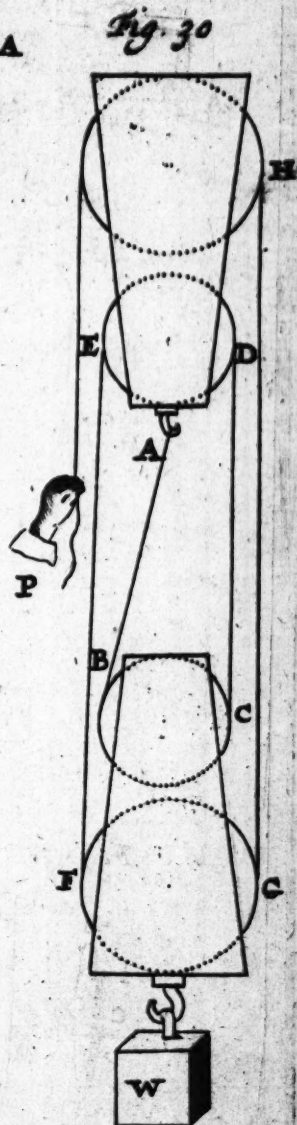
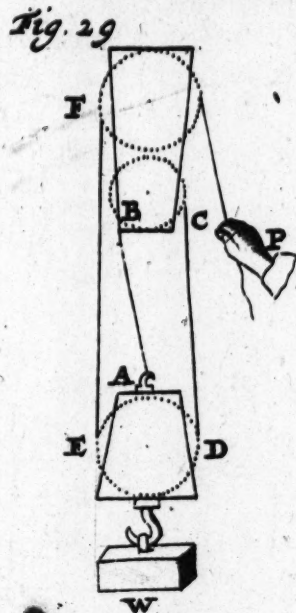
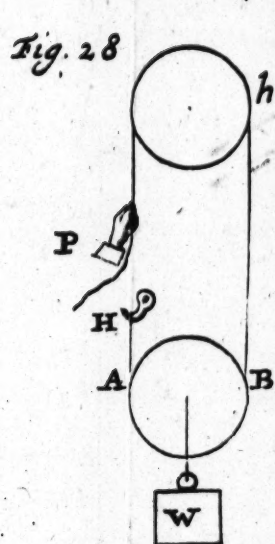
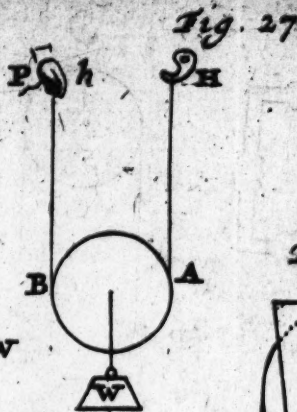
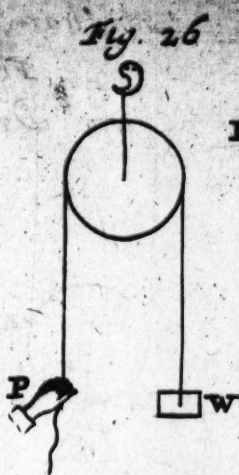
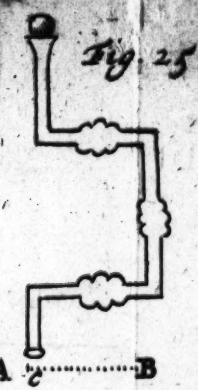


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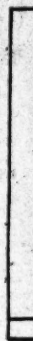


Fig. 3



Fig.



Fig. 32

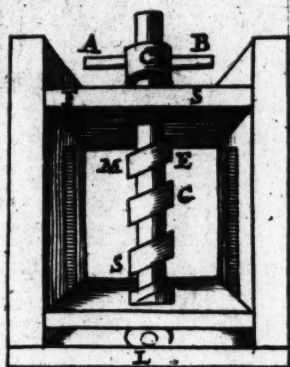


Fig. 33

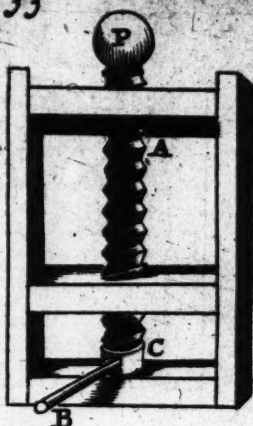


Fig. 34

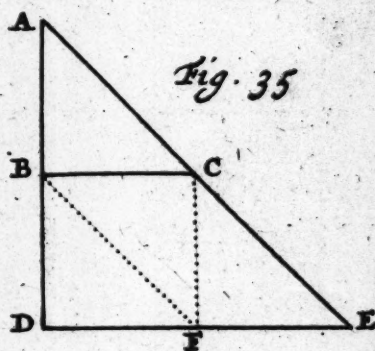
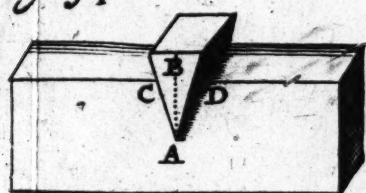


Fig. 36

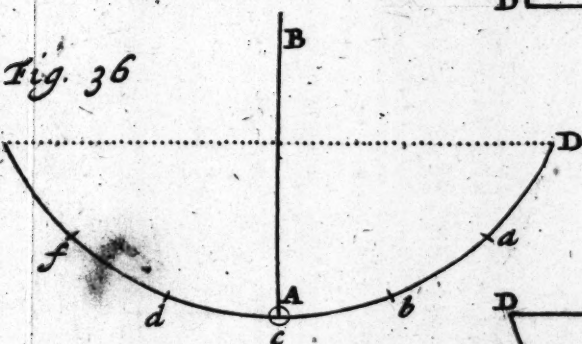
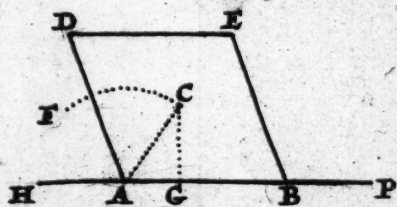


Fig. 37



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Fig. 38

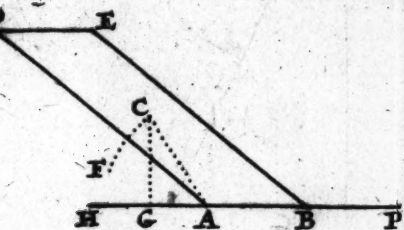


Fig. 39

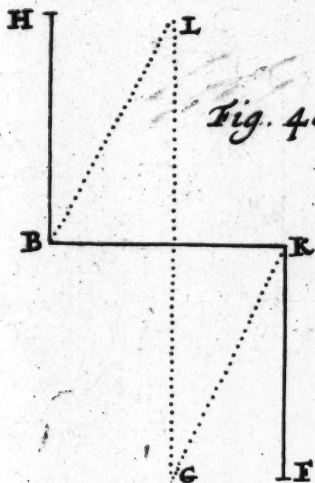
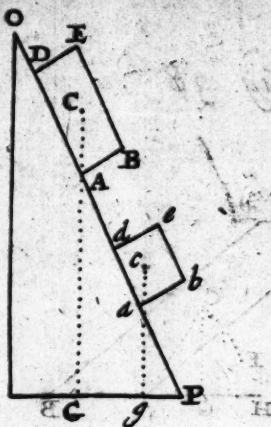


Fig. 40



Fig. 41

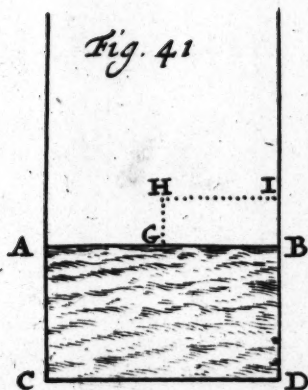
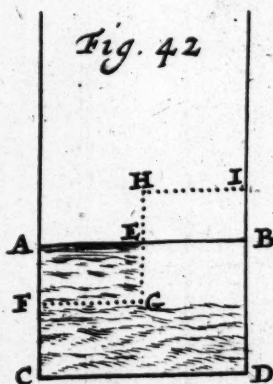


Fig. 42



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Fig



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Mechan. Plate 8.

Fig. 43

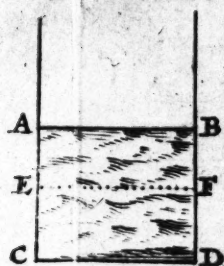


Fig. 44

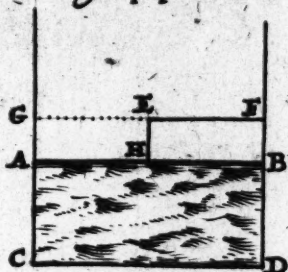


Fig. 45

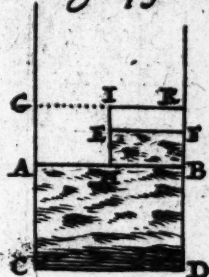


Fig. 46

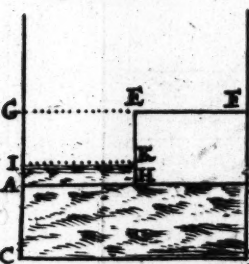


Fig. 47

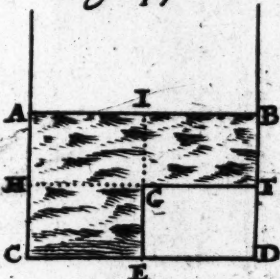


Fig. 48

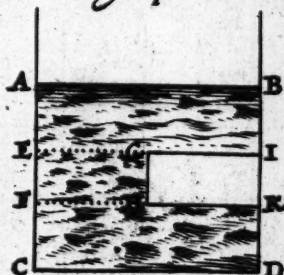


Fig. 49

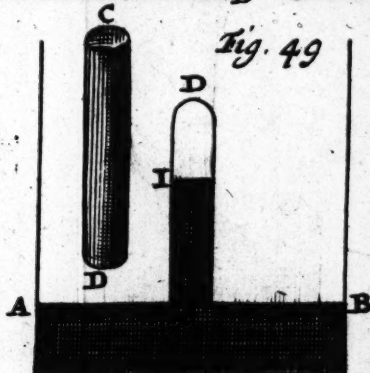


Fig. 50

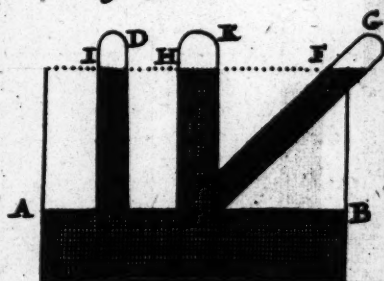


Fig. 51

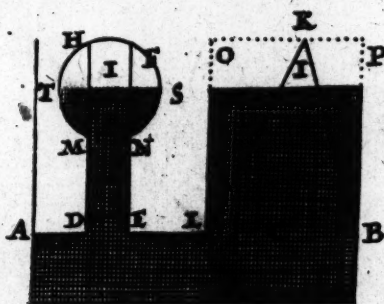


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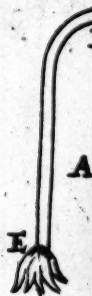


Fig. 52

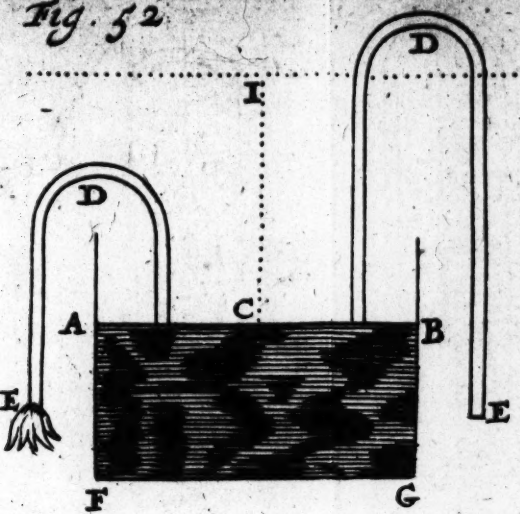
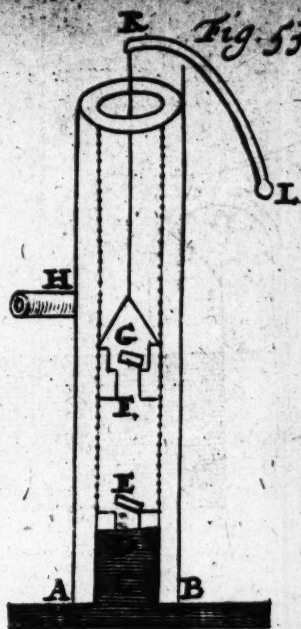


Fig. 53



THE
Young Gentleman's
OPTICKS:

CONTAINING
The more Useful and Easy
ELEMENTS of *Opticks*, more
properly so called, of *Catoptricks*,
Dioptricks, and *Perspective*.

EDWARD WELLS, D.D.
Rector of *Cotesbach* in *Leicester-*
shire.



L O N D O N,
Printed for *James Knapton*, at the *Crown*
in *St. Paul's Church-Yard*. 1713.

[Faint, illegible text, possibly bleed-through from the reverse side of the page.]

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THE PREFACE.

S Vision or Sight is the most useful and pleasant Sensation of the Body, so Spectacles must consequently be useful and pleasant, as not explaining the Manner of Vision in a Geometrical Way, also by the same Principles shewing how to supply or remedy the several Defects of Sight, by the Help of proper Instruments, such as Spectacles,

(F)

The Preface.

tacles, Microscopes, Telescopes, &c.

*Add hereto, that to this
ence is owing the Invention
several Instruments, which
to please and divert the
by curious and surprizing
rations ; such as are the
Chamber, the Magick-L
tern, &c. All which are
counted for in the follow
Treatise.*

THE
Young Gentleman's
OPTICKS.

CHAP. I.

Of Opticks in general.

THE Word *Opticks*, as it literally signifies in the Greek Tongue any Thing that relates to the Sight; so in its largest extension it is used by the Learned, to the whole Compass of Science or Knowledge (Physical as well as Mathematical) relating to Vision or Sight.

It is now agreed by the Learned, that it is caus'd by the Eye's receiving in Rays, which issue from the Object. These Rays, if they pass from the to the Eye through a Medium all

(F 2) along

1.
Opticks in general, what.

2.
Opticks properly so call'd, what.

along of the same Nature, diffuse
selves all along after the same Man-
ner right (because the shortest) Lines. W
this Sort of Vision is call'd *Direct*
and the Word *Opticks* is taken in a
restrain'd Sense, to denote that P
Opticks in general, which treats of
Vision.

3.
Catop-
tricks,
what.

If the Rays come not directly
the Objects to the Eye, but fall
on some impenetrable Body, and
thence reflected or beaten back
Eye, then the Vision is called *Re-
flection* ; and not the Object it self,
Image is seen. A rough Surface so
and scatters the Rays, that they
no Image at all, or at best but a v
perfect Image, of the Object ; and
fore those Bodies, which are cap
being most polish'd, or made most
make the best Reflexion. Such i
us'd therefore now-a-days for L
glasses ; but Glafs being of it se
cid or transparent, there is usuall
the Back-side of Looking-glasses,
silver to render it impenetrable
Rays. Before Looking-glasses
vented, the Ancients made use of
Metal ; and such a Piece of Met
use of to see one's self in, the G
led *κατοπτρον* ; and from thence
of Opticks in general, which

Vision, is distinguish'd by the
of *Catoptricks*.

the Rays of the visible Object pass
through different Mediums, so that they
more or less diffus'd in the one than
the other, then each Ray will be re-
fracted or broken in one Medium, from
a right Line wherein it diffus'd it self
in the other Medium; whence this is cal-
led *refracted Vision*. Thus a Ray passing
from Water into the Air appears refrac-
ted, i. e. broken or bent, from that right
Line made in the Water. And because
the knowledge of refracted Vision is most
useful in order to the making of Tele-
scopes, and such other Instruments; by
means of which, Objects are more
clearly seen; hence that Part of Opticks
generally, which treats of refracted Vi-
sion is distinguish'd by the Name of *Diop-
tricks*, *Διοπτρικὴ* being a Word capable of
signifying in the Greek Language any In-
strument made for to look through.

4.
Dioptricks
what.

the foremention'd Parts of Opticks
generally, may be added *Perspective*, or
that Part of representing visible Objects in
Picture, just as they appear to the
Eye. This Art is so call'd, because
the Picture is to be suppos'd between the
Eye and the Object, and transparent
so the Object may be seen through
the Word *perspicere* in the Latin
(F 3) Tongue

5.
*Perspec-
tive, what.*

Tongue signifying to see through a

I shall speak of each of the foregoing several Parts of Opticks, so is requisite to the Design of this Treatise; after that I have here adjoin *Definitions* or Explications of such Words, as are of principal Use in Opticks; as also such Theorems, as are agreeable both to the Principles of Geometry and Experience, and therefore us'd as Axioms in demonstrating the Theorems of this Treatise relating to Opticks and Dioptricks.

DEFINITIONS

1. *A Radiant* is whatever sends Rays from its several Points. Here I shall only take for the Object, suppose a Candle called the Radiant; but also its Image, suppose the Image of a Candle seen in a Glass, is call'd so likewise. As also the Image of an Image, and so on. Where note, that for Distinction's sake the Object is usually specify'd by the Name of the *prime* (or *primary*) Radiant. And so the immediate Image of the Object may be distinguish'd by the Name of a *second* Radiant; the Image of the Image, by the Name of the *third* Radiant, and so on; that which is seen by the Eye being always distinguish'd

there are many Images) by the
of the *last* Radiant.

Parallel Rays are such, as keep all
at an equal Distance one from the

Diverging Rays are such, as being
moved both Ways, concur or meet in
Point that Way, which is contrary
to their Motion. Thus *Fig. 10*, the Rays
AD, AB, and AF, which are suppos'd to
come from A, are diverging Rays.

Converging Rays are such, as being
moved both Ways, concur the same
Point they move. Thus *Fig. 10*, the Rays
ED, OB, and HF, which are conceiv'd
to move toward a, are converging Rays.

B. Parallelism, Divergency, and
Convergency are to be understood of Rays
in the same Point.

The *Focus* is that Point, where the
Rays of the same Point being produced
meet. Thus *Fig. 10*, A is the Focus of
diverging Rays AD, AB, and AF;
a is the Focus of the converging
Rays ED, OB, and HF. Whence it is
manifest, that the Focus of parallel Rays
is conceiv'd to be at an *infinite* Di-
stance, i. e. at so great a Distance, as that
Rays of the same Point, though they
strictly diverging or converging, yet
do not converge so very little, (at
least in respect of that Length and Porti-

on of them, wherein they are consid-
as that they may be look'd upon a
rallet.

6. The *Angle of Incidence* is nat-
and so properly the Angle ABC (F
comprehended between the incident
AB and the Surface BC which it (i
or) falls upon. But the Angle AB
ing always the Complement of th
gle ABP to a Right; and because
is to be prov'd of the Angle ABC
be primarily, and so more easily p
of the Angle ABP, hence for Con-
cy sake Writers of Opticks do
take ABP for the Angle of Inci
and agreeably define it to be the
comprehended under the incident
AB, and a right Line PB perpend
to B the Point of Incidence. Agr
also hereto,

7. A *Reflex Angle* is that, wh
comprehended under the reflex B
and the foresaid Perpendicular P
the Angle EBP Fig. 8: Though
properly or naturally EBG be the
of Reflexion.

8. A *Refracted Angle* is that, w
comprehended under the refract
BG and the Perpendicular KF
(Fig. 28.) viz. the Angle GBF.

By *Inflexion*, as a general Word, is
 ed either Reflection or Refraction.
 consequently both the reflecting Sur-
 BC (Fig. 8) and the refracting Sur-
 BD (Fig. 28) are stiled inflecting
 res. And both a reflected Ray BE
 8) and a refracted Ray BG (Fig. 28)
 mprehended under the Name of in-
 Rays.

A X I O M S.

A Ray of Light falling perpendicu-
 on an inflecting Surface, either goes
 in a right Line, or is reflected in-
 self. Thus (Fig. 8.) the Ray AC
 be conceiv'd as reflected by the re-
 Surface BC into it self. And the
 AD (Fig. 28) is to be conceiv'd to
 forward beyond the refringent Sur-
 in a right Line DE or DN.

The Inflexion of any Ray is per-
 in a Surface perpendicular to the
 ing Surface. Thus (Fig. 8.) the Ray
 reflected into BE in the Surface
 perpendicular to the reflecting Sur-
 C. And likewise (Fig. 28) the Ray
 is refracted into BG in the Sur-
 BGND perpendicular to the re-
 Surface BD. And note, that
 id Surface wherein any Ray is in-
 flected,

The Young Gentleman's
 flected, is thence stil'd the *Plane*
section.

CHAP. II.

Of Opticks properly so call'd
Direct Vision.

THEOREM I.

Fig. 1.

THE Eye is always placed
 Center of its own Sphere
 sion.

Demonstration. At what Distance
 ever, suppose Oa , the Eye O can
 Way, it is self-evident, that the
 Eye, if by no means hinder'd, can
 the same Distance any other Way
 towards b it can see at the Distance
 towards c at the Distance Oc ,
 quite round. Wherefore the several
 stances Oa , Ob , Oc , &c. being equal
 to the other, and all proceeding from
 same Point O , it follows that the
 the Rays of a Circle, whose Center
 and Circumference $abcdefgh$. Whence
 so it follows, that the said right Lines
 Ob , Oc , &c. are the Rays likewise

generated by the Turning of the
 mention'd Circle round about any
 Diameters, suppose ae , as an Ax-
 and consequently that O the Eye
 be the Center of the said Sphere. Q .

Prop. 1. As it is evident from what has
 said, that could the Eye be placed
 it might see every Way, the Space,
 which would then fall within its Sight,
 would represent an entire Sphere; so it
 follows, that by the Interposition of the
 Earth, the Space or Compass of actual
 Vision, even when the Eye has a full
 Field, is equal but to an Hemisphere.
 Now, supposing ae to represent the up-
 per surface of the Earth whereon the Eye
 stands, the Extent of actual Vision will
 be equal to the Hemisphere $Oabcde$, the
 EF denoting the Horizon or the
 Boundary of the Sight downwards.

Prop. 2. From this Theorem it follows
 that whatever Portion of the Hea-
 ven (whether All $abcde$, or only Part
 as bd , or bc , &c.) is seen by us, it
 appears as a Portion of the concave Sur-
 face of a Sphere.

Prop. 3. Because the Sun and Moon
 and Stars are beyond the Extent of di-
 rect Vision, and consequently the Eye
 discerns, how far one is more distant
 than the other; hence it comes to
 pass,

pass, that the Sun, Moon, and
do appear to us, as all situated in
Surface *aceg* of one and the same S
O*aceg*, and so equally distant fro
though they are in reality at sever
stances from us.

Corol. 4. So much of the Heaven
seen by us, *viz. abcde*, appearing
Spherical Figure only for the R
contain'd in this Theorem; it then
lows, that the Body of the H
may be of a Quadrilateral Figu
ABCD, or of any besides a S
cal.

Scholium. This first Theorem w
Corollaries is of good Use to
young Students for Astronomy.
have chosen to place this Theorem
direct Vision, partly because it w
the more easily understood, and
because, (though it be not one
geneous Matter contain'd in the R
or Space which we call Heaven, a
sequently what we see therein
considerable Distance, we see not
rect, but refracted Vision, yet) i
to the same in respect as to the C
fore us, whether Things in the
are visible to us by direct or refra
sion.

THEOREM II.

The Eye can see at one View (at Fig. 2.

Time and Place) no more Objects,

whose Rays fall within the Com-

pass of a Semicircle, to which the Eye,

with its Pupil, is the Center.

For the Eye can see only

Objects, whose Rays, passing thro'

Pupil, reach to its Retina or Optick

placed at the Bottom of the Eye.

Now it is evident from the bare In-

formation of Fig. 2. that no Ray can en-

ter Pupil O, but what falls within

semicircle DHE, whose Center is O.

Supposing a Ray to pass along ED

Diameter of the Semicircle, it will

pass over the Pupil O, and not enter it.

Consequently all Rays falling with-

in the said Semicircle, will much less

enter the Pupil. Q. E. D.

Now Rays of Light (as well as other

things, whether natural or artificial) ha-

ve a greater or less Force, as they are

more oblique, it follows that such

as pass through the very Middle of

semicircle DHE, are of most Efficacy

in Vision, as entering the Pupil of

the Eye perpendicularly, and consequent-

ly falling perpendicularly upon the Reti-

na at the Bottom of the Eye. Thus

the

the Image of the Object A will be painted most lively and distinct on the Retina. The Image *b* and the Objects B and G will be painted lively and distinct than the former, as being made by oblique Rays, alike lively and distinct in respect of another, as being made by the Rays *b* and G, equally oblique: and more lively and distinct than the Images *c* and *d* of the Objects C and F, because the Rays *b* and G are less oblique than the Rays *c* and F.

Schol. Agreeably hereto we find by Experience, that we see most distinctly such Objects, as (*ceteris paribus*) are placed directly before our Eyes. And upon Account it is, that, in all the Parts of Opticks largely so called, the principal Regard is to be had to such Rays as enter the Eye perpendicularly.

THEOREM III.

Fig. 3.

An Object appears greater or less according as it is seen under a greater or less Angle.

Demonst. Let the Lines AB and CD be of equal Length, so that they are of equal Bigness. Let the two Objects of equal Bigness. It is evident that the Angle AOB, under which is seen the Object AB, is only a part of the Angle COD, under which is

CD. It is also evident, that the
AO and BO being extended be-
yond O the Pupil of the Eye ODC
fall respectively upon the Points
c and d of the Retina in the Bot-
tom of the Eye; and likewise the Rays
DO being extended beyond O,
fall upon the Points e and f of the

Whence it follows, that *ab* the
of the Object AB will be so much
proportion less than the Image *cd* of
Object CD, that is, the Object AB
appear to a Spectator so much less
than the Object CD, (though they be
of an equal Bigness in reality,) as the
Angle AOB is less than the Angle COD.

Hence it appears, why the Dis- *Fig. 4.*
tance between the same two Objects A
and B appears to be greater or less, ac-
cording as the Distance of the Spectator
from the said Objects is greater or less;
because the Distance AB between
the two Objects is seen under an An-
gle proportionably greater or less, as the
Distance of the Eye from the said Objects
is greater or less; that is, the Angle
AOB is proportionably greater than the
Angle COD, as the Distance OD is less
than the Distance ED. And consequent-
ly to this *Theorem III.* the
Object AB will appear so much in pro-
portion

position greater to a Spectator at O
at E. *Explanatio* *quod* *habetur* *in* *Fig. 5.*

THEOREM IV.

Fig. 5.

The Rays of an Object being ad
through a narrow Hole; do there
one the other, so as that the Image
by the said cross Rays will be inv
respect of its Object.

Demonst. The Ray *Aa* proceeding
the Point *A* of the Object or Arrow
being (in direct Vision) a right
and so likewise the Ray *Bb*, the
cross one the other, being exten
yond the Hole *O*. And there
upper Point *A* of the Arrow *AB*
come the lower Point *a* of the Im
and the lower Point *B* of the Ar
will become the upper Point *b* of
ab. And the like will hold as to all
mediate Points, (except the very
Point *C*, which being perpendicu
a right Line with *O*, its Image *c*
wise be the middle Point of the
ab) and consequently the Image
be inverted in respect of its Ob
Q. E. D.

Schol. 1. Agreeable hereto a
ments of this Nature. Namely,
being darken'd by putting to
Window-shuts, and a small H
made with a common Gimblet

in one of the Window-shuts, and
Glas of the Window being remo-
ved from before the Hole by open-
ing the Casement or the like; such
as are without, and so situated
that their Rays will pass through
the Hole, will appear upon a Sheet of
Paper, held on the Inside overa-
gging the Hole, in an inverted Manner
according to this Theorem. And the
less the Paper is held to the Hole, so
less will the Image be; because as
less as the Rays Aa and Bb are ex-
tended beyond O the Hole or Point of
Meeting, so much less is the Dis-
tance between them: Namely, the Dis-
tance ab is less than the Distance cd , and
consequently the Image of the Object
(the Arrow) AB will appear less
on Paper held at the Distance cd from
the Hole, than if the Paper be held at the
Distance ab .

And the same has been found, by
Experiments made for this Purpose, to
be good in respect of the Eye it self,
being as it were a small dark Cham-
ber into which are let pass through the
Hole the Rays of outward Objects,
which paint their Images on the Retina in
the bottom of the Eye, agreeably to this
Theorem, that is, in an inverted Man-
ner in respect to its Object. As is il-

(G)

lustrated

illustrated Fig. 6, which represents having on its hinder Part a little Piece of each of its Coats or Skins cut away, so that you come to the vitreous Humour. A Candle being held before the Eye, and a Piece of white Paper being applied to the hinder Part prepared as aforesaid, the Image of the Candle has been found to be made on the said Paper in an inverted Manner; All other Rays being kept from falling on the Paper, so as to darken the Room where the Experiment was made. Concerning which more shall be said in Chapter IV, for as the Rays passing through the Crystalline of the Eye are refracted, and consequently it is requisite to understand the Cause of Refraction, before we can understand how Vision is caus'd in the Eye. And for the same Reason I omit saying any thing of the Use of Glasses in the Eye to a dark Room, for rendering the Images more clear and distinct.

3. I shall add here (as being necessary for the clearer Understanding of the Use of the Eye has been or shall be said in this Chapter of Opticks) a Description of the several Parts of an Eye, represented in the Figure, where A denotes the *Crystalline*, B the *Vitreous*, C the *Aqueous*, D the *Cornea Tunica*; E the *Retina*.

call'd *Choroidea*; G the Coat call'd
Vitrea, being a Part of the *Dura Mater*
 lined about the Ball of the Eye on its
 Part; H the Optick Nerve without
 Ball of the Eye; I the Coat or Skin
 the *Vitrea*; K the Hole of the U.
 call'd in one Word the *Pupil*.
 remains only to observe further, that
 if not all the Particulars taken no-
 of in this Chapter, belong not to di-
 vision alone, but are applicable also
 to direct and refracted Vision; which
 we proceed to speak of in their Order.

CHAP. III.

Catoptricks, or Reflex Vision.

THEOREM I.

Let Ray AB of Light be reflected by a Fig. 8||
 Surface GC, the Angle PBE of
 Vision will be equal to the Angle PBA
 Hence.

Const. Draw BP, and also AC, per-
 pendicular to GC. The Medium GC do
 suppos'd homogeneous to (i. e. of
 the same Nature with) the Medium
 EBCD,

(G 2)

EBCD, it follows that all the Rays
 prehended between AB and AC
 which take up or spread all over the
 Line BC, were they not hinder'd
 the reflecting Plane) from passing
 the Medium GCde, would therein
 themselves after the same Manner,
 the other Medium EBCD, that is
 right Line AB being continued to
 AC to *d*,) at the Distance Be they
 diffuse or spread themselves all o
 And whereas the reflecting Plane B
 neither increase nor diminish the
 ing of the Rays, but only turn
 back into the same Medium they
 afore; hence it is obvious, that a
 Reflection the Rays will spread
 selves in the same Manner, as they
 have spread, had they not fell up
 Surface GC, but (that being re
 gone on in the same homogeneous
 um. But in that Case, at the D
 Be, the Rays would (as is afore
 spread themselves all over *ed*.
 fore in the Distance $BE = Be$, th
 spread themselves all over $DE = D$
 consequently the Figure BCDE wi
 all Respects like and equal to the
 BCde; and indeed is no other t
 Figure BCde reflected, or turn'd a
 it were) half round upon BC.
 fore, if from the equal Angles E

there be taken away the right Angles
and $\angle PBC$, there will remain the An-
 $\angle BP$ and $\angle Bp$ equal one to the other.
 $\angle BP = \angle Bp$, therefore $\angle ABP = \angle EBP$.

D.

1. Hence the Angles $\angle EBG$ and
(which, as has been *Defin.* 6 and 7
d, are more properly call'd the
of Incidence and Reflection) are
one to the other. Namely, be-
 $\angle PBG = \angle PBC$, and $\angle PBE = \angle PBA$.
ore $(\angle PBG - \angle PBE) = \angle EBG = (\angle PBC$
 $=) \angle ABC$.

2. If the reflex Ray BE be taken
Incident, then the incident Ray
will be its Reflex.

3. If the Angle $\angle PBE = \angle PBA$, or
 $\angle CBA$, then BE is the Reflex of

What has been prov'd as to a *Fig. 9.*
Plane GC , the same holds good
respect of any reflecting *Curve* Sur-
face. For the Inclination or Directi-
on of the Curve, at B the Point of In-
cidence, is the same with the Inclination
of the Plane DE that touches it there.
Therefore the Reflection following
the Inclination, will be the same,
if it be suppos'd to be made by B
Particle of the Curve Surface PBQ ,
the Plain DBE . And the same
good as to refracting Surfaces.

(G 3)

THEQ-

THEOREM II.

Fig. 10.

At what Distance CA an Object placed before a reflecting Plane CF (whether of Metal or Glass, &c.) at the same Distance Ca will the Image of the Object appear behind the said reflecting Plane, each Distance CA and Ca being measur'd upon one and the same perpendicular to the said Plane, viz. Aa .

Demonst. Let AD , AB , and AO be Rays proceeding from the Object (any Point of the Object) A ; and let BO , and FH be their respective reflected Rays. It is evident, that these being extended beyond CF (*i. e.* behind the reflecting Plane) will all meet in a , therefore will be the Focus of the Rays, and consequently the Place where the Image of A will appear. But the Angle $aDC = EDF$, and $EDF = ADC$ by *Theorem I.* of this Chapter; therefore $aDC = ADC$. And because Triangles ACD and aCD , the Angle $ADC = aDC$, and also $ACD = aCD$, the Side CD is common to both Triangles, therefore $CA = Ca$. And in the very same Manner may it be proved that in the other Triangles, ACB , as also ACF and aCF , &c.

CA of (any Point in the Object,
consequently of all) the Object
equal to the Distance C_e of the Image
E. D.

1. Hence it follows, that suppo-
se reflex Ray OB to be that which
goes to the Eye plac'd at O, though all
of the Looking-glass or other re-
flecting Plane, CF be cover'd (or taken
away) but the Part B, yet the Image a
is seen by the Eye; whereas if the
Part B be hid, and all the rest uncover'd,
the Image can't be seen by the Eye.

2. After the same Manner as Ob-
jects inclin'd towards the reflecting
Plane, will also their Images be inclin'd.
consequently in such a Plane or
Looking-glass plac'd horizontally, Objects
appear inverted, or with their upper
ends downward.

3. Because $CB = AB$, therefore
 $CB + BO$, that is, the Distance of
the Image from the Eye is equal to the

namely, as the visible Object is conceiv'd to con-
sist of several Radiant Points, so the Image of the whole
is made up of all the Images of the several Radi-
ant Points taken together; as is more fully illustrated
in the next Proposition, and 12, of which see more in the following

(G 4)

inci-

incident Ray and reflected Ray together.

Cor. 4. Whatever has been for the Image of any Object or point, the same holds true also for the Image of an Image. Whence the multiplying of Images by two or more reflecting Planes deduced. Wherein this is most remarkable the Distance of every Image is equal to the Ray propagated from the point to the Eye, through all the mediate Reflexions.

Schol. 1. It is observable, that by the Theorem, the Focus A of Rays AB, and AF falling on the reflecting Plane CF being given, thereby to find the Focus *a* after Reflection; namely, by drawing AC perpendicular to the Plane, and extending it to *a* so, as that CA be equal to CA. For then *a* will be the Focus sought.

Schol. 2. For the Sake of such as do not so readily apprehend from the Figure how the Image of a whole Object is formed by Reflection, I have therefore added 11 and 12. In each of which 11 notes a Cross, and *ab* its Image formed by the incident Rays reflected to the Eye by the reflecting Plane CF. Name 11 shews expressly, how the Ray

that come from the two Extremities of the Object are reflected to the Eye and so cause the Image of A and B to appear at *a* and *b*; and Fig. 12 shews in like Manner the Images of the Extremities D and H of the Object appear at *d* and *h*; namely, in both Figures the Images appear, where the reflex Rays EG and FH being extended, meet with the perpendiculars Aa, Bb, Hh, and Dd; and $Ca=CA$, $Fb=FB$, $Ch=CH$, and $Hd=HD$. And the same may be shewn of any other Points.

THEOREM III.

If an Object be reflected in a reflecting Glass (or other Surface) Fig. 12.

which is spherical, either concave or convex, and the Object E be far distant from the Glass; its Image will, to the Eye placed in the Axis AB of Radiation, appear at C the Middle of the Semidiameter AB of the Glass. But if the Object

be not far distant, then its Image Fig. 14, 15, 16.

to the Eye in the Axis, appear at Place C, where $(BC : CA :: BE : CE)$ that is, where) the Distance of the Image from B the Vertex of the Glass will be as its Distance from A the Center of the Glass, as the Distance of the Object from the said Vertex is to its Distance from the said Center.

I have chosen to comprehend all relates to reflecting spherical Glasses, respect to the Eye placed in the Axis of Radiation, under one Theorem, thereby may the more easily be discov'ed in the uniform Manner, whereby Vision is perform'd in such Cases.

In reference to which it is to be observ'd, that (although in the Figure belonging to this Theorem, the Point D is placed at some considerable Distance from B, for the more distinctly perceiving the Demonstrations, yet) D is to be suppos'd very near to B, because otherwise the reflex CD of the Incident Ray ED will not affect the Eye placed in AB. For the reflex Rays of all such Rays as fall upon the Glass remote from B, will pass by on one side of the Pupil of the Eye, and so contribute nothing to the Sight of the Object. Add hereto, what has been observed in the Corollary of Theorem 2, Chap. 1. Hence Notice is here taken only of those Rays as fall upon the Glass very near to its Vertex B. These Particulars premis'd, I come now to the Demonstration of this Theorem, in respect to four principal Cases following.

Fig. 13.

Case 1. When the Object is far off from the Glass, so that the Rays coming from any one Point thereof may be receiv'd parallel one to the other, and

the Axis AB, as the Ray ED, is in
 Case the Image will appear, to the
 need somewhere in the Axis, at C
 middle of the Semidiameter of the
 For bisect AB in C, and draw
 CD, and produce them on the
 Side of BD the Glass. Because
 point D is look'd to be so very
 to B, as in a Manner to coin-
 with it, therefore we may also
 upon $CD = CB$; and by Construc-
 $CA = CB$, therefore $CA = CD$, and
 hence the Angle $CAD = CDA$. But
 Angle $CAD = EDA$ the Angle of Inci-
 of the Ray ED, (for AD is perpen-
 to the Surface of the spherical
 wherefore the Angle CDA is e-
 the Angle of Incidence of ED,
 wherefore (by Cor. 2, Theorem I Chap.
 C is the Reflex of the Incident ED
 the Concave Surface of the Glass
 And the like may be demonstrated
 the Convex Surface of the Glass
 for, because the Angle $EDA = EDO$,
 $EDA = NDO$, therefore the Line
 will be the Reflex of the Ray ED,
 being produced backwards (or on the
 ve Side of the Glass) will touch
 so at C. And what has been de-
 rated of any Ray ED taken at plea-
 the same holds true of all Rays in
 the Circumstances. Wherefore Rays
 parallel

parallel to AB, and whose reflex contribute to the Sight of the Image they fall upon a Concave Glass, their Reflexion will concur at C, from thence diverging again, will render the Image visible at C, to the Eye placed somewhere in AB. And the reflex of such parallel Rays, as fall upon a Convex Glass, do diverge from C, consequently render the Image visible at C, to the Eye plac'd in AB produced the convex Side of the Glass; that is, if CD be the incident parallel Ray, NE be the Convex, which will form the Image at C. (Q. E. D.)

Corol. Hence, and from *Corol.* 2. *rem.* 1. of this Chapter, it follows, Rays diverging from C and reflected by a Concave Surface, or converging and reflected by a Convex Surface parallel to AB; that is, if CD be the Incident, DE is the Reflex; or if DE be the Incident, DC is the Reflex.

Fig. 14.

Case 2. If the Object E be not distant from BD the Glass, and so the Rays proceeding from any single Point of the Object are (not parallel, but) diverging, the Image will, to the Eye in the same Place, appear at that Place C, where $BC : BE :: EA$. And this shall be demonstrated first in respect of Concave Glass, and when the Distance of the Ob-

than half the Semidiameter of the
 For let the Point C be so taken in
 as is requir'd; and draw AD and
 Because (for the Reason above-
 and) $ED = EB$, and $CD = CB$,
 ore by Construction $CD (=CB)$
 $: DE (=BE) : EA$. Wherefore al-
 ly $CD : DE :: CA : EA$. And so
 prop. 3. *Euclid*. 6.) the Angle ADE
 C But ADE is the Angle of In-
 of the Ray ED; therefore (by
 e. *Theorem* I. of this Chapter) DC
 Reflex of the Ray ED. And ED
 taken at Pleasure, it follows that
 focus of all other Rays diverging
 E will, after their Reflection by a
 e Glass, be at C, and consequent-
 Image of the Object will appear
 to the Eye placed in the Axis
 roduced, or) EB. Q. E. D.

1. Hence C will be the Focus of
 D converging to E in the like Cir-
 cles, and reflected by a spherical
 Reflector.

2. Hence and from *Cor. 2. Theo-*
of this Chapter, if CD be the Inci-
 DE will be the Reflex; and if ND
 Incident, De will be the Re-

3. And the same holds true, when *Fig. 13.*
 stance of the Object is less than
 Semidiameter of the Glass. For
 in

in AB extended, let C be taken
ing to the Prop. be requir'd;
AD and CD be drawn and pro
as also let ER be drawn parallel
The Arch BD being as Nothing
fore $ED = EB$, and $CD = CB$.
 $ED : EA :: CD : CA$; and so
son of DC being parallel to ER
 $EA :: ER : EA$. Wherefore ER
and the Angle $ERD = EDR$.
is the Angle of Incidence of E
 $ERD = NDA$ its Altern, there
Cor. 2. Theorem I. of this Chapter
is the Reflex of the Incident ED
ED being taken at pleasure, it is
that all Rays proceeding from E,
flected by a concave Glass, being
ed backwards, will concur in
consequently the Image of the Ob
appear at C, to the Eye placed in
is. Q. E. D.

Corol. 1. Hence if CD be the
on a spherical Convex Reflector,
be the Reflex, and so the Image
pear at E.

Cor. 2. Hence and from *Cor. 2.*
I. of this Chapter, if ND be the
DE will be the Reflex; and if
Incident, DC will be the Reflex

Fig. 16.

Case 4. The like holds good
of convex Glasses. For in AE
taken according to the Propo

in this *Theorem*, or (which comes the same) so as that $AC : CB :: AE :$
 and let CD be drawn and extended ;
 parallel thereto let ER be drawn,
 meets in R with AD produced. The
 BD being as Nothing, therefore
 CB , and $ED = EB$. And therefore
 $CD :: AE : ED$. But because the
 angles ACD and AER are equiangu-
 therefore $AC : CD :: AE : ER$; and
 $ED :: AE : ER$; and therefore
 ED . And consequently the Angle
 or its Altern, and so Equal)
 EDR the Angle of Incidence of
 Wherefore DN is the Reflex of the
 ent ED . But ED being taken at
 re, it is evident, that all the Rays
 ing from E , and entring the Eye
 in the Axis, after they are reflec-
 the convex Surface BD , will di-
 from the Focus C ; and conse-
 ly the Image of the Object E will
 at C to the Eye so placed. Q.

U. Hence if ND be the Incident,
 will be the Reflex; and if in a con-
 reflecter ED be the Incident, DC will
 Reflex; or if CD be the Incident,
 will be the Reflex.

From this Theorem is deduced
 of finding the Focus of paral-
 lel

lel or other Rays, falling upon
cal Surfaces, after their Reflection

The Focus C of such parallel
ED after Reflection is found by
ing the Semidiameter AB of the
in C.

And the Focus C of other Rays
upon a spherical Surface, is found
Reflexion, by taking C so, as the
 $AC : : BE : AE$.

And thus it has been shewn, by
Way of Theorem and Problem,
the Image of an Object will appear
ny spherical Glass, (or other like
ing Plane) to the Eye placed in the
of Radiation. And this is sufficient
our present Purpose, not only
most optical Instruments are made
this manner, but also because the
only in this Situation of the Eye,
so lively and distinct, as to deserve
Name of an Image. Hitherto both
and Image have been denoted only
gle Points, as being sufficient to illustrate
what has been afore deliver'd.
proceed to speak of Object and
consider'd as Lines or Surfaces.

THEOREM IV

Image CT of a radiant plain Surface, made by a spherical Glass BD, plain Surface.

Fig. 17
& 18.

Let A the Center of the Glass, draw perpendicular to FE, and meeting the Glass in its Vertex B. And (according to Prop. III, of this Chapter) let C be the Image of the Point E, through which draw parallel to FE the Plane CT. In the Plane CT will appear the Image of the Point FE made by the Glass.

Let AF be the Ray, drawn from the Point F of the radiant Plane to the Center of the Glass, and meeting the Glass in D, and the Plane CT in H. And by Construction let CD be the Reflex of the Incident ED; and BH be the Reflex of the Incident FB. Now, because the Ray FD in H. Now, because we suppose in the present Case the Angle AFE to be small, therefore the Angle DFE will be also small, and in effect less than a little or short right Line. The Circumference of the Circle described with the Diameter BE will pass through the Points D and E, because the Angles FEB and FDB are right. Whence the Angles BFD and BED being in the same Segment, are equal. And when the Points A are Verticals or the same,

(H)

it

it will follow that $FBA = EDA$. (because by *Theorem* I, of this $ABH = FBA$, and $ADC = EDA$, fore $ABH = EDC$. Whence the angles ABH and ADC are equal and so similar. Wherefore $AB : AD : AC$; and whereas $AB = AD$ fore $AH = AC$. But by reason of Smallness of the Angle CAT , look upon $AT = AC$, and there may also look on $AH = AT$. But Image of the Point F in the radiant whence the said Image is placed in the Plane CT . And the same may be the same Way as to the Image of other Point in the Plane FE . Whence the Image of the Plane FE is placed in the Plane CT . Q. E. D.

If the radiant Plane be far distant the Images of several radiant Points will be (by *Theorem* III, of this in the Mid-points of the several diameters of the Glafs tending to the radiant Points, that is, the Image of the radiant Plane far distant will have the form of a spherical Surface concentric to the Glafs. But because the said Radiant Plane according to our Supposition) seen under a small Angle, that small Portion of the spherical Surface, which is taken up by the Image, will scarcely differ from a plane Surface, to which AB is perpendicular.

the this Theorem holds good in all
for the Demonstration will serve
other Case, as well as those two
mentioned in *Fig. 17* and *18*.

If the Angle *EAF* be too great,
the Line *AH* will be sensibly less
T. Whence an Object being seen
such an Angle, its Image, if made
concave Glass, will appear concave;
by a convex Glass, will appear

THEOREM V.

Object *HF*, and its Image *bf*, are *Fig. 19*
under equal Angles *HBf* and *bBf* & 20.
The Vertex *B* of the reflecting Curve
whether convex (as *Fig. 19*) or con-
(*Fig. 20*.)

Draw *AE* perpendicular to
which by *Theorem IV*, of this Chap-
consequently be perpendicular to
meeting the reflecting Curve *BD*
Draw also *BF*, *BH*, *Bf*, *Bb*, and
the last will pass through the Cen-
forasmuch as according to our
on the Image of every Point is
the Axis of Radiation. In like
the Points *H*, *A*, and *b* will be
the Axis. Now by *Theorem III*,
Chapter. $BE : EA :: BC : CA$.
or $BE : BC :: EA : CA$. But (by
the equiangular Triangles *AEF*
 $EA : CA :: EF : Cf$. Where-
(H 2) fore

fore $BE : EF :: BC : Cf$ And
 the Angles BEF and BCf are right
 fore the Angle $EBF = CBf$. And
 Manner the Angle $EBH = CBb$. Wh
 $HBF = bBF$. Q. E. D.

Corol. The Object FH (if it be
 and its Image fb , are one to the
 their Distances from the Vertex,
 BC . But if the Object be a Surface
 its Image will be one to the other
 Squares of their Distances a
 Whence, the Distance of the O
 the Image from the Reflector bein
 thereby is given also the Ratio or
 on of the Image to the Object. An
 Manner may be found the last
 an Object, when it is propagated
 ny Reflecters. Lastly, it is
 that the same will hold true i
 spect, if fb be the Object, an
 Image.

Schol. By what has been said
 fie to account for and illustrate
 culars relating to Images made
 rical Reflecters. Of which the
 markable are these that follow

1. If the Reflector be conc
 the Distance BC of the Object
 the Vertex of the Reflector, b
 half the Semidiameter, then Its
 will appear beyond or behind
 ter, and in a right Position, (as

HF,

er, namely the upper Part of the
 will appear the upper Part of the
 the lower Part of that, the low-
 of this. &c.) and as the Object is
 nearer or farther from the Reflec-
 thin the Distance of the Semidia-
 So will the Image be nearer or far-
 from the same, and appear less or
 magnify'd. All which Particulars
 illustrated by comparing together
 and 21 and 22. Namely in *Fig.*
 Object *bf* being placed a fourth
 of the Semidiameter BA from
 ecting Concave BD, and in *Fig.*
 Object *bf* being placed a third
 of the Semidiameter BA from the
 concave Reflector, it is evident that
 former the Image HF (as well as
 ect *bf*) is nearer to the Reflector,
 proportionably, than in the lat-
 and in both Figures the Image ap-
 a due Position, viz. F is on the
 of the Axis AB as *f*, and H as
 therefore if *f* be the upper and
 lower Part of the Object, F will
 rise the upper, and H the lower
 the Image. Lastly, it is evident,
 both Figures *bf* and HF, i. e. the
 and its Image, are one to the other,
 Distances from the Vertex BC and
 in *Fig.* 19, $BC : BE :: 1 : 3 ::$
 And in *Fig.* 21. $BC : BE :: 1 :$
 HF, (H 3) 2. It

2. It is evident from comparing *Fig. 19* and *22*, that if the *ter* be convex, and so *HF* the and *hf* its Image, then likewise the will appear in its due Position; as the Object is brought nearer Reflector, so will the Image come. But in this a convex Reflector differs from a concave, *viz.* that (whereas in a concave, the nearer the Object *hf* is to the Vertex *B*, the less will the Image appear, as is evident from comparing *Fig. 19* and *21*, the contrary) in a convex, the nearer the Object *HF* is to *B* the Vertex, the more will the Image *hf* appear, as is evident from comparing *Fig. 19* and *22*. This is so remarkable, that be the Object moved never so far distant from the reflecting Convex beyond the half Semidiameter, yet its Image will fix it at the half Semidiameter.

3. If the Reflector be a Concave, and the Object *HF* be more distant from the Vertex than the length of the Semidiameter (as *Fig. 20* and *23*) then the Image *hf* will be more distant from it than the Semidiameter, and yet less than the whole diameter, that is, it will appear between the Object and the Reflector. Also it will appear in an inverted Position, that is, the Point *F* and its Image

on contrary Sides of AB the Axis, as the Point H and its Image h ; (and any other Point of the Object, and Image,) whence if F be the upper or Hand Part of the Object, f will be lower or left hand Part of the Image, Likewise it is evident from comparing 20 and 23, that in this Case, as Object HE is remov'd farther from reflecter, so its Image hf will come and appear less; and on the contrary as the Object comes nearer, the Image will go off farther, (and appear greater) till they meet one the other at Center A. In like Manner if fb be the lower or left hand Part of the Object, then HE will be the Image; and the Rays whereof are easie to be accounted for, from what has been said. It is also observable that if the Object HE be mov'd so far from the Reflector, as the Rays of it falling near the Vertex of the Reflector, may be esteem'd parallel to AB, then (according to the first part of *Theorem III*, of this Chapter) the Image hf will appear at the Mid point of the Semidiameter of the Reflector. If the Sun be the said far distant Object, then the Place of the Image (or Point of the Semidiameter) will be the turning-point of the Reflector, if it be sensibly larger, than the Image of the Sun. But if a lucid Body, as a Candle,

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be plac'd in the said Mid-point Semidiameter, it will cast a Light great Distance. Add as in this Case, but Light will appear on the face of the Reflector; so when other objects are placed at the half Semidiameter nothing but their Colour will appear on the Surface of the concave Reflector.

4. It is observable, that suppos'd an Object to stand still, and the Reflector change its Place, the same Alteration will be produc'd in respect to the Image as if the Object had chang'd its Place in a correspondent Manner.

5. It is evident from Fig. 19— that a reflecting Concave magnifies an Object, a reflecting Convex lessens an Object. Namely, if in the said Figures BDC be consider'd as a Concave, then *bf* will be the Object, and *HF* the Image, which in all the said Figures much larger than *bf* the Object. But if *DBC* be consider'd as a Convex, then *HF* will be the Object, and *bf* the Image, which in the said Figures much less than *HF* the Object.

6. It is observable, that cylindrical Reflectors, whether concave or convex, will render the Image deform'd. For a Cylinder being generated by the Motion of a right Line round two parallel Lines, hence such a Reflector must partake of the Properties of a plain Re-

of a Spherical. Of that, in re-
spect of its right Lines, in Longitude; of
in respect of its circular Lines,
and ways. Hence the Longitude or
height of an Object being represented
as by a reflecting plain Surface; but
altitude magnify'd or diminished, ac-
cording as the Reflector is a Concave, or
Convex; the Image appears disproportion-
able. But on the same Account, if a
Picture be drawn proportionably bigger
in breadth than in Length, its Image will
be represented by a reflecting Cylinder in
all Dimensions. Which is illustrated
in Figs. 24, 25, 26. Namely, in *Fig. 24*, is
the Picture in its just Dimensi-
ons, and divided into Parallelograms;
in *Fig. 25* are drawn as many circular
Lines as there are (in *Fig. 24*) horizon-
tal Lines parallel one to the other, viz.
all the said circular Lines being con-
tained to the circular Basis of the Cy-
linder; and distinguish'd proportiona-
ly by right Lines drawn a-cross them in
many Divisions, as the Picture (*Fig.*
24) is divided into Parallelograms: So
the Image of the Picture, as is contain'd in each
Parallelogram being to be drawn in each
of the foremention'd Divisions answering
thereto. Which being done, and the
reflecting Cylinder being plac'd on *C*, the
Image of the Picture will appear in the
said

said Cylinder according to its just Dimensions, but less than the Picture, if the reflecting Cylinder be convex; which is generally us'd in this Case, and is represented Fig. 26.

Lastly, It remains only to observe, by the foregoing Theorems may be found such a Position of the Radiant, as the said Radiant may have a given proportion to its Image made by the Reflector. For Instance, let BD (Fig. 2) be the Reflector, and the given Proportion be that of BA to AM. If the Object be a Line, bisect BM in E, and by Theorem III, of this Chapter find the Focus answering to the Focus E, which will be the Place of the Radiant. For $BC : CA :: BE : EA$; therefore $BC + CA :: BE + EA$; that is, because $BE = EM$, $BC : BA :: BE : BA$, and therefore $BC : BE :: BA : AM$ by the Corollary of this Theorem V. to BE, as the radiant Line in C to its Image in E; therefore the Radiant in C, is to its Image made by BD as BA to AM, is a. In the Proposition. If the Radiant be a Surface instead of AM, a right Line must be found to which BA has a subduplicate Ratio that which it has to AM. And this is sufficient to our Design, concerning toptricks or reflex Vision.

C H A P. IV.

Of Dioptricks, or Refracted

Vision.

T H E O R E M I.

A Ray AB of Light be refracted by *Fig. 28,*
 the plain Surface BD of a Medium of *29.*
 different Thickness, the right Sine of ABK
 Angle of Incidence will, in respect of
 same different Mediums, always have
 same (Ratio or) Proportion to the
 Sine of GBF the Angle of Refrac-
 tion; however the Ray AB be inclin'd to
 Surface BD.

Demons't. Let BG be the Refract of the
 AB, whether AB passes out of a
 thinner Medium into a thicker, (as *Fig.*
Fig. 29.) Now as the Light proceed-
 from A, and contain'd between AB
 AD, will be diffus'd within the Me-
 dium DK all over BD; so after it has en-
 tered the new Medium DG, it will at the
 point of BG diffuse it self all over GN:
 as if it had the same Medium DK been
 con-

continued on each Side of BD, the Length of BC ($=BG$) would have been diffus'd all over CE. But in both Cases (namely, whether the Medium DG different from or the same with the Medium DK) $FN=ME$, and consequently both the said Lines may be look'd upon as not at all depending on the (*) Facilities of the Medium's, and so of no Consideration in the present Case. Where GF (i. e. $GN-FN$) and CM (i. e. $—ME$) are to be look'd on, as the genuine Effects of the Facilities of the two Mediums DG and (DC, or which is the same) DK; that is, GF is to CM , as the Facility of the Medium DG is to the Facility of the Medium DC or DK. CM is the right Sine of the Angle ($CBM=$) ABK , which is the Angle of Incidence of the Ray AB; and according to the same Semidiameter, GF is the right Sine of GBF the Angle of Reflection of the same Ray AB. Where since the Angle DAB ($=ABK$) is at pleasure, the like will hold good in any other Angle; that is, in the Reflection of any Ray AB, let it fall how it will on the Plain whereby it is refracted, the Sine of the Angle of Incidence

(*) This Word is us'd to denote the several Facilities which different Mediums have to diffuse the Light.

Sine of the Angle of Refraction, as Facility of the Medium DK is to Facility of the Medium DG, whereby Ray AB is refracted into BG. But in all of the same Mediums, the Thicknesses of the Mediums, and the Facilities are arising, and their Ratio will abide the same. Wherefore in the Refraction of any Ray, the Sine of the Angle of Incidence always keeps, with respect to the Mediums, the same Ratio or Proportion to the Sine of the Angle of Refraction. Q. E. D.

Schol. 1. If BG be the refracted Ray of Incident AB, the rest remaining the same, BA will be the refracted Ray of the Incident GB.

Schol. 2. The refracted Ray BG of any Incident AB is rightly assign'd, when the Sine CM (of the Angle CBM =) ABK the Sine of Incidence, is to the Sine GF of the Angle GBF contain'd under the assign'd Ray BG, and the right Line BM perpendicular to the refracting Surface as the Facilities of the given Mediums are one to the other. Namely, this Proposition is no other than the Converse of this first Theorem.

Schol. 1. In a Ray's passing out of a thicker Medium into a thinner (as Fig. 28.) it will be so inclin'd to the refracting Surface, that GF (which is to CM, as the Facilities

Facilities of the given Medium) do exceed the Semidiameter BC ; then the incident Ray AB will have no refracted Ray, (after the Manner of an impossible Case in a geometrical Problem ;) which ought to be the refracted Ray entering the thinner Medium DG, being reflected by its Surface, according to *Theorem* I. of Catoptricks. And this is illustrated *Fig.* 30.

Schol. 2. When a Ray of Light passes out of the Air into Glass, it is observed that the Sine of the Angle of Incidence to the Sine of the Angle of Refraction as 3 to 2 in whole Numbers ; and in passing from the Air into Water, I is to R as 3 to 2 ; (by which Symbols henceforward is denoted the Ratio of the Sine of the Angle of Incidence to the Sine of the refracted Angle, which measures the Refraction) as 3. And on the other hand, in the passing of the Ray out of Glass into Air, I will be to R as 2 to 3 ; and in its passing out of Water into the Air, I will be to R as 2 to 3.

4. Whence the Reason is manifest, that a Ray passing out of Glass, and falling on the Surface of the Air so, as to make the Angle of Incidence more than about 42 Degrees, will not enter into the Air, but is reflected by its Surface. Namely because $2 : 3 :: 42 : 63$; that is, the Ratio sesquialtera (as it is called) of

and consequently the right Line GE, is to denote the said Ratio of the of 42 Degrees must exceed the Ray, being the Sine only of 60 Degrees. which Case the Ray is reflected accord-

Schol. 1. Schol. 3. It is demonstrable that if diverging (Fig. 30 and 31) from and refracted by the Surface BD, do ge from C, the Mediums being trans- but the same intermediate Surface remaining, the Rays converging to ill after Refraction converge to C. before what shall be demonstrated following Theorems concerning di- ing Rays, may also be apply'd to ing Rays.

THEOREM II.

an Object E be seen through diffe- Fig. 30, Mediums BDA and BDO, the Image & 31. e said Object will appear, at that C in the right Line EB (perpendi- to the plain Surface BD of the re- ing Medium, whether thicker or er) where $CB : EB :: I : R$, that is, the Distance of the Image from the Surface of the refracting Medium the Distance of the Object from the surface, as the Sine of the Angle of Inci-

Incidence is to the Sine of the Angle of Refraction.

Demonst. Let ED be any Ray of light from Object E falling upon the Surface of Refraction Thro' D draw AO parallel to EB, AC and D, and produce CD to F. Rays only being here (as well as in the foregoing Chapter) consider'd, the near EB the Axis of Radiation, wherein the Eye is suppos'd to be. It follows (for the Reasons mention'd in the foregoing Chapter) that we may look on $ED = EB$, and $CD = CB$. Wherefore $CD : ED :: I : R$. But CD is equal ED, as the Sine of the Angle BED is Equal EDA, to the Sine of the Angle BCD or its Equal ODF. Therefore the Sine of the Angle EDA is to the Sine of the Angle ODF, as I to R. But ED is the Angle of Incidence of the Ray ED, therefore ODF is the refracted Angle answering thereto; that is, DF is the refracted Ray of the incident Ray ED. The same may be shewn of any Ray diverging from E. Wherefore D will be the Focus of all Rays diverging from E and refracted by BD, that is, the Image of the Object E will appear at D. Q. E. D.

2. 1. Hence and from *Cor. 1*, *Theorem* of this Chapter it follows that (*paribus*) Rays in the Medium converging to C, will after Refraction converge to E. And if the Medium be transpos'd, then from hence and *Theorem I*, of this Chapter it follows that Rays in the Medium BDO converging to E, will, after Refraction, converge to C; and that parallel Rays after Refraction at the plain Surface of any Medium, still continue pa-

2. 2. If BDA be Water, and BDO then $CB : EB :: 3 : 4$. Whence it follows that Water appears not so deep, as it really is, by a fourth Part. But if BDA be Glass, then $CB : EB :: 3 : 4$.

From this Theorem is deduced a Method of finding the Focus C of Rays refracted by a plain Surface, *viz.* drawing EB perpendicular to the refracting Surface DD, and therein taking such that $CB : EB :: I : R$.

THEOREM III.

If the Surface BD of the Medium of *Fig. 32*, of what Thickness be spherical, and the Distance E be very far distant, then its Image will, to the Eye plac'd in AB the

(I)

Axis

Fig. 34,
35, 36,
37.

Axis of Radiation, and parallel Incident Rays, (as ED,) appear in Place C of the Axis AB produced there is Occasion, where $BC : CA ::$ But if the Object E be not very distant, then its Image will, to be placed in AB produced if there be on, appear in that Place C of AB the Ratio compounded of the Ratio EA to AC and of CB to BE is equal to the Ratio of I to R. (*)

Demonst. The first Part of this Theorem (as it relates to Objects at a distance from the refracting Surface) that the Rays proceeding from each Point therein, may, consider'd by themselves, be esteem'd parallel one to another, so it) is thus demonstrated. Let ED denote any Ray falling on the Surface, draw AD and CD, and produce ED to A. The Sine of the Angle BAD or of the Angle EDO is to the Sine of the Angle CAD (or its Complement to two Right Angles) as CB to AC, or (by reason of the Similarity of the Triangles BCD and ACD) as CB to AC, that

(*) I have comprehended all here relating to spherical Surfaces under this one Theorem for Reason, as I comprehended all relating to reflecting Surfaces under one Theorem; and also the Harmony between reflected and refracted Vision may better appear.

rection, as I to R. But EDO is the
of Incidence of the Ray ED, there-
DC is its refracted Ray. In like
may it be shewn, that any o-
of the parallel Rays proceeding
(any Point of) the Object E after
tion will pass through C. There-
will be the Focus of all such Rays,
ch is the same, at C will appear
Case the Image of an Object very
ant. Q. E. D.

latter Part of this Theorem is thus
strated. Let ED be the incident
draw AD and DC, and through
CH parallel to AD, and meeting
H. By reason of the suppos'd
s of the Arch BD, we may look
=CB, and ED=EB. Wherefore
o of I to R is equal to the (Ratio
to AC and the Ratio of CD and
ether; that is, by reason of AD
parallel to CH, is equal to the Ra-
CD to ED and the Ratio of ED
together, or which is the same, to
o of CD to DH. But CD is to
the Sine of the Angle (DHC, or
plement to two right, viz. ADH=)
to the Sine of the Angle (DCH
C, or in some Cases to the Sine
omplement of ADC to two Right.
ore EDO being the Angle of In-
of the Ray ED, it follows that I

is to R, as the Sine of the Angle
cidence of ED to the Sine of the
ADC. Wherefore (by *Theorem I*
Chapter) DC is the refracted Ray
incident Ray ED. And ED being
at pleasure, it is evident that C
the Focus of all Rays proceeding
after their aforesaid Refraction
consequently at C will appear the
in such Cases. Q. E. D.

From the first Part of this T
and the Corollary of *Theorem I*,
veral Corollaries; among wh
shall here take notice of these fol
viz.

Fig. 32.

Corol. 1. Rays ED in the Air
to AB the Axis, after their Refra
the spherical convex Surface DB
do converge to that Point, C, wh
stance BC from the Vertex B is
3AB, three Semidiameters of the

Corol. 2. Rays ED in Glafs pa
the Axis, after their Refraction
spherical convex Surface of the
diverge from C that Point, wh
stance BC from the Vertex, is
(3AB or) the Diameter of the Sp

Fig. 33.

Corol. 3. Rays ED in the Air pa
the Axis, after Refraction at
concave Surface of the Glafs,
verge from C a Point three

3 AB distant from the Vertex : as

4. Rays eD in Glass parallel to Axis, after Refraction at a spherical Surface of Air, do converge to point distant from the Vertex B the Center of the Sphere (*): that is, $BC =$ as *Fig. 33.*

5. In all the four Cases, which are the Converse of those mention'd in four Corollaries, the Rays after Refraction will become parallel to (the Axis to) a right Line drawn through the Incident Point and the Center of the

to the latter Part of this Theorem, are eight principal Cases relating to, which may all be demonstrated in the same Manner, as those four of which are here mention'd, as being sufficient to our Purpose; and are expressed by *Fig. 34, 35, 36, 37.* Of *Fig. 34* and *35* relate to Rays proceeding out of a thinner into a thicker Medium, the other two, *Fig. 36* and *37*, relate to Rays proceeding out of a thicker Medium into a thinner. And in both Cases the former Figure relates to concave Refractions, the latter to convex. And in *Fig. 36*, is represented the Case, wherein an Incident Ray ED is not refracted, but reflected into DC , according to what

(1 3)

was

was observ'd above, in *Schol.* 1 and *Theorem* 1, of this Chapter.

Schol. 1. From the former Part of *Theorem* is deducible the Way, to find the Focus of parallel Rays falling upon Spherical Glasses, viz. by taking AB so, as that $BC : CA :: I : R$. And the latter Part of this *Theorem* is used the Way, how to find the Focus of diverging Rays falling upon a spherical Glass, viz. by taking C in AB so, that the Ratio compounded of the Ratios EA to AG, and CB to BE may be equal to the Ratio of I to R.

Schol. 2. If the Mediums proper be Air and Glass, and the Ray falls out of the Glass into the Air upon the Glass (as *Fig.* 34 and 35) the Focus C may be very easily found, namely, by making $\frac{1}{3}EA : AB :: EC : AB$. For by tripling the Antecedents, $(AB =) AD :: 3EC : (BC =) DC$. EA is to AD, as the Sine of the Angle EDO is to the Sine of the Angle EDO, and $3EC$ is to DC, as the Triple Sine of the Angle EDC or HDC is to the Sine of the Angle DEA. Wherefore the Sine of the Angle EDO is the Triple Sine of the Angle HDC, and consequently is to the Sine of the Angle DEA as 3 to 2. Therefore DC, or De is in the same direct Position, is the Refraction of the Ray ED falling out of the Air into the Glass.

When the Ray passes from Glass into Air (as Fig. 36 and 37,) then the Ray may be found, according to the Principles, by taking C so, as that $AB :: EC : BC$.

3. By what has been said un- Fig. 36.
 foregoing Theorems, there being one Focus of a given Lens, the Ray may be found. Where it is to be that by a *Lens* is denoted a (diaphanous or) transparent Body (such as Crystals, Burning-glasses, &c.) of a certain Thickness from the ambient Air, transparent, terminated by two Surfaces, which are either both spherical, or the one plane and the other spherical. A straight Line perpendicular to both its Surfaces is call'd the *Axis* of the Lens. The Point where the Axis intersects the first Surface is call'd the *Vertex*; one the *Vertex of Incidence* or *Immerſion*, the other the *Vertex of Emerſion*, accordingly as it is in the first or second Surface, on which the Rays first fall, and through which they pass out again. The Thickness of the Lens, is the Distance between its Vertex's. To which add, where more than one Lens is us'd, the first which is next to the Object, is thence call'd the *Object-Lens*; and that which is next to the Eye, is thence distinguish'd by the Name of the *Eye-Lens*.

Fig. 38.

Fig. 38.

Now if the Focus before Incidence
 Immersion be given, and the Focus
 Immersion be sought; let there be
 first the Focus of the Rays after the
 fraction at that Surface of the Lens
 which they first fall; and this
 by *Theorem II*, if the Surface of the
 be plain; but if it be spherical by
rem III, namely, by the former
 it, if the Rays are parallel; and in the
 latter Part, if diverging or (*) con-
 verging. Having thus found the Focus
 Rays after Refraction at the first
 of the Lens, (that is, while they pass
 through the Lens, whence the Focus
 is call'd the *Focus of Transmittion*)
 like Manner may be found the Focus
 after Refraction at the second Surface
 of the Lens, or rather at that Surface
 the ambient Medium, which is
 common to this second Surface; that
 Focus after Emergence.

If there be more than one Lens
 pos'd, after the like Manner is
 operation to be carried on in respect
 each.

(*) Namely, according to what has been
 said of converging Rays in *Schol 3. of Theorem I.*

in like Manner, there being given the
 of one given Lens or more, there-
 may be found the Focus before Inci-
 ce, that is, the optical Instrument,
 given, thereby may be determin'd
 Distance of the visible Object.

THEOREM IV.

The Image CT of a radiant plain Sur- *Fig. 39.*
 EF, made by a refracting Surface
 whether plain or spherical, will be
 a plain Surface.

Demonst. Let A be the Center of BD
 refracting Surface, and AE be perpen-
 dicular to EF, meeting with BD in B.
 C be the Focus of the Rays diverging
 from E and refracted by BD. From F,
 Point taken at Pleasure in the radi-
 ated plain draw, FA meeting with BD in
 T and the Plain CT in T. The Ray
 FT will be the Refract of ED; and let
 BT be the Refract of FB. Because the
 Angle EAF is suppos'd to be small, there-
 fore the Arch BD may be look'd on
 as a short right Line; and a Circle drawn
 with the Diameter BF will pass through
 Points D and E, because of the right
 Angles BEF and BDF. Whence the An-
 gles EBF and EDF, (*viz.* the Angles of
 Incidence of the Rays FB and ED) being
 in the same Segment, are equal; and con-
 sequently

sequently their refracted Angles BAH and ADC will be equal. Therefore by reason of the equal Angles at A , the Triangles BAH and DAC are equiangular. BA is to AH as DA to AC ; and, when $BA=DA$, therefore $AH=AC$. because the Angle EAF or TAC is small, therefore (in a manner) $AT=AC$ and therefore AH may be look'd on as equal to AC , that is, the Focus of the radiant Point F , is placed as near as may be in the Plane CT . And the Point being taken at pleasure, it holds good so in all other Points of the Plane EF , their Focus's, are in the Plane CT ; that the Image of the radiant Plane will in this Case be also a plain Surface. **Q. E. D.**

Corol. 1. Hence it follows, that the Image of the radiant Plane EF , when the Axis of the Lens is perpendicular to the Plane, will also be a Plane parallel to the Plane. For the Image CT is to be receiv'd as the plain Surface, which sends forth Rays upon the second Surface of the Lens.

Corol. 2. If the Angle EAF be great, so that AT is so much longer than AC , as not to be capable of being esteem'd equal thereto, then the Image of the Plane EF will be concave towards the Lens if BD be the convex refracting Surface.

thicker Medium, or the concave refracting Surface of a thinner Medium; and the contrary.

THEOREM V.

The Angle fGb , under which the Image appears from G the Vertex of Emergence in a Lens, is equal to the Angle FBH which the Object appears from B the Vertex of Incidence in a Lens. Fig. 38.

Dem. Let GB be the Axis of the Lens, and perpendicular to the visible Surface of the Object FEH at E , and consequently (by *Corol. 1, Theorem IV*.) perpendicular to its Image fCh . Draw BF , Gf , and Gh . Of the innumerable Rays flowing from the Point F , and after Refraction at the Lens again united in the Image of the Point F , let two be chosen, whereof one FB meets the Lens at B its Vertex of Incidence, and there refracted tends to p the Focus of Transition in respect of F ; and being again refracted at L tends towards f . The other Ray FD being first refracted at D tends directly to p , till passing out of the Lens at G the Vertex of Emergence, it is refracted again, and thence proceeds directly to f . The Angle of Incidence of the Ray DB is DGB , and its Angle of Refraction is CGf ; and the Angle of Incidence

dence of the Ray LB, which would be refracted into BF, is the Angle LBG, and its refracted Angle EBF. Now because the right Lines pB and pG are to be esteem'd equal, (reason that the Thickness of the Lens is not to be consider'd,) therefore the Ratios of the Angles DBG and LBG being equal, and consequently the Angles themselves DGB and LBG, and therefore the refracted Angles CGf and EBF will be equal. In like manner it may be proved that the Angles CGh and EBH are equal. Therefore the Angles FBH and fBH are equal. (And the like may be shewn in other Case,) Q. E. D.

Corol. Hence it follows, that a Point is to its Image made by a Lens, as the Distance of That from the Vertex of Incidence is to the Distance of That from the Vertex of Emerfion, or (the Thickness of the Lens being not regarded) as their Distances from the Lens. But if the Radiant be a Surface (the homologous Lines will keep in the same Ratio, but the said Surface will be to its Image (in the Ratio duplicated, or) as the Squares of their Distances from the Lens. And thus may be determin'd the Ratio, which the last Image, (*i. e.* that which is immediately seen by the Eye) made by the

ne Lens or more, has to the visible
ect, whose Image it is.

bol. From what has been said, may
accounted for and illustrated the Affec-
of (or several Particulars relating
refracting Surfaces, whether plain
pherical. Among which Affections
more remarkable are these that fol-
viz.

If the prime Radiant or Object be *Fig. 40.*
stant, and the Surface PCQ of the
be plain, the Surface PDQ be of
and convex, and the ambient Bo-
the Air, then (by *Corol. 4, Theorem*
Db will be equal to the Diameter of
phere PDQ; (for by *Axiom 1*, the
parallel to BC pass through the
Surface PCQ, whereon they fall
indicularly, without being refrac-
and consequently by *Theorem IV*
f, be will be the Image of the far
Object, from which proceed the
FBE; and therefore the said Image
appear in an inverted Situation with
to its Object: Namely, the Point
the Object, and the correspondent
f of the Image, will be on different
of Bp the Axis; and so of the o-
Points B and b, E and e. And
ore, if F be the lower Part of the
f will be the upper Part of the
; and so as to the rest agreeably.

2. But

Fig. 41.

2. But if the Surface PCQ be convex and PDQ plain, then (by *Corol. 1, rem II, and Corol. 1, Theorem III of Dioptricks*) Cb will be equal to the Diameter of the Sphere PCQ, and a third Part of the Thickness of the Lens over. Or neglecting the Thickness of the Lens, (usual in the Object Lens of a Telescope,) in this as well as the former and consequently in general of any convex Lens, it may be said, that the Image of an Object far distant, made by such a Lens, will be equal to the Diameter of the Sphere.

Fig. 42.

3. If the Lens PQ be of Glass, and equally convex on both Sides, then (by *Corol. 1. Theorem III, and Theorem III of Dioptricks*) Db will be equal to the semidiameter of either Sphere. Lastly

Fig. 43.

a whole Glass Sphere, the Image of an Object far distant will appear at the Distance of half the Semidiameter from the Center of the Sphere: For in this Case Regard must be had to the Thickness of the Lens.

Of Burning-glasses.

4. In all these or the like Cases, if the Sun be the far distant Radiant or Object, and the Lens be considerably larger than the Sun's Image, in the Place of the Image will be the *Burning-point*: Any such convex Lens will burn faster than a concave Reflector (*cateris*).

by reason more Rays are lost by the
than by the former.

If in the foremention'd Place of the
there be placed a lucid Body it self; the Image of the said Body will ap-
at a great Distance; that is, the
lucid or shining Body will cast a
at a great Distance, so as that
so far distant may be clearly seen
the said Light. And this is the Manner,
by a Candle, put into a Dark-Lan-
with a convex Chrystal, gives a
at so great a Distance as usual

*Of Dark-
Lanterns
with Con-
vex Glas-
ses.*

If the Radiant or Object be not (as
far distant, but yet is more distant
the Lens than is the Place where
appear the Image of a far distant
; besides the Affection aforemen-
(viz. that the Image will appear
ed,) there will be in this Case also
other Affections. Namely, as the
comes to the Lens, the Image
from it, and contrariwise; till
radiant being come into the Place,
would appear the Image of a far
Radiant, its own Image becomes
stant. All which Affections may be
d in a Dark-Chamber, into which
at several Distances send their
through a convex Lens or Glass.
Place of the Image of each Radiant
may be distinctly known, by ob-
serving

serving *where* the Image of the said
does appear most distinctly on a Sh
White Paper or the like.

*Of a Ma-
gick Lan-
tern.*

7. And on these same Princip
pend the Mechanism of (what is
a *Magick-Lantern* ; namely, w
the Images of little Pictures are rep
ed on a white Wall or the like.

8. If the Radiant be nearer to
vex Lens, than the Place where
appear the Image of a far distant
ant or Object, then its Image will
on the same Side of the Lens w
Object it self ; and its Place may
termin'd from the given Place of t
diant, as afore. The Image in th
will always appear in the like Si
with the Object, and greater than
if the Object comes to the Lens,
mage will also ; if that goes fro
Lens, this will also ; only the Im
in both Cases move quicker.

*Fig. 44,
& 45.*

9. If the Lens be concave, th
the respective Corollaries of *The*
of Dioptricks) the Image *ebf* ma
plain concave Lens, PQ, will be
the Diameter of the Sphere PD
will be erect or in the like Positi
the Object, and on the same Sid
the Object reckoning from the V
If the Surface PCQ be also concave
the Object not far distant, its

be determin'd after the like Method, finding (according to *Theorem IV* of *Opticks*) the Image of that Point of Object which is situated in the Axis of the Lens. In respect to which Image, as what has been already said, it is observ'd, that it will together with the Object come to or from the Lens, but

Further, it is here observable, that the foremention'd Theorems depends on the Mechanism or Contrivance of the several optick Instruments, made use of to assist the Eye, or to supply the several Defects of our Sight. For, as the Eye is the natural Organ or Instrument, design'd for this End, namely, that on the Bottom of the Eye may be painted the distant Images of outward Objects; so it is manifest that the same Eye can see distinctly at a certain Distance from the visible Object. Could the Eye always place itself at such a Distance from the Object, as is necessary to distinct Vision, then without the other Requisites to Sight being given, such as a due Degree of Light, the Eye might always see distinctly. It is true indeed that the Distance requisite to distinct Vision is not rigidly determin'd to one single Point, but admits of a Latitude; forasmuch as the same Eye can so alter its Figure according to

of Telescopes, Microscopes, and Spectacles.

(K)

the

the various Distance given, that it be look'd on not as one Eye but several. But then, since this Latitude of Distance is contain'd within certain Bounds beyond which the Eye can by no Means see distinctly, hence arises the Need of artificial Instruments. A Lens, or spherical reflecting Glass, is sufficient to remedy this; forasmuch as by the Image of such an Object, can't come to as we would, make the Help of the Theorems above demonstrated) be brought near us, so as they may have a distinct View thereof. of this Kind are those single Glasses by such as can't see well at a certain Distance, and apply'd by them to their Eyes, when they would discern the Face or Picture of a Person (or thing) that is farther distant from them than they can distinctly see with the bare Eye. As the Word *Telescope* does in the common Tongue denote an Instrument which enables us to see far off, so these single Glasses may be call'd *single Telescopes*, to distinguish them from such Telescopes made of two or more Glasses.

II. But because (beside distance) it is often requisite in humane Vision that the more minute Parts of an Object should be discern'd; and because it is found by Experience, that an

h appears under a less Angle than of Minute, appears but as a Point, or that its Parts can't be distinguish'd from the other : Hence it often comes to pass, that the Object being brought so near to the Eye, as that its Particles to be examin'd may be seen under a sensible Angle, thereby the Object it self becomes near to the Eye, so as not to be within the Bounds requisite to distinct Vision. This Inconveniency, when alone, may almost be remedied by any given Lens or refracting Glass ; forasmuch as the Image of the said Object (*) may by the said Lens or Glass be represented (in any given Measure, *i. e.*) so as to have any given Ratio or Proportion to its Object.

Now this may be done in respect of a reflecting Lens, as is shewn above in *Schol 7*, to *Theorem V*, or last of the Book. How the same may be done in respect of a refracting Glass, shall be here shewn. Let a Glass be given (*Fig. 46*) the Semidiameter of whose fore-
 face is AB, the Semidiameter of the hindermost face is CD. Draw CM as you please ; and let the Ratio be such as ought to be between the homologous Parts of the Radiant and its Image, and be denoted by the Ratio MD to DC. Draw AM, where M is a Point on the fore-face AB, and through B draw a Line BE, meeting CM in E ; ME doubled will be the Distance of the Radiant from the Lens. And after this Manner may be found, in respect of any given Lens, the Position, or Place where any Radiant is to be placed, (its Image made by the Lens may be equal to a given Measure, which is similar or like to the Radiant, *i. e.* that the Radiant may have a given Ratio [to its Image] made by the Lens.

Fig. 46.

(K 2)

And

And of this Kind are those single Glasses us'd to see the Shape or Parts of Insects, and the like, and thence *Microscopes*, the Word importing in Greek Language an Instrument, whereby we see *small Things*. To these be referr'd Spectacles, of which more and by.

But if both the foremention'd Inconveniencies concur, then they are not remov'd but by the joyn't Help, either a Lens and Reflector together, or more than one Lens, or lastly of more than one Reflector. And how Instruments consisting of two or more of these are made, shall be next illustrated.

Fig. 46.

13. Let R denote the Object given under the given Angle under which the Image is to be represented, D the given Distance of the Sight, and L the given Distance of the Eye from the Lens. Draw the Triangle AOB, so as that the Vertex Angle at O may be equal to the given Angle S, and OE the Perpendicular from the Vertex to the Basis may be equal to the given Line D. If you'd have the middle Point of the Object be the Axis of the Lens or Reflector, (which is most convenient for Practice) the Angle AOB must be made an Angle of 60°. Take $OV=L$, and at V place a

ter so, as that its Axis may fall
th OE.

en having E thus given for one Fo-
f the Lens or Reflector, by the re-
ive *Theorem* III of Catoptricks or
ricks or their Scholium, find the o-
ocus e ; namely, that so taking e for
ocus before Incidence, E may be the
after Inflection at the Lens or Re-

. Through e draw aeb parallel to
meeting with Va and Vb (drawn
gh V, and parallel to VA and VB)
nd b.

ollows from *Theorem* V, of Catop-
or Dioptricks (respectively, as you
ate for a reflecting or refracting
) that if aeb be the Radiant, AEB
e its Image. Wherefore if the Ob-
ven R, (which is here suppos'd to
r at hand) and a second Lens or
ter be so plac'd, according to *Schol.*
Theorem V of Catoptricks, or accord-
the Note before added to *Schol.* 11
Theorem V of Dioptricks,) that the
of the Object made by this second
r Reflector, may appear just in the
Situation, and Bigness of aeb ;
will be thus made such a Micros-
is requir'd. For aeb will be the
of the given Object R, the Image
ch Image, and that seen by the
will be AEB. And this will appear

(K 3)

under

under the Angle AOB equal to the Angle S; and in the Distance OE to the given Distance D, and consequently will appear distinct; and lastly Distance of the Eye from the Lens or reflector next to it in V, will be equal to the given Distance in this respect. so the Instrument will be in all Respects such as is requir'd.

14. If the Instrument be made for the Eye of an aged Person, then the Line OE becomes infinite, and consequently the Point e is to be found by *Theorem III* of Catoptricks and Dioptricks. As for the rest of the Work, it is the same as afore.

If the Object propos'd to be discovered be far distant, then having all the other things (as afore) given, but the Angle S, a Telescope may be made fit for the Purpose. In a right Line extended toward the remote Object propos'd, take from the Eye toward OE and OV equal to the given Distance D and L; and in V place a Reflector or Lens having its Axis in VE. Then find the Focus E of the Lens or Reflector plac'd at V. Being thus given, find the other Focus e, namely, that this being taken for the Focus before Inflection, E may be taken for the Focus after Inflection. In the right Line OE so place a second Lens or Reflector having also its Axis in OE, that the

of the propos'd Object made there, may appear in the right Line *aeb* perpendicular to *OF* ; and so there will be such a Telescope as is requir'd. The first Image of the far distant Object sh'd will be in *aeb* ; and the Image of the Image will be in *AEB*, the Distance which *AEB* from *O* is by Construction equal to the given *D*, and consequently distinct to the Eye ; and also the Distance of the Eye from *V* is equal to the *L*. And from hence may be found the Angle, under which the last Image is

By the Help of three or more Lens's or Reflecters, an Instrument may be made to present even a far distant Object under a given Angle. Namely, let any one Lens or Reflector form the Image of the Object propos'd ; and then with the other two make (as afore) a Microscope, presenting the first Image (as being a Radiant nigh at hand) according to the Conditions propos'd ; and so there may be made such a Telescope as is requir'd.

In like Manner, a Microscope being made of three Lens's or Reflecters, by adding a fourth it will become a Telescope.

In all which Cases is known the Proportion, which the Image seen by the Eye has to the Object, or (which comes to the same) the Proportion,

(K 4)

on,

on, which the Angle under which said Image is seen, has to the Angle under which the Object is seen without Instrument, (which, in respect of distant Objects, is as the Distances Lens's or Reflecters from the common focus *e.*) And consequently from (according to the Corollary of T. IV, Chap. III and IV,) may be computed how much the Instrument does heighten Sight.

Fig. 48,
& 49.

17. I shall next adjoin some Observations, in reference to a dark Chamber, as abovemention'd in *Schol. 2*, T. IV, Chap. II. Namely, it was the serv'd, that Rays let into a dark Chamber through a naked little Hole, will paint the Images of their respective Objects on a Sheet of white Paper placed against the Hole. To which it is here added, that the same will be done through a much larger Hole, if a Lens or Convex Glass be placed therein, with the difference, that the Images of outward Objects will be painted much more clear and distinctly this Way than they will without a Lens; which is thus accounted for, Through the little Hole (Fig. 48) must necessarily pass fewer Rays from the outward Objects than through a much larger Hole (Fig. 49.) And not only so, but those fewer Rays, which

gh the bare Hole are dispers'd; as by a convex Lens or Glass all the proceeding from any one Point of Object, are united again at a certain place, and so render the Image more lively and distinct, than the Way. This is illustrated *Fig. 48* 49. Whence it is also obvious, why with Cases, the farther the Paper is from the Hole, the bigger the Image appear; as also why the farther the hard Objects are from the Hole, the their Images will be; and why the made by a Glass will appear most fully at the Distance *ac* (*Fig. 49*) with such like Particulars.

But it is observable, that in both, either with or without a Glass, Image will appear inverted in respect of the Object, as has been afore observ'd under *Theorem IV, Chap. II*, and is evident from *Fig. 48* and *49*. And from *Fig. 48* it is evident, that when the Image painted erect on the Bottom of the Eye, then the immediate Radiant *abc* it is seen inverted by us; and on the contrary, when the Image *abc* is painted erect on the Bottom of the Eye, then the immediate Radiant *ABC* erect. For as in the said Figure the Image *abγ* is erect in the Eye, so if we were put in the Place of the Paper,

pet, the first Image *abc* would be
ted therein inverted, in respect of
Object *ABC*.

19. This being so, the Manner
that Sensation, which we call Vision
perform'd, seems to be the same, a
wherby a blind Man by the Thrust
End of several Sticks against his
can thereby distinguish, which
thrusts from above, which from
Namely, so by the Sensation can
the Ends *a* and *b* of the Rays *Aa*
and *Cc*, touching the Retina, we
turally endued with a Faculty of
distinguishing, from whence each
proceeds, viz. that the Ray *Aa*, as
ing the lower Part of the Retina
proceed from the upper Point *A*
Object; and the Ray *Cc* as touch
the upper Point of the Retina, do
ceed from the lower Point *c* of t
ject; and the Ray *Bb* as touching
Middle of the Retina, does proceed
B the Middle of the Object. And
quently we are enabled to judge
Situation of Things aright, by re
their Rays after such a Manner as
appears from the fore said Experiment
do: Which is the same as to say
we see Things in their Erect or
tuation, by having their Images
on the Retina in an inverted M

contrariwise, we see Things invert-
having their Images painted on
Retina in an erect Manner,

I shall now, in the last Place, ex- of Specta-
the Mechanism of Spectacles, or how cles.

come so to help the Eye. It is then

from the Rules of Dioptricks,

convex Glasses turn the Rays in-

or towards the Axis of the Glass;

the more convex they are, so much

the inward the Ray is turn'd. It is al-

so by Observation or Experiments,

the Chrystalline Humour has the

effect as a convex Glass. Where-

when the Surface or Coat of the Fig. 56.

chrystalline Humour is of such a due

curvature, as that it makes the Rays of

several Points of an Object to unite

in so many several Points just up-

on the Retina, then Vision is duly per-

formed as Fig. 50.

But when the Chrystalline Humour

is not convex enough, but too flat, (as it Fig. 51.

happens through Age,) then the Rays pas-

sing through it are not united soon e-

nough, i. e. are not united at the Retina,

their Point of Union is further be-

hind the Retina, and consequently then

we can't see duly or distinctly, but

confusedly, the Objects, from

whence proceed the Rays. Wherefore to

correct this, convex Glasses, (call'd Specta-

cles)

cles) are us'd, whereby the Rays are made to unite in their proper Place at the Retina. In order thereto, the flatter the ChrySTALLINE Humour is, the more aged the Person is, the more convex must the Spectacles be.

Fig. 52.

22. On the other Hand, if the Surface of the Chaystalline Humour be too convex, (as is the Case of short-sighted Persons,) then the Rays are thereby refracted too soon, or before they come to the Retina, and so Vision is not duly perfected. Hence such Persons hold Things near to their Eyes, to see them the better, because (according to the Rules of Opticks) the nearer the Object is to the Eye (Lens, or in this Case) the ChrySTALLINE Humour, the further will be the Focus of its Rays on the other Side. Hence so concave Spectacles helps such Persons to see at a Distance, by making the Rays unite in their proper Place, *viz.* at the Retina. Lastly, such Persons see better and further as they grow elder; because the ChrySTALLINE Humour grows more and more convex, or less concave, in their old Age: Wherefore the way is the Reason, that such Persons do not use Spectacles when they are Young, but only when they are Old, and this is sufficient to our Purpose concerning Dioptricks.

C H A P. V.

Of Perspective.

perspective the chief Things (beside Eye and the Object) to be considered and therefore explain'd, are those are contain'd in the following Definitions.

I.

*Definitions
of Terms
us'd in
Perspective*

(†) *Geometrical Plane* is a plain parallel to the Horizon, and placed lower than the Eye, in which we place the visible Objects without any alteration (except it be reducing a great into a small one,) and upon which representation of the Object to be represented in Perspective is describ'd.

2.

The Geometrical Plane, what.

Situation (call'd also the *Ich-* or *Plan*) of an Object is its geographical Projection upon the

3.

The Situation of an Object, what.

also called the Basis. This and the following are here denoted, are not represented in Figures; being not easie to be so apprehended by the Eye; but they may be more easily apprehended by the Imagination, or else by actually placing so many such a Manne:.

(*) geo-

(*) geometrical Plane, or, that which is describ'd upon the Geometrical Plane, when from all the Points of the Object right Lines are drawn perpendicular to the said Geometrical Plane. the (Plan or) Situation of a right Cylinder is a Circle, and the Situation of a right Cube is a Square.

4.
The Picture, what.

The Picture is a plain Surface pos'd as transparent as Glass, always plac'd at some Distance between the Eye and the Object, to represent the Object in Perspective; where the Picture is also call'd the *Picture Plane*.

5.
The Ground-line, what.

The Picture stands (usually perpendicular) upon the geometrical Plane. Whence the common Section of the Picture and the geometrical Plane, is call'd *the Base of the Picture*, or the *Ground-line*.

(*) If the Orthographical Projection be (not upon a geometrical Plane, but) upon a Plane parallel to the vettical Plane (describ'd §. 11) it is call'd *Front*; and if it be upon a Plane perpendicular to the vettical Plane it is call'd *Profile*.

(†) Sometimes the Picture is inclin'd to the Plane or Horizon, and has also a curve Surface. As the Surface of an arch'd Roof is to be drawn, being not common, the Picture is look'd upon in this Chapter as a Plane perpendicular to the Plane or Horizon.

Horizontal Plane is a plain Surface parallel to the Horizon, and which receiv'd to pass through the Eye, and perpendicular to the Plane of the

6.
The Horizontal Plane, what.

Horizontal Line is that right Line, which the horizontal Plane and the Plane of the Picture intersect, and which is parallel to the Ground-

7.
The Horizontal Line, what.

Principal Ray is a right Line from the Eye, perpendicular to the Plane of the Picture, which therefore must run along the horizontal Plane.

8.
The Principal Ray, what.

Point of Sight, call'd also the **Principal Point**, is the Point where the principal Ray is cut by the principal Ray, must necessarily be in the horizon-

9.
The Point of Sight, what.

Point of Distance is a Point in the horizontal Line, whose Distance from the Point of Sight, is equal to the Length of the principal Ray.

10.
The Point of Distance, what.

Vertical Plane is a plain Surface, going along the principal Ray, is perpendicular to the Horizon, and so to the geometrical Plane, and also to the

11.
The Vertical Plane and Line, &c. what.

The common Section of the Picture and vertical Plane being call'd the **Line**, and being also the Measure of the Height of the Eye; and the common Section of the geometrical and vertical

vertical Planes being call'd the
Station.

12.

*The Ap-
pearance
of a Point,
what.*

The Representation or Appearance
ny Point of an Object is that Point
the Picture is cut by a right Line
from the Eye to the Point propos'd
Object.

13.

*The Acci-
dental
Point,
what.*

The Accidental Point of a right
the Point, where the Picture is
right Line drawn from the Eye pa
the Line propos'd. Whence it is
conclude, that all Lines, which ar
l parallel to the Picture, have no ac
Point; and that all other Lines
are parallel one to another, ha
same accidental Point. It is also
able, that all right Lines, which
pendicular to the Picture, have th
cipal Point for their accidental
and that all those, which make
right Angle with the Picture, ha
of the Points of Distance for their
tal Point.

14.

*Observa-
bles from
what has
been said.*

It is also observable from w
been said, that all the Parts of an
which are lower than the Eye or
tal Plane, ought to be represente
Picture below the horizontal Line
on the contrary, all above the
tal Plane, or higher than the Eye
to be represented in the Picture ab
said horizontal Line. In like Man

Objects, which with respect to the
 re on the right Hand of the verti-
 cal, must in the Picture be repre-
 sented on the right Side of the vertical
 and such as are on the Left, must
 be represented on the left Side of the said
 vertical Line.

In order to perform any Operation,
 of Paper, which you would
 upon, must be divided into two
 by the Line AB (Fig. 53) which
 represent the Ground-line: The up-
 per Part of the Paper, viz. ABDD, must
 be for the Plane of the Picture;
 the lower Part ABYZ of this Paper
 be a geometrical Plane.

15.
*How to de-
 scribe on
 Paper the
 Plane of
 the Picture,
 and the
 Geometri-
 cal Plane.
 Fig. 53.*

The next Thing is to know, (under
 an Angle the Picture ought to be seen,
 whatever is represented therein may
 be in just Proportion, and may easi-
 ly be taken in by the Eye at one View;
 in short,) how far the Points of
 the Picture ought to be from the Point of
 View. Let there be propos'd a Square,
 which takes in all that you would repre-
 sent in Perspective. And let the Ground-
 line be of equal Length with one Side
 of the Square propos'd. Wherefore, if
 the Eye of the Spectator was at G, he
 could not see the two Ends A and B, be-
 cause the Eye could see, (†) at most, but

16.
*How to
 find or set
 off the
 Points of
 Distance.*

According to Theorem II, of Chap. II.

(L)

fo

so much as is comprehended under right Angle GHI. But if the Eye were at K, it could see the Ends A and B, because the Angle AKB is less than a right Angle, viz. 80 Degrees. And the Eye would see the Ends A and B better at L, than at K, better yet at M, where the Angle AML is 60 Degrees. And from such a Distance the Objects (to be represented in Perspective, and contain'd in the forementioned Square) may be seen in Perfect Perspective, the visual Angle AMB being neither too great nor too little. The Angle ANB may also be very well. Wherefore bisect AB in F, and from F draw a Line FV perpendicular to DD, a vertical Line, and consequently V will be the visual Point or Point of Sight. From the said Point V set off the Distance (marked with an Asterisk) FK or rather FL, or) FM, on each Side upon the horizontal Line DD, viz. to D and D, which will be the Points of Distance requir'd or found.

17.

A general Rule concerning the same.

And this may be look'd on as a general Maxim, viz. that the Distance twixt the Point of Sight V and the

(*) If the Distance VD were less than FK, the Perspective Square ABCE (concerning which see the next Page) would appear irregular, because it would be seen under too great an Angle.

Distance D and D must be (at least) to FA or FB. And it will not be to let this Distance be somewhat. And, if in this Case the Plane of the Picture be not wide enough to have two Points of Distance, there shall only one be mark'd, and the principal Point or Point of Sight V may be on one Side, as Fig. 59, &c.

When the Points of Distance D and D (Fig. 58.) being found, draw the Lines AV, BV, as also AD and BD. And the Figure ABCE will be the Appearance (in the Picture) of the Square, propos'd to be represented in Perspective; which Appearance of the said Square is in short the *Perspective Square*.

Proceed we now to the Representation (in the Picture) of Points, Lines, and Planes. And first, how to find in the Picture the Representation or Appearance of a Point given in the geometrical Plane.

From C the given Point (Fig. 54.) let fall upon the Ground-line AB the perpendicular CE; and from the Point C draw to the principal Point V the Line CV. Upon AB set off EF (or EA) = EC, and then draw FD (or AD either way) which will upon VE give at d the Appearance of the given Point C.

18.
The Perspective Square, what.

19.
How to find in the Picture the Appearance of a Point given in the geometrical Plane.
Fig. 54.

20.
To find in
the Picture
the Appearance
of a
right Line
given in the
geometrical
Plane.

Fig. 55,
56.

Secondly, how to find in the Picture the Appearance of a right Line given on the geometrical Plane. Suppose (Fig. 55 and 56) to be the right Line mn . Find (as afore) the Appearance of the Point M, viz. at m , and the Appearance of the Point N of the Line MN, viz. at n . Then join m and n , the Line mn will be in the Picture the Appearance of MN the Line proposed (*).

21.
To find in
the Picture
the Appearance
of a
curve Line
given on the
geometrical
Plane.

When the Line given on the geometrical Plane is (not a right Line, but a curve Line, then from several Points on the Line draw Perpendiculars to the Ground-line; by means of which, and what has been said, may be found in the Picture the Appearances of all those Points, which being join'd by a Curve Line, that Curve will be the Appearance of the Line propos'd.

(*) That every Thing you design to represent in Perspective, may appear in just Proportion, it is sometimes to have the Eye at a great Distance from the Picture, which may hinder from marking either the Distance upon the horizontal Line. In which case you must mark only half of the Distance of the Eye from the Picture upon the horizontal Line, as (Fig. 57) the Point Q, which will represent one of the Points of the Line. And then you must only set off half the Perpendicular upon the Ground-line AB, from I to P. Then the Point p will be the Appearance of H the Point proposed.

Thirdly, To find in the Picture the
 Appearance of a plain Figure given on
 a geometrical Plane, suppose the Square
CEGH Fig. 58. Find the Appearance
 (as been afore shewn) of its four an-
 gular Points *C*, *E*, *G* and *H*; which will
 be *c*, *e*, *g* and *h*. Join the said (last)
 Points, and the Perspective Square *cegh* will
 be the Appearance of the given Square
CEGH, when seen foreright, or when
 the Line *KL*, of the given Square falls in
 the vertical Line. If the given
 Square be all on one Side of the vertical
 Line *VF*, (as Fig. 59) then the Perspec-
 tive Square *cegh* (in Fig. 59) will be the
 Appearance of the given Square *CEGH*.
 There also it is to be noted, that the
 Appearance *g* of the Point *G* may be
 found also after this Method. Namely,
 from the Ground-line *AB* take the Point *B*
 as Centre, and draw *BV*. Then set off
 a Length equal to the Perpendicular *IG*, and
 draw *MD*, which upon the Ray *VB* will
 meet the Point *N*. Through which *NC*
 draw a Line parallel to *AB*, will upon
 the Ray *VI* give the Point requir'd *g*.
 This Method may be used, when the
 Perpendicular *IG* is so long, that the
 Length thereof can't be set off upon the
 Ground-line *AB* within the Picture.
 In the same Manner may be found in
 the Picture the Appearance of any other
 plain

22.

To find in
 the Picture
 the Appearance
 of a
 plain Fi-
 gure given
 in the geo-
 metrical
 Plane.

Fig. 58,
 59.

23.

A Remark.
 Fig. 59.

24.

Another
 Remark.

plain Figure, viz. Triangle, Pentagon, Heptagon, &c. Namely, by finding the Appearance of each Point of the plain Figure propos'd then joining the Appearances so for right Lines.

25.

To find in a Picture the Appearance of a Circle given in the geometrical Plane.

Fig. 60.

It shall here be only observ'd in reference to plain Figures, that in the Picture the Appearance of a Circle given in the geometrical Plane, must be describ'd about it a Square (Fig. 60.) the Square EFGH about the Circle ILKM. One Side of the Square viz. EF (or GH) must be parallel to the Ground-line AB, and consequently the other Side EH (or FG) must be perpendicular to AB. Draw the two Diagonals EG and FH, which intersecting at the Center of the Circle, will give upon the Circumference of the Circle four Points, P, Q, R and N. Then in the Picture the Appearance of the Square EFGH, which will be the Perspective Square *efgh*, and also the Appearances of the Points L, Q, K, R, I and P; which will be in the Perspective Square the Points *l, q, k, r, i* and *p*. A Curve drawn through these last Points will determine the Appearance of IKLM the Circle propos'd. Note, that the Appearance of the Circle will also be a true Circle, if the

It should be seen fore-right, that is, if its
(*) LM, being perpendicular to
make one right Line with VF the
al Line. But if the Circle propos'd
be situated (as Fig. 61,) then its Ap-
pearance will be (as there) elliptical.

Proceed we now to shew, how to re-
present in Perspective a *Floor of equal*
squares seen fore-right, without a geo-
metrical Plane. Divide the Ground-line
(Fig. 62) into as many equal Parts
as please, each of which will repre-

26.

To repre-
sent a Floor
of equal
Squares
seen fore-
right.
Fig. 62.

to have the Appearance of a Circle in the Picture,
as well as a Circle, the Distance between the Eye and
the Picture must be of a determinate Length, which may
be thus. Having produc'd the Side of the circum-
square EFGH, 'till it meets at right Angles with
the horizontal Line DD in a Point as S, draw SL, and
from it SC=SV, and the remaining Part LC (of SL)
be the Distance between the Eye and the Picture, or
the Distance to the said Distance. If VD be given, and you
draw VE (or the Distance between the horizontal
Line and the Ground-line AB, that is) the Height of
the Picture, that the Appearance may be also a true
Circle, the rectangular Triangle SVL shews, that the
Length of the Line EL (or of the Ray of the given Circle
must be taken from the Square of the Line LS, and
the Side of the remaining Square will be the Height re-
quired. Note further, that the Perspective Square *efgh*
is equal to the Square *efgh*, and the Mid-point X of the Line *mL* (or *ml*) will
be the Center of the Perspective Circle; upon which there-
fore the said Circle may be drawn without any
other, or without finding the Points *l, q, k*, &c. Lastly,
as in Fig. 60, the Perpendiculars EI and TN are
drawn from the Ground-line AB, partly to avoid Confusion
in drawing the Arch of many Circles, partly and chief-
ly because it is evident (from the setting off FK and QR)
that EI and TF=TK.

sent

sent the Side of a Square. Draw the each Point of Division to the principal Point V, as many right Lines or the two last of which will be VA VB. Then draw the Ray AD (or which will cut the foregoing Ray Points, through which you must draw Parallels to the Ground-line AB. The last of these Parallels will be EF, which will have its Divisions equal between G and H. And the like equal Division may be continued from G to E, and from H to F, in order to draw these new Points of Division, from the principal Point V, other Rays will upon the Lines DA and DB meet the foregoing Parallels respectively below to them. Thus you'll have in Perspective all the Squares, which can be comprehended in the Space ABFE. If you would have more, draw DE, which will cut all the Rays that proceed from V in Points, thro' which (as afore said) must draw Parallels to AB, the last of which will be KL. And so, go on as before.

27.

To represent
a Floor of
Equal
Squares
seen Corner-wise.
Fig. 63.

If you would represent in Perspective a Floor seen fore-right, and containing equal Squares seen *Cornerwise*, work thus. The Side AB of the square Floor is determin'd upon the Ground-line A B. Describe the Appearance of the square

drawing from the two Ends A and B
the Side given, to the principal Point
the Rays VA and VB; and to the
Points of Distance the Rays DA and

These Rays will cut the former in
Points E and F, which being join'd,
Line EF will be parallel to the Ground-
; and ABEF will be the Perspective
re. Having divided AB (or the
of the Perspective Square) into e-
Parts, to each Point of Distance D,
Rays through each Point of Divi-
; which Rays by their common In-
ctions, will form the Appearances of
Squares seen Corner-wise. With
Squares it will be easie to fill the
pective Square ABFE, because all
Rays that proceed from the two
s of Distance, divide equally in
same Points the Side EF parallel
AB; which is also divided equal-
d in the same Points, by the said
which go from the two Points of
nce.

represent in Perspective a Floor 28.
of equal Squares seen fore-right, *To repre-*
encompass'd with a Border or Frame, *sent a Floor*
at a geometrical Plane; work thus. *of Squares*
the Ground-line AB into as many *seen fore-*
alternatively equal and unequal, *right, and*
would have Squares and Borders, *encompas-*
Points 1, 2, 3, 4, 5, 6, 7, 8. *sed with a*
(M) From *Border.* Fig. 64.

From all these Points draw Rays to the first Ray will be VA, the last Then draw the Ray DA, which will those that go from V in Points, thro which you must draw Parallels to the last of these Parallels will be which terminates the Perspective Square ABFE. And so you will have the presentation of the Floor requir'd. you may continue it, if you draw ther Ray through the Point E, and Point D; and then proceed to work as afore,

29.
To represent a Floor of equal Squares seen Corner-wise, and with a Border, &c.
Fig. 65.

To represent such a Floor as is mention'd, but seen corner-wise, thus. Divide the Ground-line AB into Parts as afore, viz. alternatively equal or unequal. Then draw thro' the Points Division, to the Points of Distance, or Lines; which will (as afore) terminate in the respective Square, this being to be describ'd as is afore taught.

30.
An useful Way to represent in Perspective one or more Figures;

Lastly, It is observable, that if you describe Squares given in a geometrical Plane, then the Ground-line AB may be divided into Parts equal to the Sides of the given Squares. And the little Perspective Squares, not only will be the appearances of those in the geometrical Plane, but also may be very useful in Perspective one or more figures made up of several Lines;

Int

F

ence, a fortified Polygon. Namely, said Polygon (or Wall of a fortified town) being describ'd on the geometrical Plane with the Squares, it will not be difficult to describe the same likewise in Perspective with the Squares of the Picture. drawing such a Part of it in each Part of the Picture, as is describ'd in the correspondent Square of the geometrical Plane. All which will be sufficiently illustrated by a bare Sight of *Fig.*

and in like Manner, *Fig. 63*, if upon a Square be drawn in the geometrical Plane, as *ABGH*, whose Representation is the perspective Square *ABEF*; that Square *ABGH* on the geometrical Plane be divided into other little Squares by Lines parallel to the Diagonals *AG* and *BH*, the said Square *ABGH* may be made use of, to put or represent in Perspective several Things at once, the Images of the said Things being determined upon the said Square.

Since thus I have taken notice of some Part of Perspective, as is agreeable to the Design of this Treatise. And therefore I will here put an End to this Treatise of Opticks.

31.

A like Method.

32.

The Conclusion.

F I N I S.

ERRATA to Trigonometry.

PAGE 7. Line 33. For *fit for Use*. Read *not fit for Use*. p. 9, l. 1.
E-D E-D

r. —₁₀ax. p. 19. l. 5. f. —₂—₂B. r. —₂—₂D. p. 30. l. 1

E.A. p. 35. l. 22. f. $E=350$. r. $E=35$ degs. p. 43. l. 13. f. $CA=793$. p. 44. l. 6. f. *Arch* CBA . r. *Angle* CBA . p. 51. l. 1. f. BA . r. *Line* BC . p. 54. l. 16. f. *Angles* meet. r. *Angles*. l. 17. f. 55. l. 13. f. r. at M . r. at N . *ibid.* l. 19. f. at N . r. at M . p. 56. at the End m . r. at the End n . *ibid.* l. 4. f. at the End n . r. at the End m . p. 65. l. 1. f. so share. r. so shall. p. 82. l. 22. f. to 99. r. to 100.

ERRATA to *Mechanicks*.

PAGE 6. Line 14. For contriv'd. Read sollicit'd. p. 10. l. 21. f. r. little Body may. p. 13. l. 12. f. Laver: r. Leaver. ibid. but (the. r. but) stre. p. 51. l. 21. f. said Squares. r. said result. f. is equidistant from C to A. r. is six times as distant from p. 17. l. 1. f. to b. r. to β. ibid. l. 3. f. 6C. r. βC. ibid. l. 7. f. r. this being. p. 20. ult. f. Gz. r. Cz. p. 30. l. 10. f. were. r. ibid. l. 11. f. at C. r. at G. ibid. l. 12. f. at r. at B. p. 31. f. Mark; r. or Hook. p. 34. l. 23. f. as Fig. r. as Fig. 28, 29, 30. f. Pulley) r. Pulley as Fig. 27.) p. 35. l. 19. f. by TS. r. by R. f. d, e, f, E. By. r. d, c, f. By. p. 50. l. 6 f. CF. r. CG. p. 51. equal. r. equal. p. 57. l. 18. f. EFAB. r. EFHB. p. 65. l. 17. r. Now the.

ERRATA to *Opticks*.

PAGE 87. Line 14. For Fig. 11. Read Fig. 10. p. 88. ult. c. (Fig. 28.) p. 89. l. 5, 7, 17, 25. f. (Fig.) r. (Fig. 28.) Ibid. f. (Fig.) r. (Fig. 8) ibid. l. 16. f. Surface BD. r. BC. p. 104. *Convex.* r. *the Reflex.* p. 107. l. 8. f. *is look'd to be, r. is look'd on to be.* p. 108. *Convex.* r. *the Reflex.* p. 110. l. 2. f. *to the Prop. be requir'd.* *to be here required.* p. 113. l. 1. f. *Theor. II. r. Theor. IV.* ibid. l. penult. f. *And whereas.* p. 114. l. 4. f. *EDG. r. ADC.* p. 118. l. 5. f. *BBF. r. bbf.* ult. f. 2: *As, r. a: bf.* p. 122. l. 29. *Subduplicates. r. Submultiplicates.* p. 123. (of the Angle CBM) r. of the Angle (CBM), ibid. l. ante p. Fig.) r. (as Fig. 29) p. 126. l. 10. f. Fig. 30. r. Fig. 36. p. 127. 3 *AB. r. 2 AB.* p. 133. l. 28. f. *Concave, r. Convex.* ibid. l. 29. *Concave.* ibid. l. 30. f. Fig. 36. r. Fig. 35, and 36. p. 141. l. 28. p. 148. in Margin, f. Fig. 46. r. Fig. 47. p. 151. l. 3. f. *OF a Cr.* l. 8. f. *Charistalins, r. Chrystalins.*

In Astronomy, Page 63. Line 15. Read, *Three Diameters*.
In Chronology, Page 33. After these Words, (in the last
of the Text,) viz. *and in the Calendar adjoining to this Table*
as follows: *Or else the Golden Numbers are call'd the Prime,*
Luna Prima or the First Day of the New Moon; according to
the way of speaking the Full Moon is frequently stil'd Luna Quarta
falling on the fourteenth Day after the New Moon inclusively.

Fig. 1.

Fig. 1.

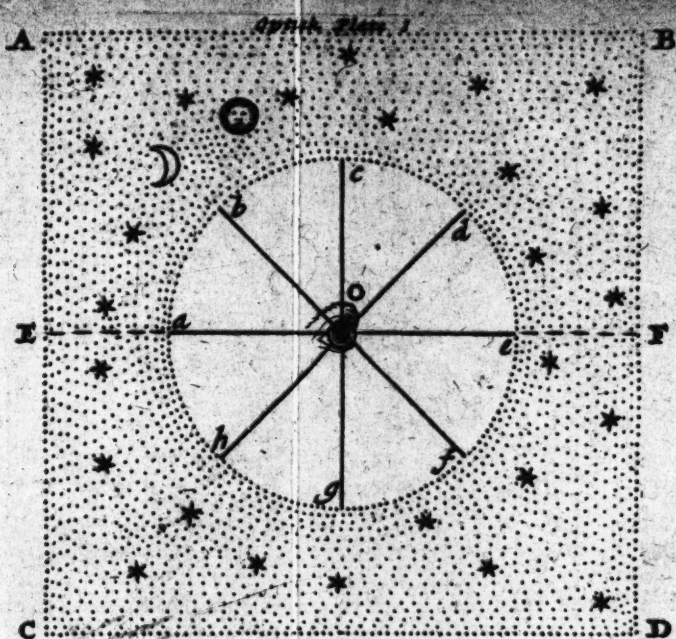


Fig. 2.

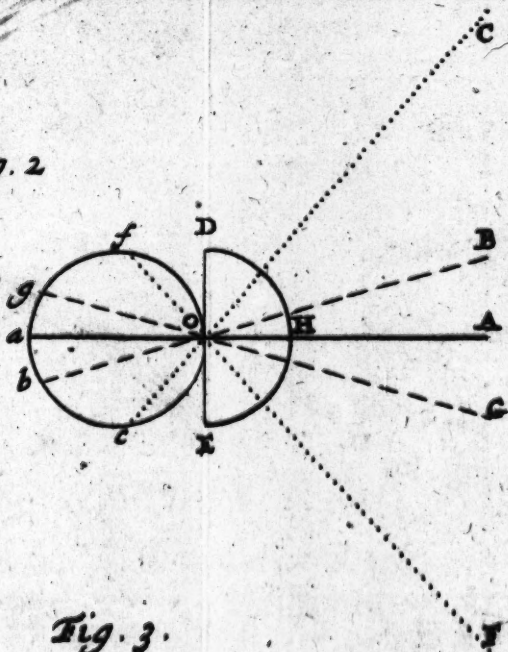
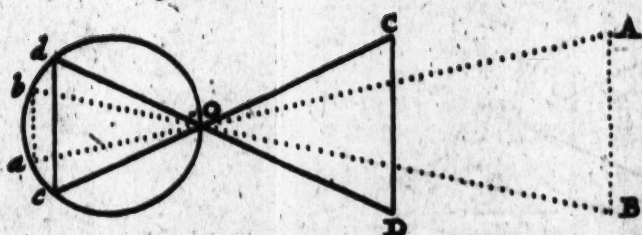


Fig. 3.





Optick Plate 2.

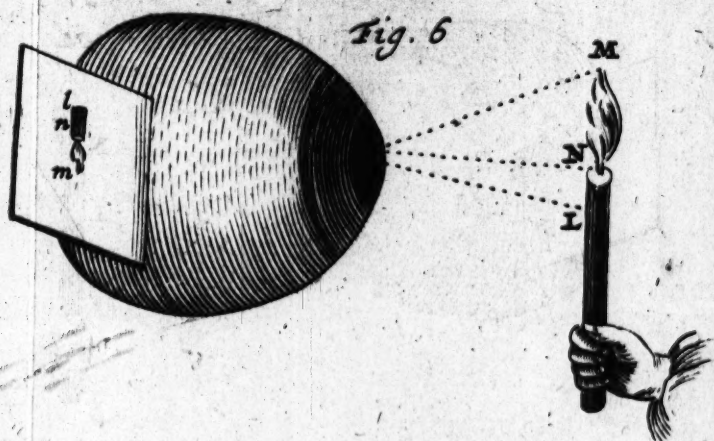
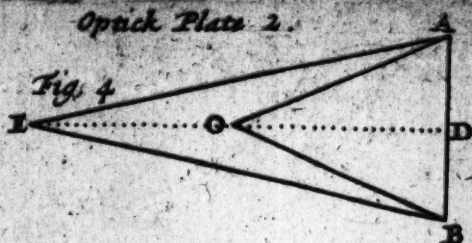
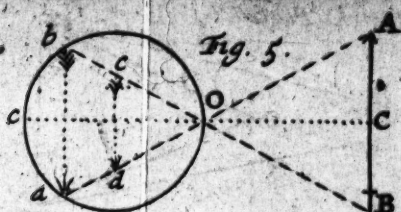


Fig. 7.

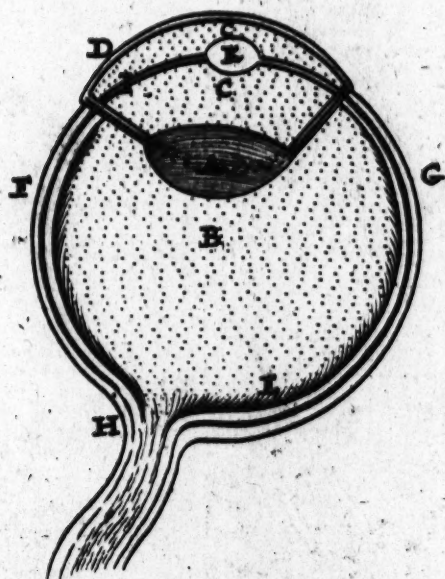


Fig. 8.



Fig. 1.

Fig. 15



Fig. 1

Fig.

H



Optick Plate 4.

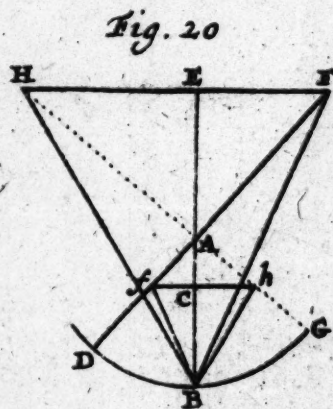
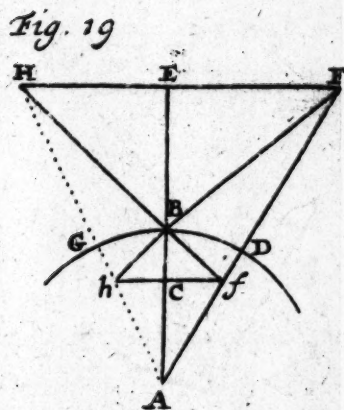
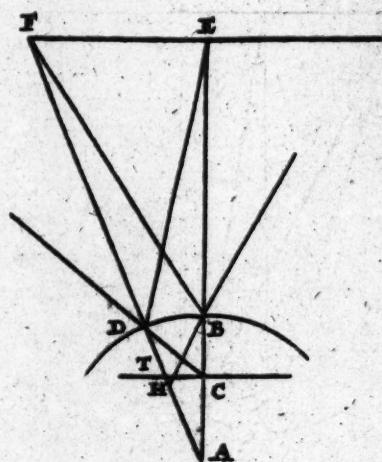
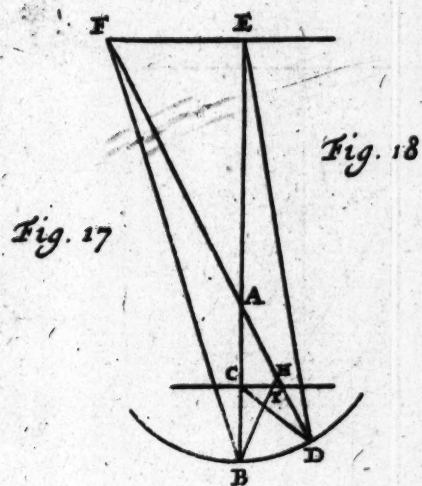
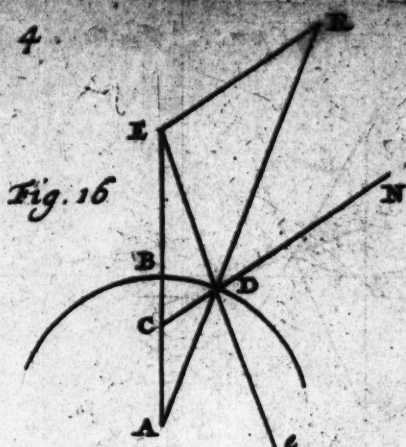
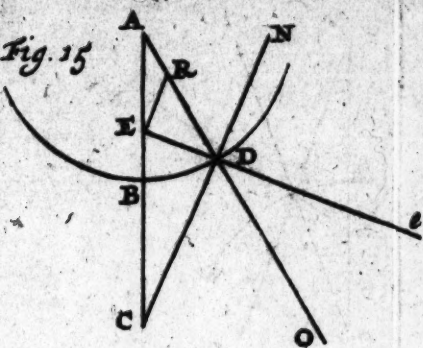


Fig. 1



Fig. 2

Fig. 3

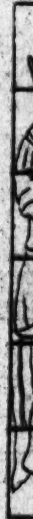


Fig. 21

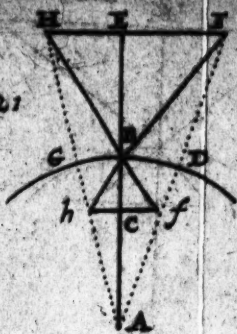
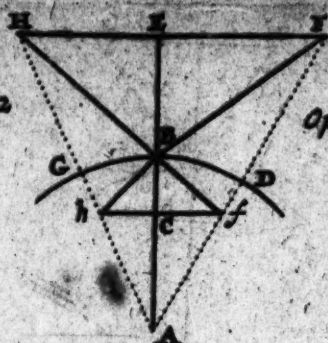


Fig. 22



Optick P. 5.

Fig. 23

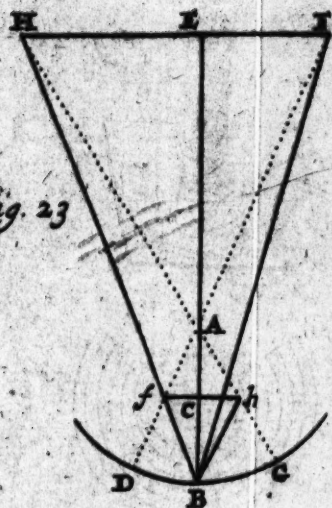


Fig. 26



Fig. 25



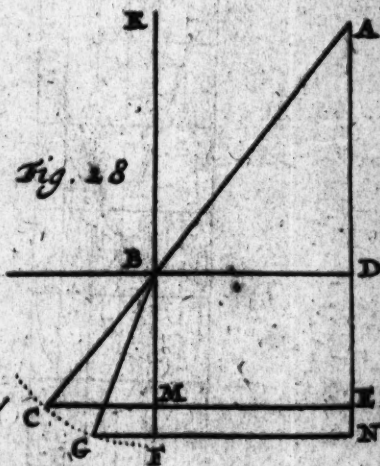
Fig. 24



Fig. 27



Fig. 28



Opnick

Fig. 29



Fig. 37

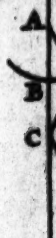


Fig. 4



Fig



Fig. 29



Fig. 30

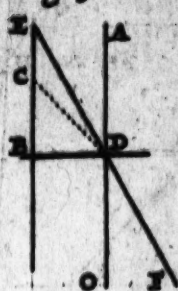


Fig. 31



Fig. 32



Fig. 33

Fig. 34



Fig. 35



Fig. 36



Fig. 37

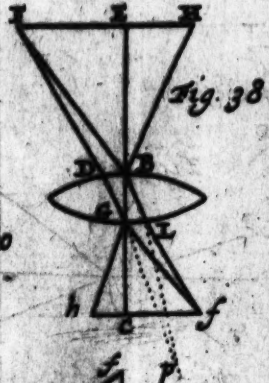


Fig. 38

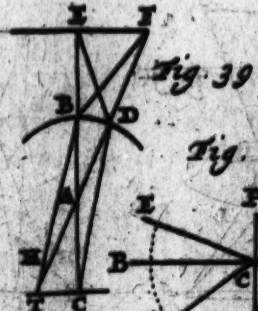


Fig. 39

Fig. 40

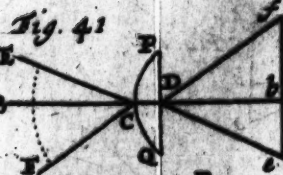


Fig. 41

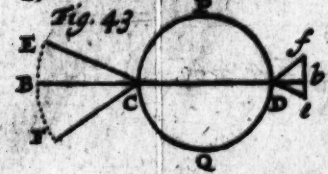


Fig. 43

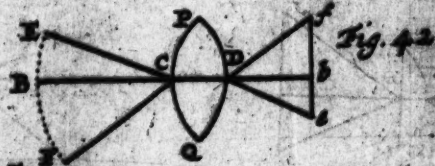


Fig. 42

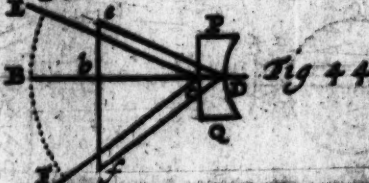
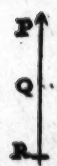
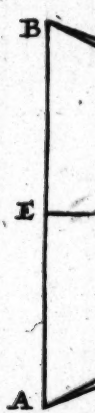
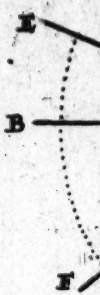


Fig. 44



Optick Plate 7.

Fig. 45

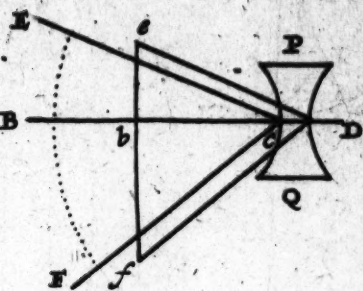


Fig. 46

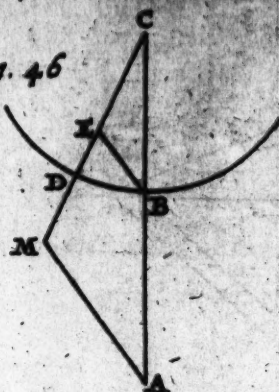


Fig. 47

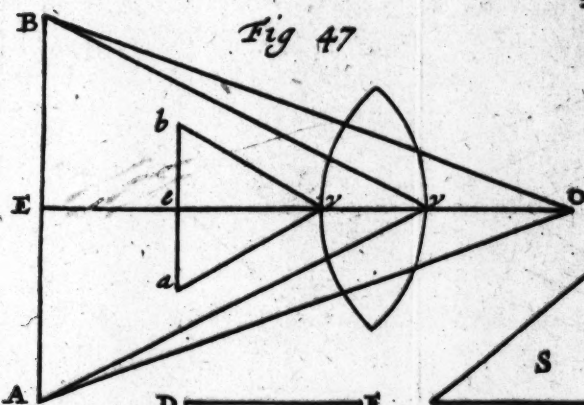


Fig. 47



Fig. 48

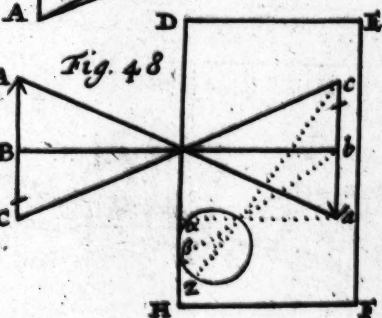


Fig. 49

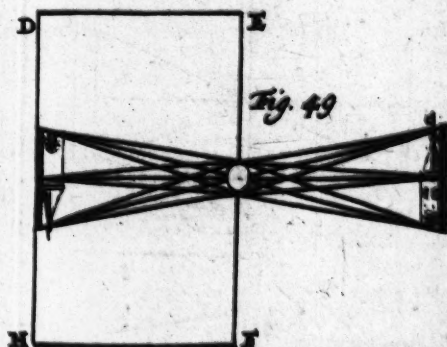


Fig. 50

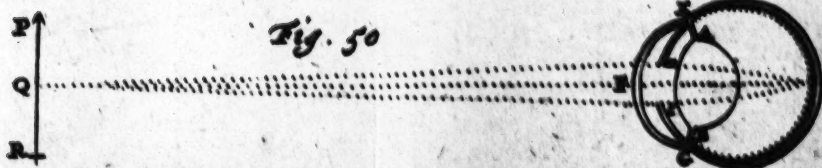




Fig.



Fig. 51.

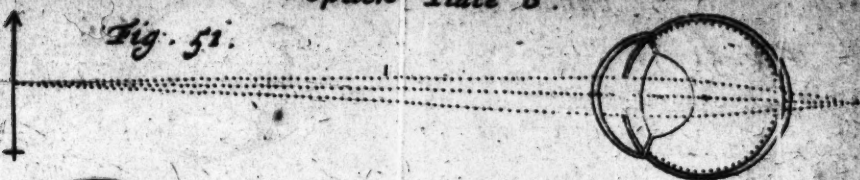


Fig. 52.

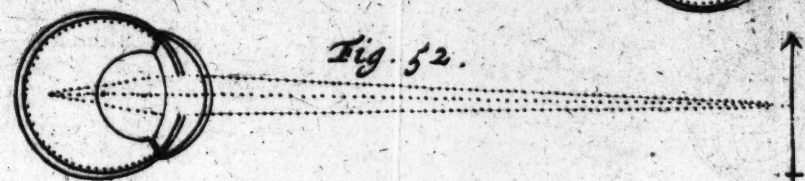


Fig. 53.

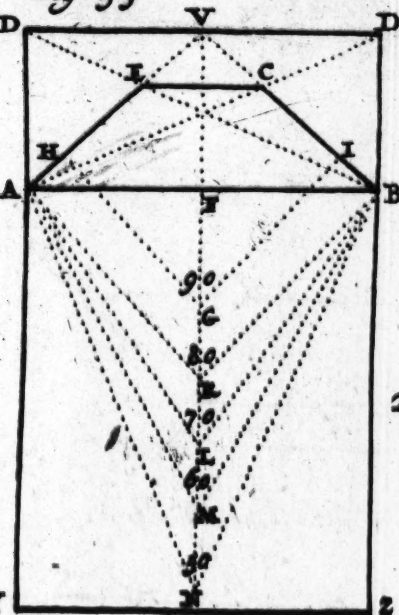


Fig. 54.

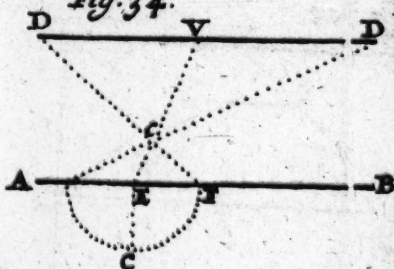


Fig. 55.



Fig. 56.

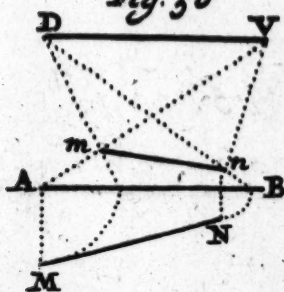
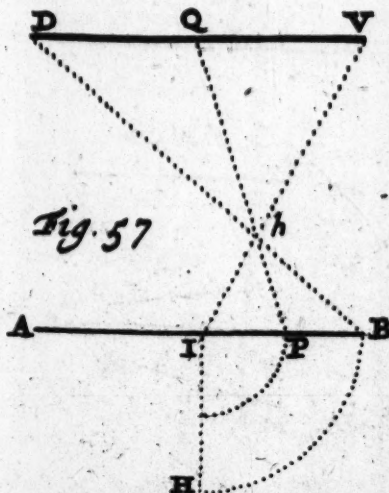


Fig. 57.



V

Γ A

Y

Optick Plate 9.

Fig. 58.

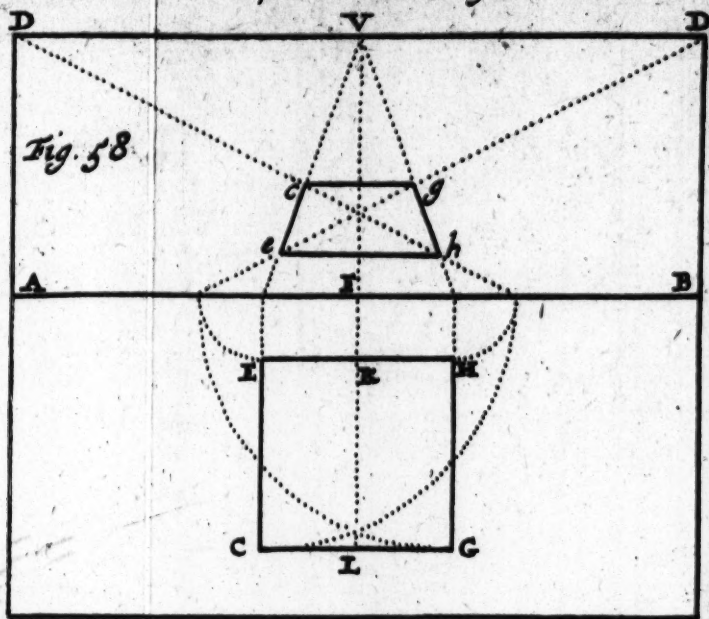
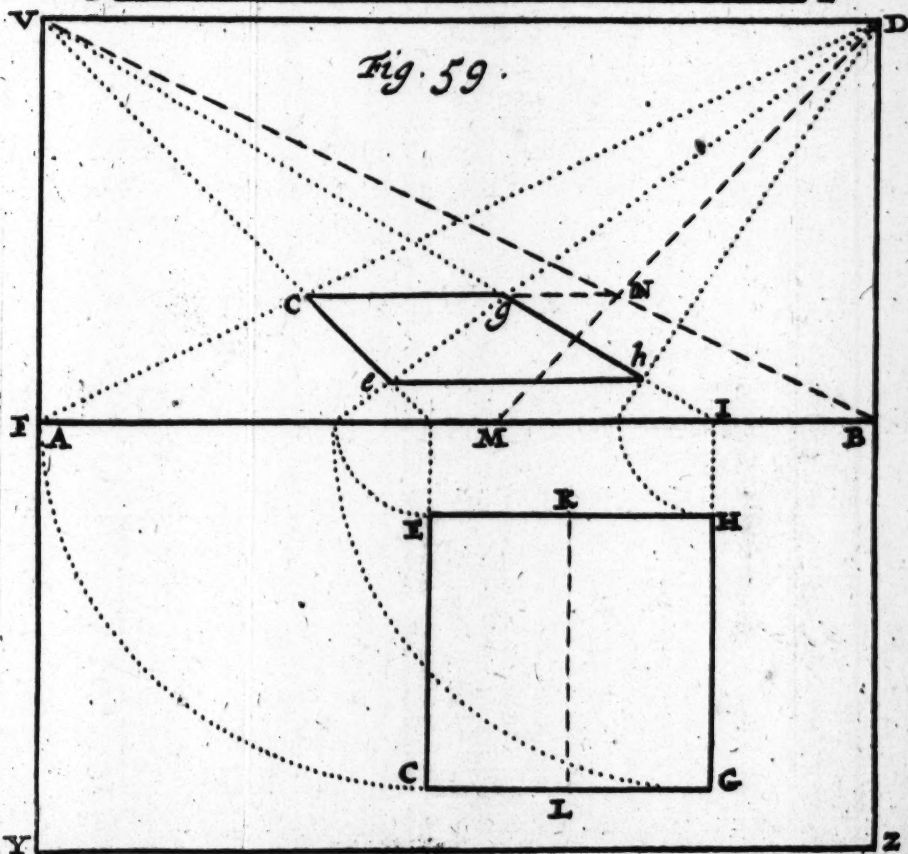
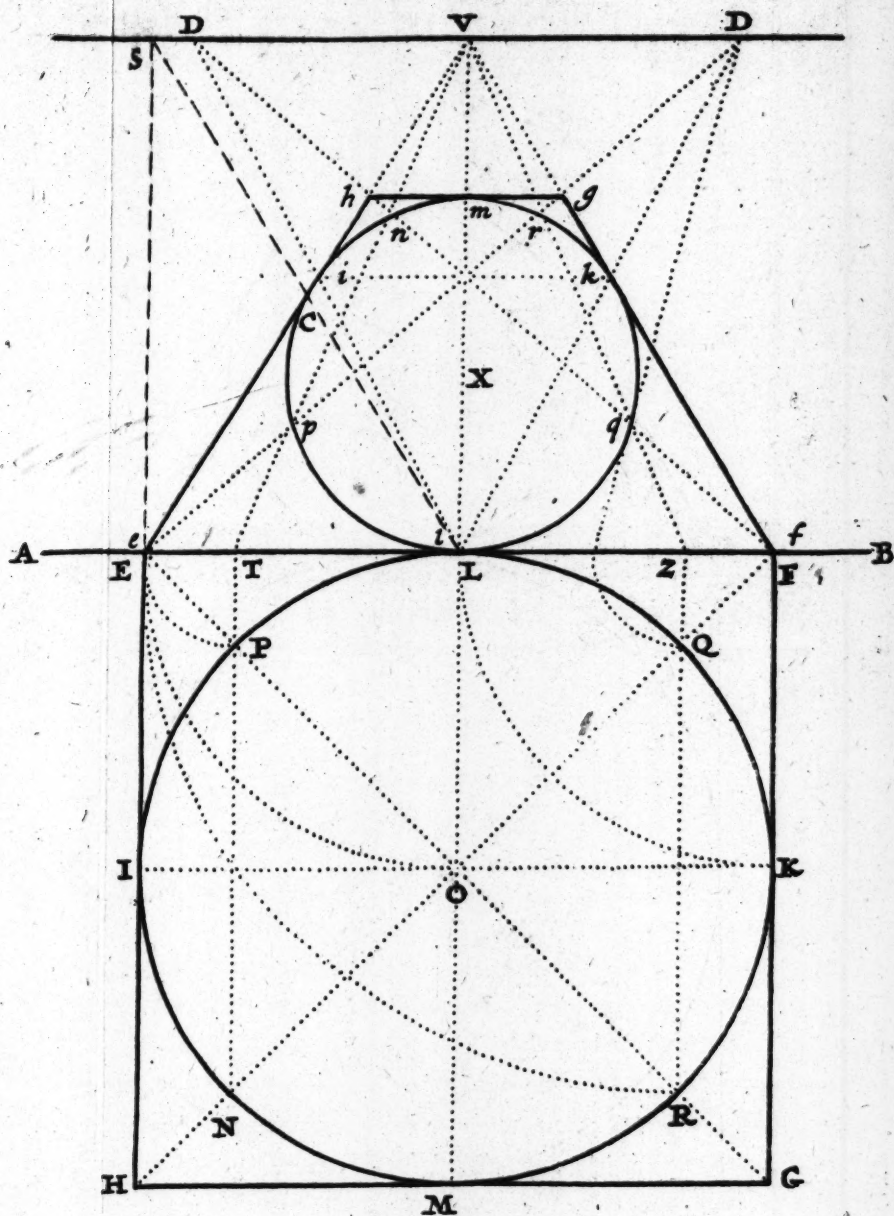


Fig. 59.



A-

Fig. 60.



A

D

K

E

A

Fig. 61.

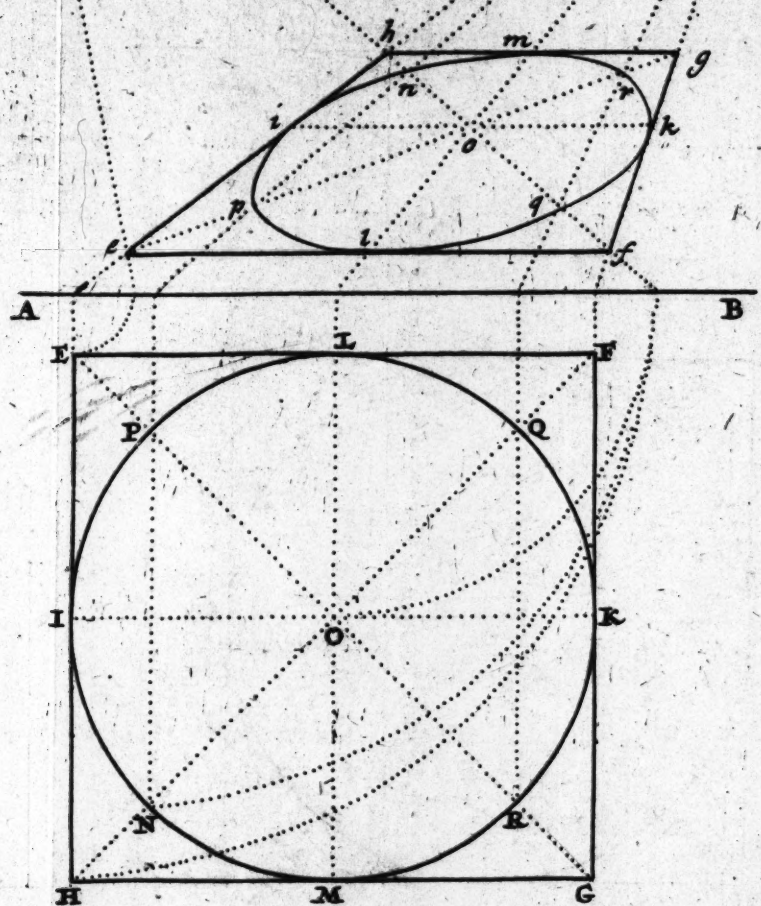
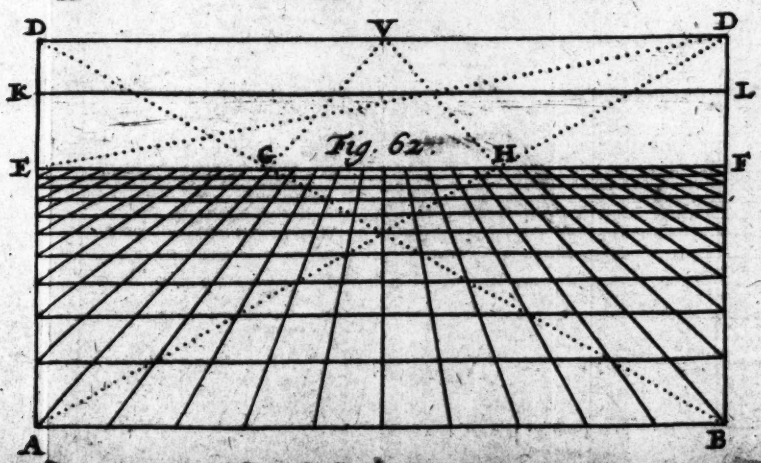


Fig. 62.

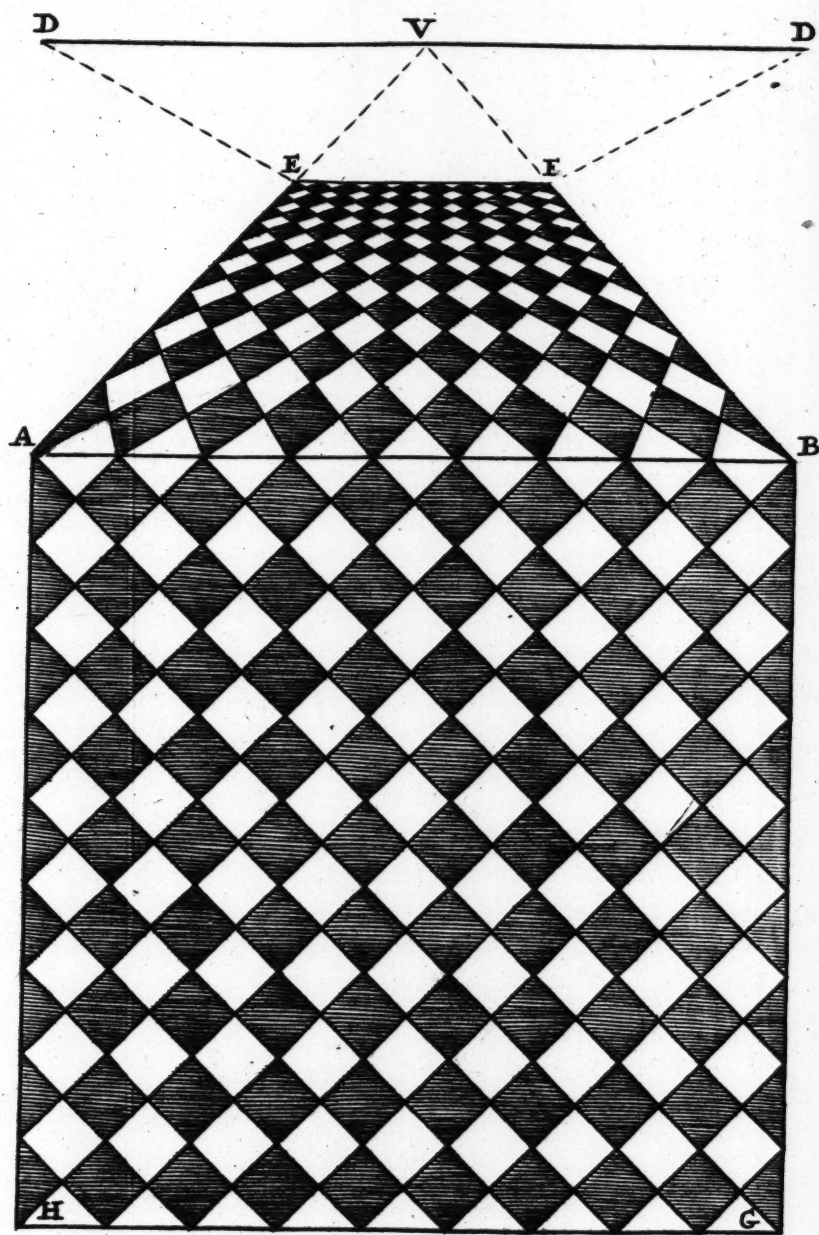


D

A

H

Fig. 63 .





Fi

Fig. 64

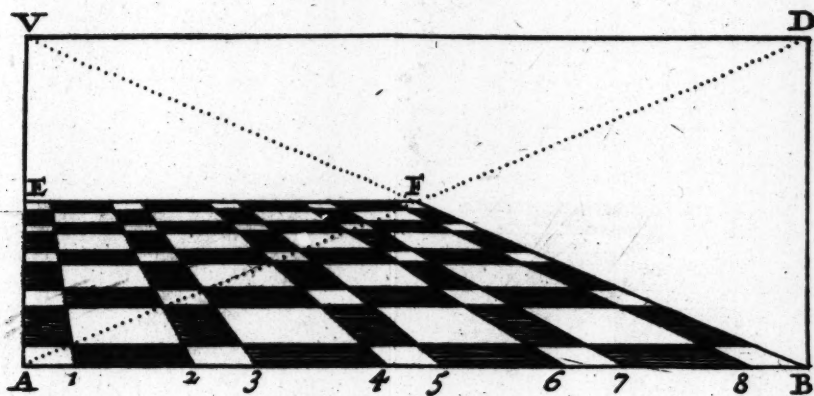
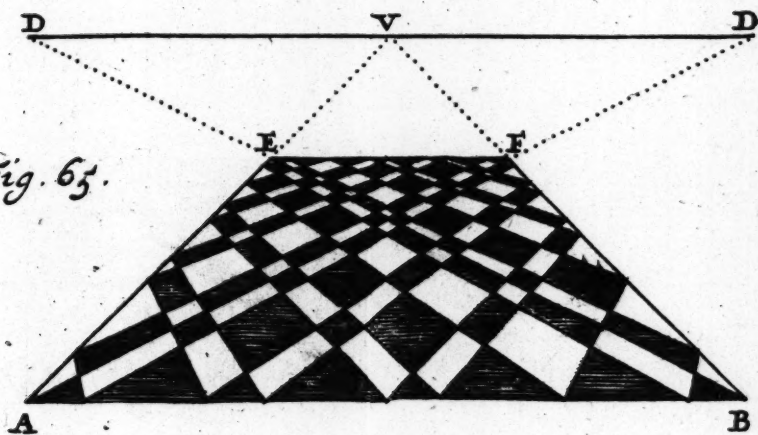


Fig. 65.



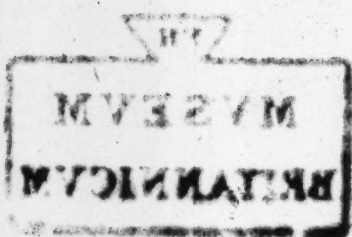


Fig. 66.

